LAND USE TYPES, SOIL PROPERTIES, AND URANIUM PHYTOACCUMULATION AT TWO ABANDONED MINE SITES IN NORTHWEST NEW MEXICO

by

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INTRODUCTION

STUDY PURPOSE

Soils with uranium contamination exist due to mining in many different climatic regions. For large areas with diffuse surface uranium contamination, plant uranium uptake from the soil is a potentially cost-effective remediation technique.

Phytoremediation of U-contaminated soils has been explored in temperate U.S. areas, but not in more arid areas. Semi-arid soils are significantly different from those in temperate areas as they typically have a higher pH, higher calcium carbonate content, and less organic carbon. Geobotanical studies in the Four Corners area have found evidence of accumulation of uranium in native plants, suggesting the possibility of phytoremediation in New Mexican semi-arid soils.

This study has three goals: 1) to describe semi-arid soil properties and geomorphology and relate these to uranium distribution at an old mine site. 2) to identify the plant species which uptake uranium in arid soils. 3) to relate the plant efficiency of uptaking uranium to arid soil properties such as carbonate content, alkaline pH, cation exchange capacity, and soil texture.

Naturally occurring uranium phytoaccumulating plants in New Mexico are identified through the evaluation of uranium uptake of plants at two old mine sites NW of Grants, NM. Relationships between site soil properties and geomorphology with uranium are also explored. The geomorphology of the site is broken into 4 "Land Uses," each with slightly different soil properties.

STUDY SITES

Two locations were selected from areas with diffuse uranium contamination, based on suggestions from Peter Luthiger of Rio Algom, and Michael Landon of the New Mexico State Land Office. The two main study sites are ~40 miles northwest of Grants, NM, adjacent to Rio Algom property. Both major mine sites were underground mines, but surface activity created a range of site conditions including waste piles, a tailings pond and a disturbed plain. In this study, these different areas of the abandoned mine are called *land use* areas. Each abandoned mine site is characterized by a flat disturbed plain, former drainage/ ponded water area, and mine waste piles. The waste piles are typically distinct, 3-4 meter tall hills which are very bare of vegetation. They are comprised of a homogenous sand at the surface, with some iron mine waste (crusher mill balls, general building material). The formerly ponded areas are depressions, with or without confining berms. These appear to have more organic matter and better water availability—the soil surface is darker, and supports more vegetation than the surrounding disturbed areas.

Minor additional plant sampling was done approximately ten miles southeast of the two major study sites in the Poison Canyon mine area in order to survey the area for additional plant species.

SECTION 27

The 'section 27' mine is privately owned but monitored by Rio Algom. The sampling site is $300 \text{ m} \times 400 \text{ m}$, and has an average elevation of 7030 feet. The site has a shallow arroyo that increases to $\sim 1 \text{ m}$ depth and drains west. The section 27 mine was closed more than 30 years ago, and left unremediated (Luthiger, 2001).

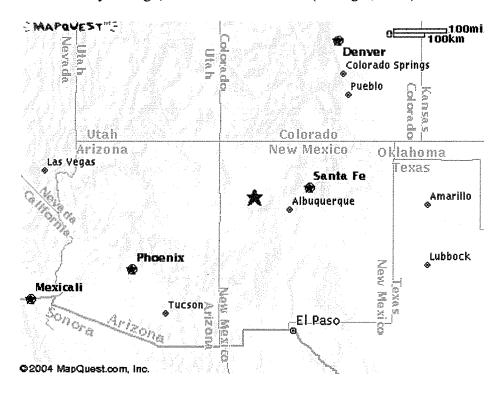
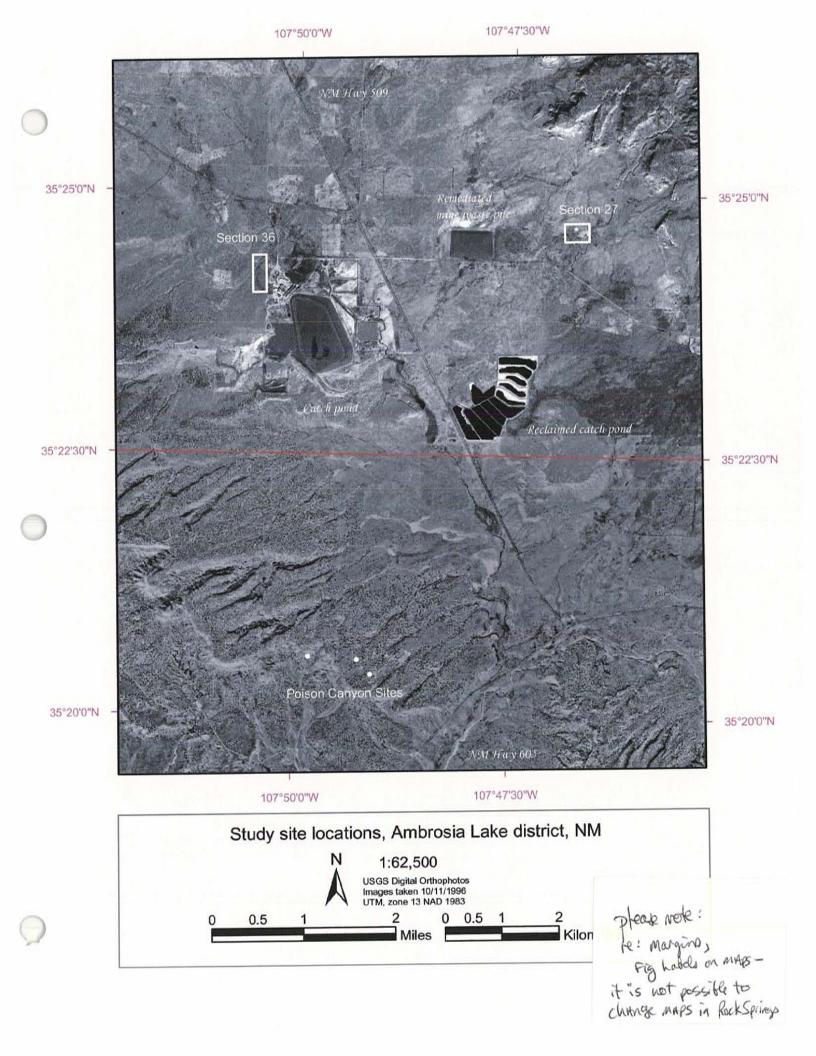


Figure 1. General Study Site Location, northwest New Mexico.

SECTION 36

The section 36 mine was one of the original mines in the area, and has been undisturbed for 50 years (Landon, 2001). It is state land with permitted access. It is directly west of the current Rio Algom operation, which is 2 miles south of the Ambrosia Lake ghost town. The site is approximately four miles southwest of the Section 27 site. The sampling site is 600 m x 200m and is at an elevation of 6970 feet. The site has a central depression which drains northward, but is a small closed basin within the site.





OVERVIEW

In 1959, New Mexico produced 3.3 tons of uranium, predominantly in the Bluewater-Ambrosia Lake area. Sixty mines were in operation at various times through 1952-1962 (Gay, 1963). The uranium boom ended in the early 1980's, due to international price competition and cutbacks in building nuclear power plants. (Chenoweth, 1990). Rio Algom, the last operating New Mexican uranium mill, closed in 2002.

The uranium ore dewatering and milling process produced significant amounts of mine waste and mill tailings containing variable amounts of uranium ore, both often left at the mine site. Some large mine sites in the Ambrosia Lake mining district have been intensely remediated, but sites with more diffuse contamination remain unremediated. Diffuse contamination remains at abandoned uranium mines throughout the semi-arid American West, including mine sites in NM, Ut, Wy, and Co. These sites typically have uranium contamination at the surface from waste rock, the ore dewatering process, and mine tailings. Rio Algom continues to work contractually to clean up a number of the abandoned mine sites in the Ambrosia Lake area.

The diffuse nature of the contamination, as well as the semi-arid climate and the radioactivity and metal toxicity of uranium make remediation a challenge. Soil uranium concentrations are below 1000 ppm. A technique that can remove a relatively small amount of uranium from a large soil volume is needed. Two current approaches for removing uranium from contaminated soil are soil washing and phytoremediation.

Soil washing can be a physical or chemical process. Physical methods involve wet screening or attrition scrubbing (Francis and Dodge, 1998). Chemical methods involve liquid additions to the soil (acidic or basic) in order to dissolve and remove uranium (Francis and Dodge, 1998). Fifty-three to ninety-three percent of uranium was extracted in different applications of soil washing (Elless and Lee, 1998; Duff et al., 2000).

Leach-based remediation is often less efficient at extracting uranium than uranium mining, due to the heterogeneous nature of soils. Soil washing generates large volumes of liquid waste, and involves a drastic alteration of soil physical and chemical properties. The leachate becomes a difficult-to-dispose-of "mixed waste," in addition to the uranium possibly left at the site (Duff et al., 2000). The soil washing process may purge the soil of iron, magnesium, calcium and silica, which are common soil elements (Duff et al., 2000). Soil washing agents can persist in the environment and may cause post-remediation radionuclide migration (Francis and Dodge, 1998). After soil washing, site vegetation restoration is often difficult because of the major soil chemical changes (Huang et al., 1998). High standards of remediation, requiring complete removal of uranium, can also make soil washing financially challenging (Duff et al., 2000).

Uranium phytoremediation is based on sequestering the contaminant to be removed within the plants grown on the contaminated site. This is a low cost and low impact alternative to soil leach remediation. Phytoremediation uses specific plants to target the contaminant of concern: plants can extract and concentrate metals from the soil, or degrade organic contaminants. This process generates a minimum amount of secondary waste and allows in-situ treatment (Huang et al., 1998). Plants that have taken

up uranium can then be gathered and ashed to reduce the amount of total remediation waste.

Phytoremediation combined with citric acid soil treatments can have up to a 99% uranium recovery rate (Francis and Dodge, 1998). Citric acid is a preferred 'soil washing' agent because it is a consistent biodegradeable multidentate complexing agent. In the case of less efficient extraction rates, the phytoextraction procedure can easily be repeated without harm to the soil.

Most uranium phytoremediation studies to date have been made in the eastern United States or in Europe (Baumgartner et al, 2000; Hossner et al, 1992; Huang et al, 1998; Meyer et al, 1998; Pfeifer et al, 1994; Saric et al, 1995; Yoshida et al., 2000). Soils of the western United States are more arid, with higher pHs and lower organic carbon content than temperate soils of the eastern United States or Europe. Both soil pH and carbon content affect uranium solubility in soil water. Conclusions drawn from studies of uranium phytoremediation in temperate soils cannot automatically be extended to more arid regions.

Oftentimes, different soils and climate dictate the natural plant community's species composition, or the type of crop plants grown in a certain area. Plants used for phytoremediation in the eastern United States will probably not grow in semi-arid areas, or accumulate uranium at the same rates. The applicability of uranium phytoremediation to soils of the western United States remains unexplored.

HYPOTHESES

Land Use Types:

 Land use types will show differences in their soil uranium content. The more disturbed areas will contain more uranium.

Null hypothesis:

Soil properties and land use type do not affect the distribution of uranium.

Uranium in soils:

• Uranium concentration increases in proportion to changes in soil properties—for example, increased pH, or decreased CaCO₃ content.

Null hypothesis:

Soil uranium content is not affected by soil properties.

Uranium in plants:

• Certain species accumulate more U than others (U per gram plant: U per gram soil).

Null hypothesis: All plant species will accumulate uranium equally well.

BACKGROUND

URANIUM CHEMISTRY

Different uranyl species form in different pH environments (figure 2). At higher, alkaline pH, UO₂CO₃⁰ and carbonate complexes predominate. Increasing pH also increases sorption by favoring precipitation of uranium minerals and complexes (Willett, 1995). Sorption of uranyl onto natural materials is maximal in the pH range 5.0 - 8.5 (figure 2). Turney (1995) found post-experiment pH of soil effluent to be "...an indicator of overall U removal from the soils" (p. 102). This suggests that soil pH could be a controlling factor on uranium phytoextraction.

Uranyl sorption onto soil is readily reversible with changing pH (Willett, 1995). This means that uranium sorption is a reversible process when based on changing soil conditions, such as the wetting and drying cycles of semi-arid soils.

Uranium primarily takes two cation forms -- U (IV) or U (VI). Each is soluble under different conditions. It is useful to briefly examine these conditions as it provides more specific insight into uranium's behavior in semi-arid soils. Due to the oxidizing conditions prevalent in semi-arid soils, U(VI) is the dominant species. In these soils U(VI) is very soluble as it forms stable complexes with chlorides, sulfates, and carbonates (Turney, 1995). The CO₃ ligand is primarily associated with the U (VI) and OH with U(IV) (Jurinak, 1993). Adsorption of U (VI) onto soil particles strongly increases from pH 4.5 - 5.5, and decreases from pH 7.5 to 8.5. This is the likely pH range of semi-arid soils, which means that U (VI) is more available for plant uptake in semi-arid soils.

Uranium (IV) is typically extremely insoluble; it occurs in very low concentrations in soil water (< .01 ug/L). It is more likely to dissolve below pH 2 or above pH 7 (Elless and Lee, 1998; Watt, 1996). Uranium (VI) appears in figure 2, below, as (UO_2^{2-}) . In figure 3, U(IV) appears as the species $U(OH)_5^{-}$.

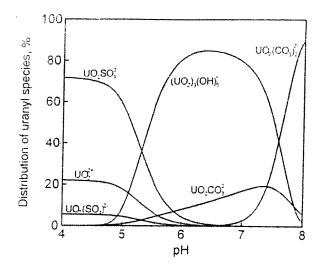


Figure 3. Uranyl species as a function of pH. Calculated at 25 C for .0025 M MgSO₄, 10 mg U L⁻¹, and in equilibrium with atmospheric CO₂. (Willett et al, 1998).

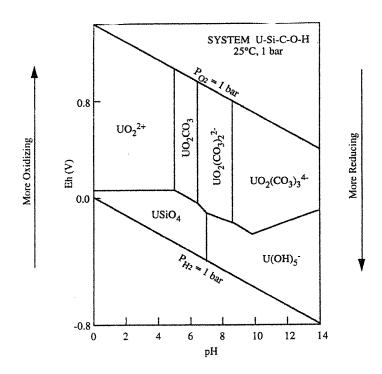


Figure 4. U-Si-C-O-H Pe-pH diagram. Assumed activities for dissolved species are: U= 10⁻⁸ M, C= 10⁻³ M, and Si=10⁻³ M (Brookins, 1998) (Turney, 1995).

Uranium movement varies between soil horizons because of different chemical and physical properties in each horizon. Soil properties and soil development relevant to uranium presence in arid soils are described later in this section.

GEOLOGY OF AMBROSIA LAKE DISTRICT

The Grants mineral belt extends from the Laguna area in a northwestern direction for approximately 100 miles, ending north of Gallup, NM. The late Jurassic Morrison formation, part of the Colorado Plateau sedimentary sequence (figure 9), is the host for more than 90% of these uranium deposits (Santos, 1963). It is primarily an arkosic sandstone with minor amounts of layered mudstone.

Ambrosia Lake uranium deposits typically occur in paleo-fan systems; here, they are fluvial sandstones with mudstone interbeds (Galloway, 1979). The Poison Canyon

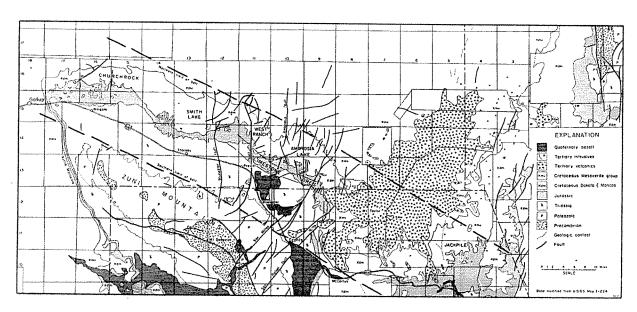


Figure 5. Geologic Map of Grants Uranium District, showing the Grants mineral belt and mining areas (Laverty et al., 1963).

ore body is in the Brushy Basin member of the Morrison formation, which is stratigraphically higher than the Westwater Canyon member (Fitch, 1979).

	:		Str Tooque		V	Gray, year fine grained sandstone
		Dakota	Pagnate Ss Tongue Day Mesa Sh Tongue		50-90	
	4	Sandstone	Cubero Ss		\	Dark gray shale (Mancos)
coaer Eertococo		Sanustone	Dak Canyon Member			Gray, very time-grained sandstone
		Morrison Formation	Brushy Basin		85-160	Upper part—Light gray and grayish tan, carbonaceous, very fine grained sandstone and silistone Lower part-Pale yellowish brown, orange, white, tine- and medium-grained sandstone
			Westwater Canyon		40-220	Greensh gray mudstone with minor lenticular, light gray and yellowish gray, line, and medium grained sandstone.
ں					90-290	Light yellowish and reddish gray, medium grained sandstone, with greenish-gray, lenticular mudstone
SSİ			Recuptive		70-250	Interbedded vangated modstone claystone sultstone and sandstone
er Jura	San Rafael	Bluff Sa	endstone		235-370	White Inphi gray gravish yellow, pale change, and reddish brown fine grained massive crosshedded sandstone
bbe		Summerville Formation		The state of the s	160-270	Interhedded varigated mudstone and siltstone, fine to very line grained sandstone
-		Todilto 1	mestone Tilling		25-35	Pale olive gray, dark olive gray, and pale yellow, thick helded finestone
		Entrada	Upper Sandstone	A	150-185	Moderate brown, bine gramed, massive crosshedded sandstone
		Sandstone	Med al Silistore	<u> </u>	40-60	Grayish red brown calcateous siltistone
- In 47 - 1 - 1 - 1			lyanteto		80-115	Moderate brown to moderate reddish orange, medium grained, crosshedded sandstone
			Owl Back		<u> </u>	Create the cast of the street and obstance analysis designed as the state of the street of the stree

Figure 6. Detail of the Stratigraphic Section of the Ambrosia Lake Area, McKinley and Valencia Counties, New Mexico (Chenoweth, Learned, 1979).

GEOMORPHOLOGY OF SOUTHWESTERN SAN JUAN BASIN

The San Juan basin is a sedimentary basin containing Jurassic and Cretaceous sandstones and limestones (Santos, 1963). Regional faulting occurred in the early Tertiary, uplifting the Brushy Basin outcrop in the Poison Canyon area. Downfaulting a mile northwest put stratigraphically adjacent uranium deposits at ~1000 foot depth. Uplift of the Colorado Plateau in the Miocene and Oligocene resulted in regional exhumation of the area. Resultant faulting currently defines some of the edges of local mesas and plains (Connors et al., 1987).

Quaternary deposits in the area consist of alluvial, playa, colluvial, and eolian sediments (Smith & McFaul, 1997). Both study sites are on flat eolian plains, sand and silt sheets, that have developed in the past 15,000 years (Smith, McFaul, 1997). There is a present-day low rate of eolian transport (Wells et al, 1983).

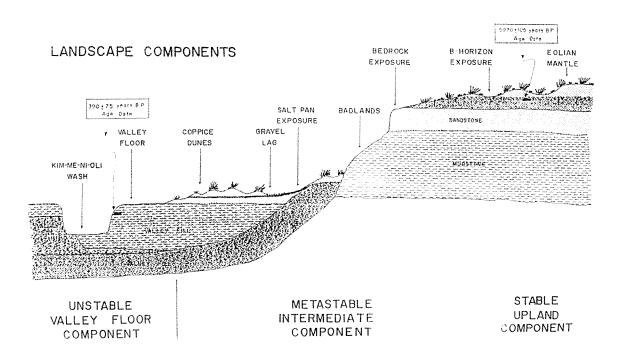


Figure 7. Cross-section of San Juan Basin landscape elements (Connors et al., 1987).

MINING HISTORY

A description of the mining techniques used gives insight into the nature of the contamination and the origins of the landforms produced. Mining operations typically disturbed the local area, resulting in a landscape containing waste rock/ mine waste piles, a disturbed plain and lowlying areas where drainage occurs.

In 1948, Poison Canyon was the first uranium mining operation in the Grants district (Melancon, 1963). By 1963, 47 mines were operating (Chenoweth and Holden, 1980). Ninety percent of all local production in 1963 was from wet-ore (below the groundwater table) bodies. Excess water was pumped and released at the surface adjacent to mine sites.

Mining Technique

In the Ambrosia Lake area, the vertical mineshaft was sunk to ore-bearing formations ranging from 600 to 1,400 feet depth. From the shaft, various levels were created in waste rock, beneath the ground-water saturated ore bodies. The mine water was pumped to the surface where it was collected for use in the mill. The volume of water pumped from each mine varied from 200 to 2,000 gallons per minute (Luthiger, 2002). Ore was cut from the ceilings of the mine tunnels. From there, it was transported to the surface and to the processing mill.

At the mill, the grayish sandstone ore, heated and dried, passed through a primary and secondary crusher and a sample tower. The ore then passed through a fine ore bin and into the rod mills which ground the ore to -28 mesh. The ore slurry (30% water added, 70% ore) was pumped to the leaching agitators where sulfuric acid and sodium chlorate were added. Uranium and any other metals that were soluble in

sulfuric acid were dissolved. The sodium chlorate oxidized the ore, which sped up the leaching process and improved the recovery. At the end of the leaching phase, the ore was pumped into cyclone classifiers for sand-slime separation (Luthiger, 2002).

The separated sand, still in a slurry state, was thoroughly washed with acid-water solution. The uranium was thus separated from the individual sand grains. The barren sand was then pumped to the tailings disposal pond. The separated ore-slurry-slime was pumped to the thickener circuit. It was washed to remove attached micro particles of uranium. Barren slime removed from the last thickener was also pumped to the tailings disposal pond. Ninety to ninety-seven percent of the ore's uranium was now in the acid-water-rock solution (Luthiger, 2002).

The leaching process also removed metals other than uranium from the host rock. The acid-water solution often contained trace amounts of vanadium, molybdenum or iron. It was necessary to extract the uranium from the acid-water solution by a liquid ion exchange process, which transferred the uranium to a solvent at three times the concentration (Luthiger, 2002). The resultant uranium-free, acid-water solution, or "raffinate," was pumped back to previous circuits as a washing solution, or to the tailings disposal pond. The uranium, in the solvent solution, was pumped to the stripping circuit. Here the uranium was stripped from the solvent and again concentrated. Ammonia, air and heat in the precipitation circuit precipitated the uranium from the solvent solution. The uranium moved through a thickening tank and a filter circuit where it was thoroughly washed and dried. The final product contained 80 to 90 percent uranium oxide in a <0.25 inch particle size (Luthiger, 2002).

In conclusion, barren acid-washed sand, barren acid-washed slime, acid-water solution with iron, vanadium, and molybdenum, and ore-dewatering groundwater pumped to the surface were added to the tailings ponds at the various mill locations. This process disturbed soils and ultimately resulted in the creation of a new landscape. The original soils were often covered over or removed. Vegetation was largely removed, and often only hardy or invasive vegetation has been able to return.

Geomorphology of the Mine Area

The post-mine landscape can be separated into four areas: waste piles, disturbed plains, drainage and/or former pond areas, and adjacent, lightly disturbed or undisturbed areas. Waste piles are made up of white, barren, homogenous medium sand from tailings and waste rock in 2 -5 meter tall piles.



Figure 8. Looking west across S27, viewing disturbed plain, with waste pile and undisturbed areas in the distance.

The ore dewatering and tailings pond or *drainage area* has a lower elevation and denser vegetation. The drainage area soil retained clays and some additional organic carbon. The *disturbed plain* is the area around the headframe and the abandoned mine site, with solid mine waste deposits over the surface soils in some areas. Areas adjacent

to the site remained *undisturbed*. Each *land use area* received different degrees and types of uranium contamination. There is waste rock uranium and leftover tailings uranium in the waste piles; uranium leached into the soils underneath the drainage areas; and blown uranium-contaminated dust over the undisturbed areas. A combination of the above, as well as refuse and truck ore-spill, impact the disturbed plain.



Figure 9. Looking east -southeast across S36, viewing undisturbed area in foreground, drainage area in middle, and existing Rio Algom uranium mill outside of study area to the east.

CLIMATE

The area has a semi-arid climate with an average annual precipitation of 10-12 inches (Soil Conservation Service, 1993). The average annual air temperature is 48-53 C, and the frost-free period 114-150 days. Short late afternoon high intensity summer rainstorms characterize precipitation. There is also a small snow contribution during the winter months, although the ground usually remains bare, not snow-covered.

SOILS

SOIL DEVELOPMENT

Six periods of eolian deposition have formed the undisturbed semi-arid soils of the San Juan basin over the last 12,000 years (Smith, McFaul, 1997). Arid soils, as they develop with time, show increases in silt, clay and calcium carbonate (Smith, McFaul, 1997). Weakly-developed soils have less potential for retarding downward movement of uranium through a soil because they lack clays and iron oxides. (Watt, 1996).

Arid soil-uranium studies found that uranium was retained in surface soil horizons (e.g. Litaor, 1995—central Co; Willett et al, 1998, 1995--Northern Territory, Australia; Shilk, 1995--Cincinnati, Oh; Watt 1996--Los Alamos, NM; Vainetti, 1996—northern Ut). More concentrated and stored uranium was found in strongly developed soils (Watt, 1996).

Studies of uranium in semi-arid soils also described the effect of different soil horizons on soil uranium distribution. A study east of the Rocky Flats nuclear plant, near Golden, Co., showed that most of the uranium was concentrated above the B horizon, located at 15-40 cm. Due to the higher clay content of the lower B horizon, uranium was retarded from further downward movement (Litaor, 1995). Highly weathered soils retained radionuclides in the surface-most few centimeters (Willett et al, 1998; Willet, 1995, and Schilk, 1995). The surface horizon had the most organic content, and water saturation caused reducing conditions. They concluded that there was no likelihood of the uranium being leached to any depth. Even in soils with weakly developed soil properties, most of

the uranium is concentrated in the upper 20 cm, within 50 m of the contaminant source



Figure 10. Section 36 undisturbed soil profile.

(Watt, 1996). A lack of water in arid areas ultimately prevents uranium from being leached further into the soil (Vaninetti, 1996).

SOIL FRACTIONS

The following soil properties influence uranium mobility: organic matter, calcium carbonate, clays (cation exchange capacity, CEC), and ferric oxyhydroxides (Elless and Lee, 1998; Watt, 1996). In one study, 20% of uranium was bound to soil carbonate, 10% to mineral oxides, and 20% to the organic soil matter (Dhoum and Evans, 1998). Uranium also binds with Fe and Mn oxyhydroxides (Watt, 1996). Clay content and mineralogy do not significantly impede dissolved uranium movement downward through a soil (Watt, 1996).

Organic Matter

Organic matter is an important reducing agent for trace elements such as uranium. However, most studies of uranium mobility in mine tailings and soils have been conducted on systems with pH <6, whereas semi-arid soils typically have pHs above 7. At high pH and high uranyl concentrations, the formation of uranyl humate is favored (Watt, 1996). The organic content of arid soils is also typically very low, often less than 1% (Vaininetti, 1996). While the organic matter that is in a semi-arid soil might be very effective in complexing uranium, the overall organic matter effect on uranium movement is probably small.

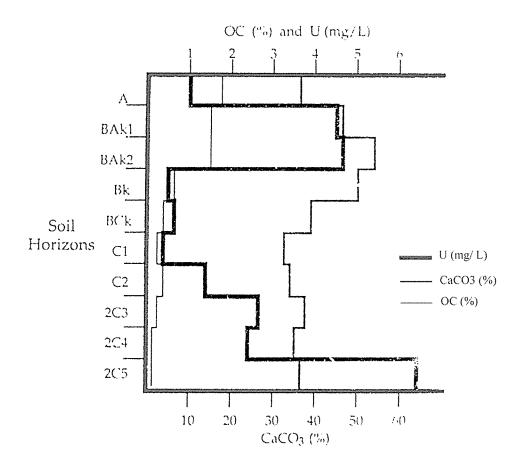


Figure 8. Vertical Distribution of OC, CaCO₃, and water-soluble U concentrations in a Nevadan aridisol. (Vaininetti, 1996).

Soil Carbonate

Uranyl carbonate species are highly mobile in soil solution (Langmuir, 1978; Willett, 1995). Adsorption in soil was lowest in high pCO₂ and low pH waters because of the formation of soluble U (VI) carbonates (Duff, 1996).

Evapotranspiration in arid climates tends to concentrate uranium and precipitating ligands, causing more uranium mineral formation (Langmuir, 1978). In arid climates, CO₂ pressures in soils and groundwaters also tend to be relatively low because of the paucity of soil organic activity (Langmuir, 1978). If the semi-arid soils in this study are

assumed to have low pCO₂ from a low plant density, and a high pH soil, these soils should therefore have fewer soluble uranium carbonates, and more uranium carbonate adsorption. As stated in the Soil Development section, carbonate content in a soil also relates to soil development. Most of the soils in this study showed little soil development and carbonate content.

Cation Exchange Capacity (CEC)

Uranium sorption increases with increasing cation exchange capacity. Two sources of CEC are clay minerals and organic matter. The type of aluminosilicate clay minerals and amount of organic material influence uranium sorption. Montmorillonite, a clay mineral with high CEC, adsorbs more uranyl ions than Na⁺ and K⁺ ions, but less than Mg²⁺ and Ca²⁺ ions (Watt, 1996). In semi-arid soils, kaolinite, a non-reactive clay, is abundant (Birkeland, 1999).

Fe and Mn oxyhydroxides

Total iron content of a semi-arid soil is typically low. Goethite is the most common iron mineral in most well-drained soils, with a yellowish-brown color (Birkeland, 1999). This tends to make up a much smaller soil fraction in semi-arid soils than another soil precipitate, calcium carbonate.

Iron and Manganese oxyhydroxides, which also occur in semi-arid soils, are complex OOH- bound soil precipitates of iron and manganese. Fe and Mn hydrous oxides are responsible for strong sorption of divalent metal cations, such as uranium (Willett, 1995). In arid soils, even though the total iron content is small, these compounds can be as or more important than CEC for uranyl absorption.

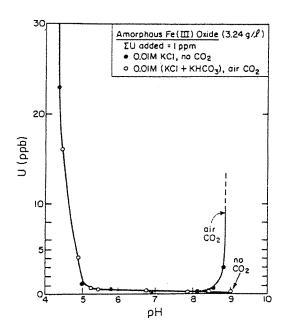


Figure 9. Adsorption of uranyl onto X-ray amorphous ferric oxyhydroxide as a function of pH (From Van der Wiejden et al., 1976, and VdW, Langmuir, 1975) (Langmuir, 1978).

Contaminant uranium concentration has been correlated with iron oxide and oxyhydroxide content, but not with total iron concentration in soils around Los Alamos, NM (Watt, 1996). More dissolved carbonate causes less U(VI) adsorption to Fe oxide and oxyhydroxide mineral surfaces (Duff, 1996). U(VI) adsorption on goethite (cis-FeOOH) increases with increasing pH in carbonate-free solutions across a large pH range (Duff, 1996). Over the pH range of 5 to 8.5, ferrihydrite (Fe₅(O₄H₃)₃) is a very strong scavenger of U (Watt, 1996; Birkeland, 1999).

LOCAL SOIL DESCRIPTIONS

The soils of the Ambrosia Lake quad have been mapped but not yet published by the Natural Resource Conservation Service (Tzschetzsche, 2003). Ambrosia Lake quad soils are consistent with the published soils of the southern adjacent Dos Lomas quadrangle. The Dos Lomas quadrangle is dominated by Penistaja, San Mateo, and Sparank soil series. These are deep soils, mainly formed on cuestas, fan terraces, flood plains, and alluvial fans (SCS, 1993). Some undisturbed soils in this region have significant calcic horizon development, although not in this area (Smith & McFaul, 1997).

The undisturbed soils of this study are Penistaja type soils, as defined by the NRCS. Penistaja soils have an extent of over 1 million acres in New Mexico, and predominate in this study area. They are formed in mixed alluvium and eolian material derived from sandstone and shale (NRCS, 2003). The Penistaja soil surface layers are a brown fine sandy loam. The subsoil is a strong brown sandy clay loam, and the substratum a reddish yellow sandy loam that is occasionally slightly calcareous.

The Penistaja soil contains a thin organic A horizon overlies a slightly leached A horizon, a B and Bt horizon enriched in iron and weatherable minerals, and a lower Bk carbonate layer with >15% CaCO₃ deeper than 40 inches. This carbonate layer becomes progressively more indurated and less permeable with time (Birkeland, 1999). The typical pedon is a fine sandy loam with up to 15% gravel. Soils at the study site are sandy loams with pale red or yellow tones.

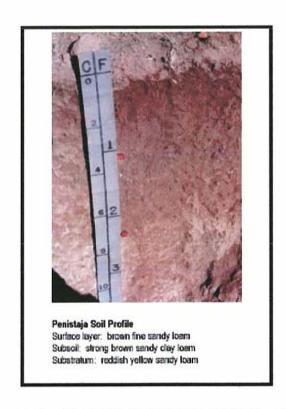


Figure 13. Penistaja Soil Profile (NRCS, 2003).

PLANTS

VEGETATION OF THE SOUTHWESTERN SAN JUAN BASIN

Vegetation in this area is primarily an eastward extension of the Great Basin desert (Dodge, 1985; Knight, 1992). It combines monostands of woody shrubs with some southern Rocky Mountain flora and New Mexico desert grassland plants. Saltbush, rabbitbrush, snakeweed, and woody buckwheat all occur in this area as small or medium woody shrubs.





Figure 14. Indian Rice Grass, right, and Spike dropseed, left.

The two study sites have vegetation representative of desert grasslands and badland lowlands. Grama grass is considered a climax vegetative species (Dewitt-Ivey, 1995). Pioneer plants include tumbleweed, goathead, and spurge. In saline or alkaline lowlands, russian thistle, pepperweed (*Lepidium montanum*) and goosefoot may be present (Knight, 1992). Intermediate stages include galleta and burro grass, cactus, and mixed weeds.

In the badland lowlands, low densities of forbs and shrubs can occur (Knight, 1992). Annuals or biennials may provide additional diversity to the shrubs, but in dry years may not grow. Alkaline clay soils support spike and sand dropseed grasses, galleta grass, and blue grama grass. Sandier soils incorporate Indian dropseed grass as a major species. Shrub growth is more precipitation dependent than determined by soil type (Knight, 1992).





Figure 15. Fringed Sagebrush, left, and Russian Thistle/ Tumbleweed, right.

PREVIOUS URANIUM-UPTAKE PLANT STUDIES

Phytoremediation utilizes plants that accumulate uranium. Plants used in uranium phytoremediation must have the ability to isolate uranium in the plant cells, preferably in above ground plant matter (Chaney, 1997). This is considered more important than high biomass of the plant, which could contribute to gross uranium extraction (Chaney, 1997).

Uranium accumulation may not always be healthy for the plant. There are two important plant reactions to a high uranium environment: detectable uranium accumulation, and anomalous growth habits (Cannon, 1951). Small amounts of uranium can stimulate plant growth, but concentrations above a very low level can be retarding or toxic. Poison effects on germination can begin at 47.6 ppm. 476 ppm can wither leaves and roots; 1% U was toxic to germination (Cannon, 1951).

The availability of uranium to plants is influenced by soil properties and the degree of uranium binding in the soil. The elemental solubility of uranium affects

uranium's availability for plant uptake (Ibrahim and Whicker, 1992). Many of the factors that are important for plant uptake of uranium, such as pH, texture, organic matter, and CEC also control uranium sorption in the soil (Mortvedt, 1994).

The uranium accumulation in the plant relative to the uranium content of the soil is represented by the concentration ratio (CR), which is a measure of the effectiveness of phytoremediation.

(mean U concentration/ g dry vegetation)

(mean U concentration/ g dry, underlying soil)

(Ibrahim and Whicker, 1992). Previous CR data shows that plant uptake of uranium is not linearly related to soil concentration of uranium (Hossner et al, 1992; Ibrahim and Whicker, 1992; Mortvedt, 1994). The CR depends on the plant species, and the soil variables identified in the previous section. Concentration ratios were highest for plants growing on the edge of a tailings impoundment because "acidity [pH 2-5] and water availability tend to enhance the solubility and availability of radionuclides for plant uptake," or because of saturation conditions encouraging plant growth (Ibrahim, Whicker, 1992).

Desert vegetation of the Four Corners area was sampled for uranium content and Juniper, Indian Rice Grass, and a milkvetch (*Astragalus Preussii var. arctus*) were identified as uranium accumulators (Cannon, 1951). In Texas, range plants were grown in uranium mine overburden and adjacent soils (Hossner et al, 1992). Sand lovegrass was the best uranium accumulator with 4 ug/g. Greenhouse investigations of plants with uranium contaminated soil found little uranium uptake (Baumgartner et al., 2000, Meyer, Mclendon, Price, 1998).

Brassica rapa, a mustard plant, is "a model plant for U phytotoxicity because of its ability to produce seed even at high levels of U (10,000 mg/ kg) (Saric et al., 1995). Species in the Brassicaceae family (Mustards) have been shown to have the "...ability to hyperaccumulate heavy metals such as Zn, Pb, and Cd under natural conditions" (Huang et al, 1998).

METHODS

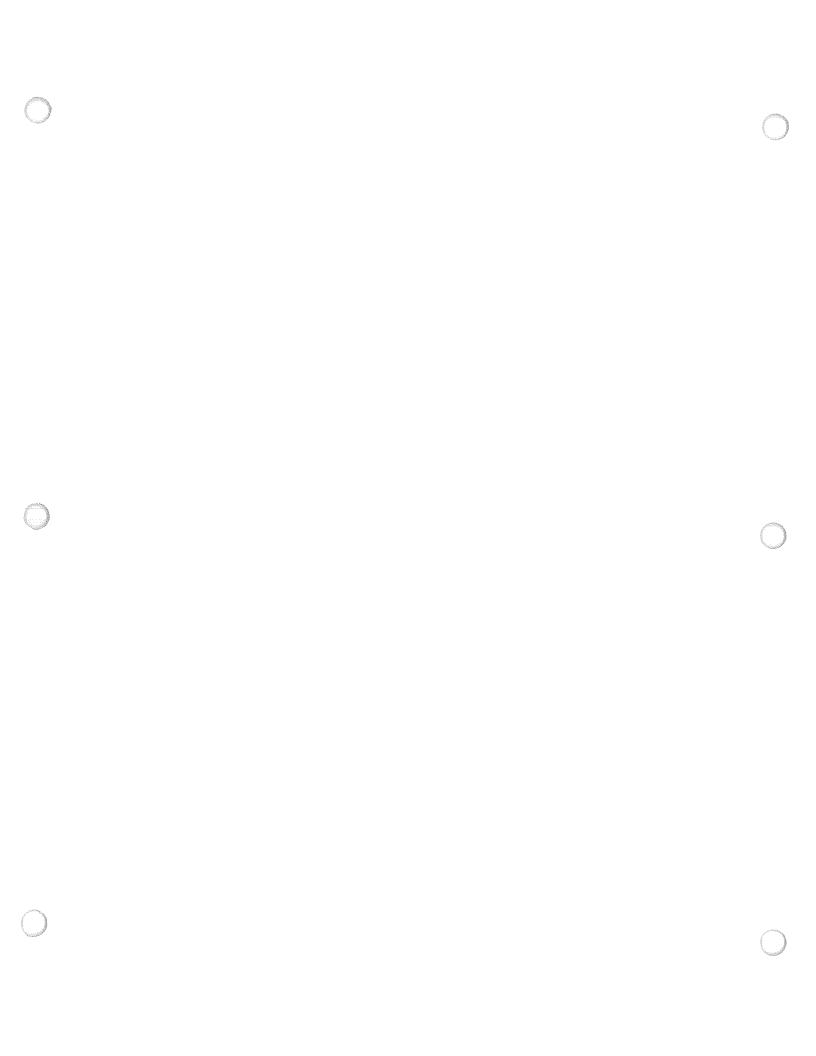
FIELD WORK

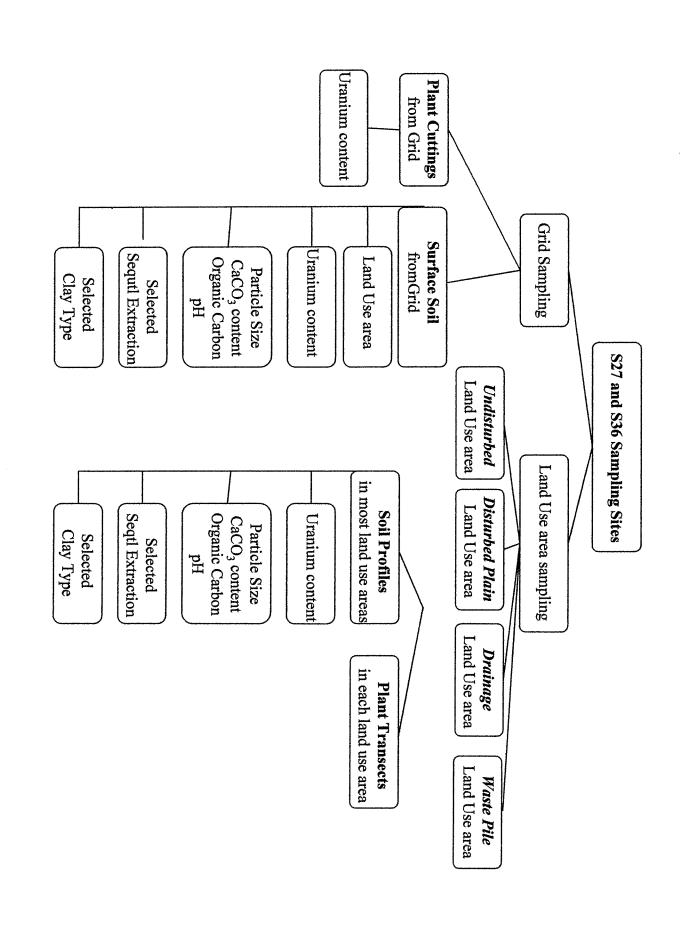
OVERVIEW

A grid was laid out over each area using a measuring tape and pace and compass mapping. Geomorphology, soil profile samples, geiger counter readings (urem/ hour), and GPS readings were described or measured at each point in this grid. Selected grid points were sampled for soil and vegetation. In the four designated land use types, plant transects were taken and soil profiles were sampled. Figure 16 details the grid and land use type sampling. These samples use the systematic and judgmental sample designs, as described in Table 1.

Approach	Relative Number	Relative	Basis of Selecting
	Of Samples	Bias	Sampling Sites
Judgmental	Smallest	Largest	Prior history, visual
			assessment of technical
			judgement
Systematic	Larger	Smaller	Consistent grid or pattern
Random	Largest	Smallest	Simple random selection

Table 1. Basic Sampling Approaches for Environmental Research and Assessment (Keith, 1991).





SAMPLING GRID

A reference grid was established every 50 m over the study area with a compass, measuring tape, and/or pacing. This helped to compare total area of land use types and map the landforms accurately. Once the grid was established, a GPS location was taken at each point flagged in the field. Based on this information, a large number of samples was anticipated, and the plant and soil sampling design was scaled down. Plant and 'surface' soil samples were taken at approximately every other point at S27, and 60% of the points at S36.

Section 27 Grid

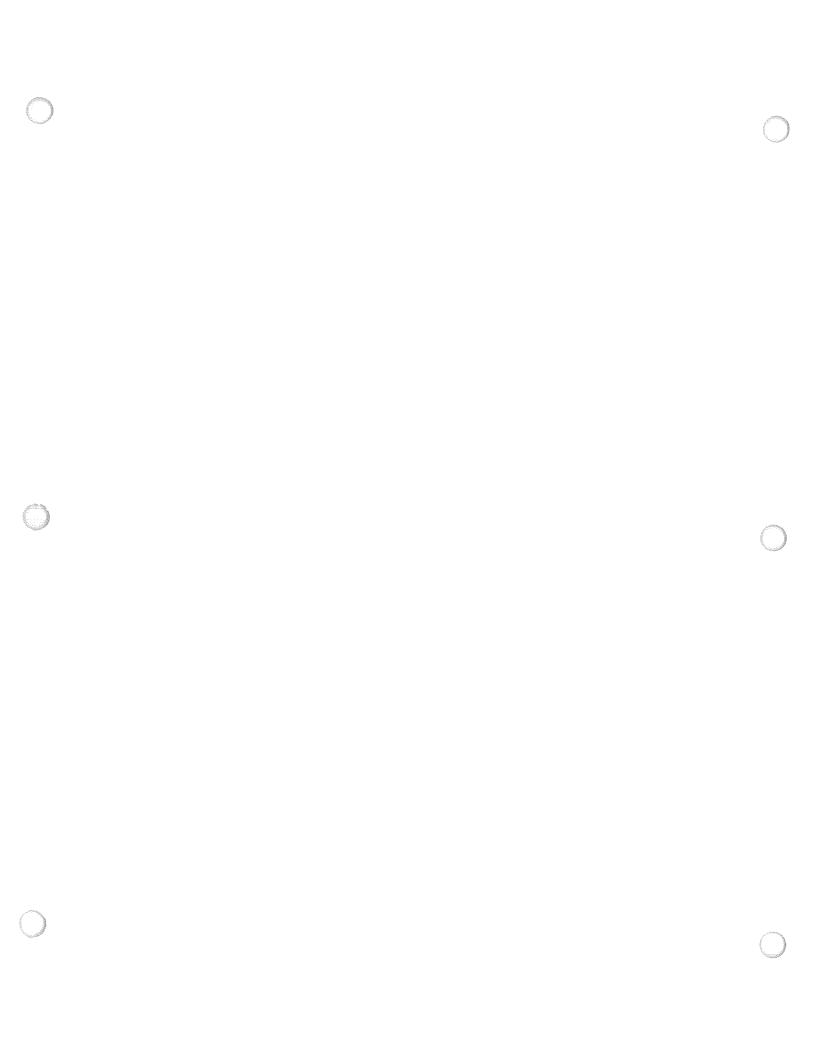
At S27, plant and soil samples were taken at 25 selected grid points in a checkerboard pattern. These 25 sampling points are shown in red on the following aerial photograph (Figure 17). An additional 73 GPS points were taken at the Section 27 mine to more accurately map the breaks in slope and drainage areas. These points were used in conjunction with the 63 initial grid points and the aerial photograph at section 27 to further map the area's land use areas: arroyo, waste pile, and disturbed plain.

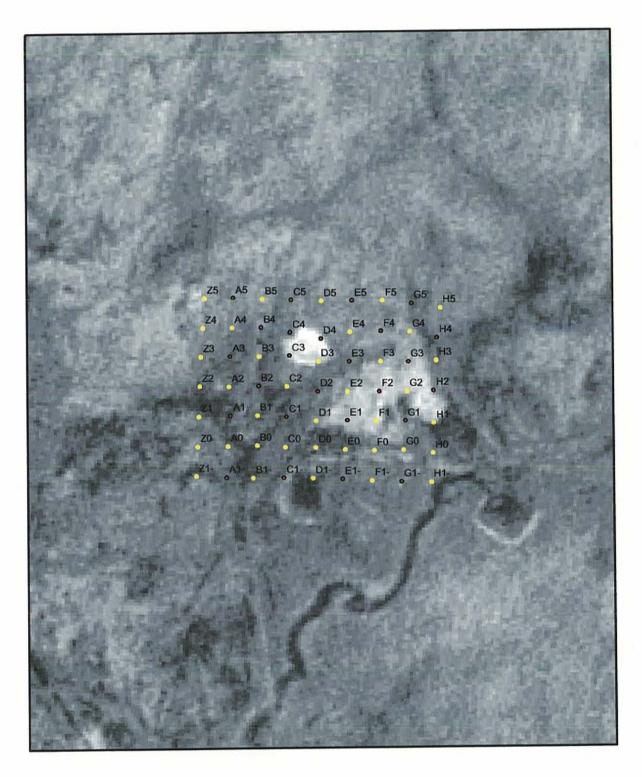
Section 36 Grid

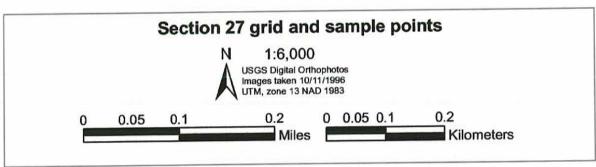
The section 36 mine had two waste piles, a large disturbed area, and a drainage area. A grid of approximately 600 x 200 m in 50-meter intervals was laid out at the site. 75 GPS points were taken, including all grid points and some topographic detail (Figure 18). Because of sample size considerations, samples were taken at 39 points in the 1, 2, 3 rows. Additional plant samples were taken along the top of the most contaminated waste pile.

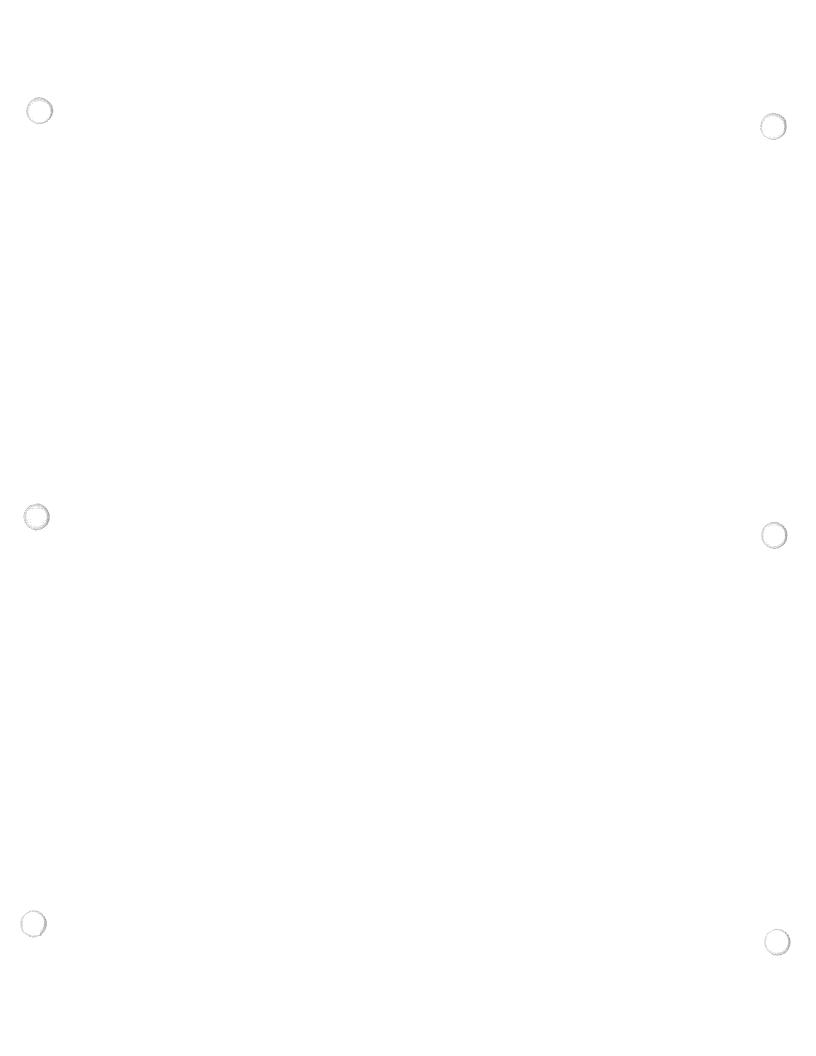
GPS Measurements

After the grid was established and marked with flagging, each point was GPS'd using a Garmin 12xls GPS unit. The GPS error (+/- 2-5 m) was typically higher than the measuring tape or paced measurement error (+/- 1-m). The original GPS points for this study use the UTM NAD 1983 datum. These plot correctly on a digital aerial photograph (rgis.unm.edu). For section 27, they correlate with the expected location, just north of an eastern-running dirt road. The coordinates were transformed to the NAD 1927 datum in order to be used on a topographic map. The points were converted from Nad 1983 to Nad 1927 using the ArcToolbox program.

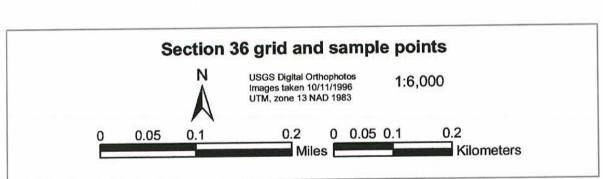












GRID POINT SAMPLING

Soil 'Surface' Sampling

At grid points, soil samples were taken at 0-5 cm depth, adjacent to the sampled plants. These are subsequently referred to as "surface" soil samples.

Plant Sampling

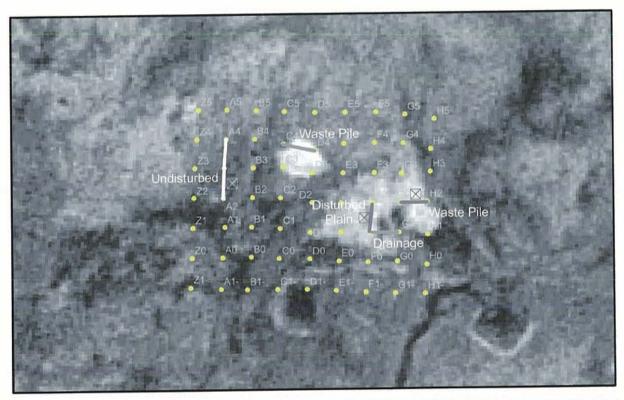
Plants were sampled above the soil surface at the grid points provided in figures 13 and 14. Three plants, those closest to the grid point, were sampled. Standard procedure was to cut these plants above the soil surface. A number of grid points had duplicate species samples.

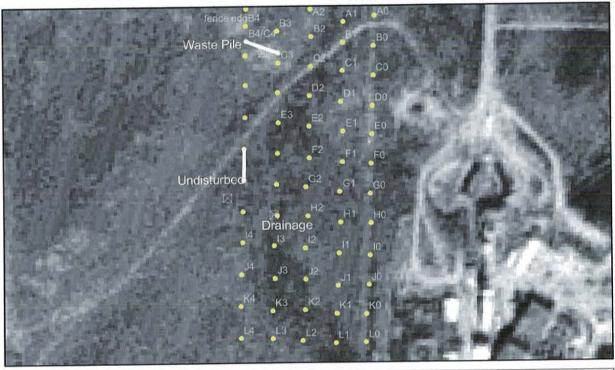
NON GRID POINT SAMPLING

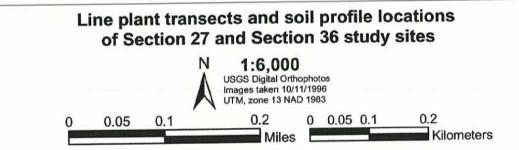
Soil Profiles

At S27 and S36, soil profile samples independent of the grid system were also taken (figure 19). These were taken to characterize the soils in the land use types: in the arroyo, waste pile, and undisturbed areas. This information was used to examine the possibility of uranium movement within the soil profile. At the section 27 mine site, soil profiles were sampled every five centimeters to 30 cm, considering uranium mobility and sample sizes. At the section 36, soil pits were dug deeper, in order to examine the soil profile at greater depths. In the S36 lowland, waste pile, and undisturbed areas, these soil pits are 60 cm deep, with samples taken every 10 cm.

In both locations, all soil pits were dug, measured and photographed. Soil horizons were identified, and soil samples taken in one 4 inch wide by 1 inch deep area at







each interval. Sampling was performed from the bottom up, in order to minimize contamination of subsequent samples.

Soil profile samples from both locations were analyzed for uranium content, pH, particle size, organic carbon, and calcium carbonate. Selected samples were analyzed for clay type and by sequential extraction for uranium partitioning between the soil fractions. These samples were selected based on high uranium values and land use location.

Plant Transects

In order to characterize the vegetation in the undisturbed areas, lowland drainage areas, and mine waste piles, vegetation transects were taken in the different land use areas at each site (figure 20). This method quantifies ground cover by species, and identifies the percent bare ground. No plants were "sampled" along these transects. These transects are a modified form of the Long Term Ecological Research (LTER) line vegetation transect (Loftin, 1999). The LTER method sums the total length of a 50-m measuring tape that is covered by each species of plant, bare ground, or litter, and gives relative percentages of each species' ground cover. Established reference grid points were used as the endpoints for the line transects. For that reason, Figure 19 showing the line transect locations uses the same reference grid as the previous diagrams.

Additional non-grid plant and soil sampling was done at the Poison Canyon study site, approximately 5-10 miles southeast of the other two sites. Because this sampling was exploratory and not done at the same scale, with designated land use types and a grid sampling system, this information is listed in Appendix E.

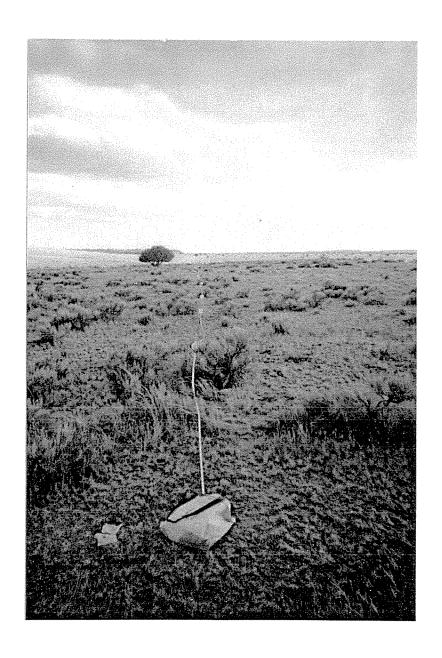


Figure 20. Plant transect along undisturbed section, Section 36.

LABORATORY METHODS

ICP-MS analysis was used to determine the uranium concentration of plant and soil samples. Soils 'surface' and profile soil samples were also analyzed for their particle size, organic carbon content, carbonate content, and pH. Certain soil samples were

selected for additional analyses based on land use area and uranium content. 10 soil samples were analyzed for clay type, and the uranium content of separate soil fractions was tested using 12 soil samples. For this sub-study the uranium bound in soils was separated into exchange sites, carbonate, oxides, organic, and residual fractions.

ICP-MS SAMPLE PREPARATION

The soils typically had a 1-5% moisture content, and were air dried in their sample bags. They were then sieved to <2mm. The >2mm gravels were weighed and set aside. The fine soil material was split for particle size, carbonate, organic carbon, pH, and uranium analyses.

Plant samples were air dried. After drying, a small section of the plant was removed from the total sample. For a grass, this was a few blades or a small clump from the rest of the grass plant; for a shrub it was typically a low branch, one that joins the stem close to the soil level. When the plant sampled had stems and leaves, the samples were split into leaf and stem samples. Grass samples were not split into stems and leaves. Tiny samples of small non-woody plants were taken as one sample and not divided into stems and leaves.

The stem and leaves were then separated into two piles. These were then held on wax paper and cut into <1 cm pieces. Any particulate matter generated during this process was removed. The ICP-MS plant subsample was then taken randomly from the prepared material for each sample. The prepared matter was generally > 4-10 X the sample size.

Microwave Digestion

Microwave digestions were conducted in a Milestone Plus Temperature Control scientific microwave oven with turntable, under pressure, in Teflon test tubes. Twelve samples at a time were prepared for ICP-MS analysis. These twelve samples usually included two of three quality control measures: a blank, a standard, or a sample duplicate. The temperature progression of a typical digestion is shown in Appendix H. The National Institute of Standards and Technology (NIST) reference material 8704, Buffalo River sediment, and 2709 San Joaquin soil, were used as reference soils. The NIST standard 1570a, trace element in spinach leaves, was used as reference plant matter. The content of these standards is listed in table 2. Trace metal grade chemicals were used in all NMT digestions and glassware cleaning procedures. These samples were prepared with nitric-acid cleansed glassware.

Element	BRS	stdev	<u>2709</u>	Stdev	2709 leach	Spinach	stdev
	%		%				
Ca	2.64	0.08	1.89	0.05	1.5	1.53	0.04
Fe	3.97	0.1	3.5	0.11	3		
Mg	1.2	0.02	1.51	0.05	1.4		
K	2	0.04	2.03	0.06	0.32	2.9	0.05
Na	0.55	0.015	1.16	0.03	0.068	1.82	0.04
	mg/kg		ug/g				
Pb	150	17	18.9	0.5	13		
Mn	544	21	538	17	470	75.9	1.9
Th	9.07	0.16				0.048	0.003
As			17.7	0.8	<20	0.068	0.01
Cu			34.6	0.7	32	12.2	0.6
Se			1.57	0.08	0.014	0.12	0.01
\mathbf{U}	3.09	0.13					
V	94.6	4	112	5	62	0.57	0.03
Zn	408	15	106	3	100	82	3
					**Extractionable fractions		

As and Se volatile elements and affected by gas losses. In dried soil, ~1% mass is lost.

Table 2. for Standards used in Microwave digestion and ICP-MS analysis.

Soil sample ICP-MS preparation

Soil samples were prepared following EPA standard method 3051. The oven-dried soils were split to approximately 0.2 gram and put into Teflon sample vessels. Under a fume hood, 10 ml of RO water, 8 ml of HNO₃, and 3 ml of HCl were added to the Teflon sample vessels. As each sample vessel was filled, it was capped. The twelve samples were pressurized at local atmospheric pressure, and microwaved at 210 degrees for 20 minutes. After the samples cooled to room temperature, they were filtered and diluted to 50-ml volume.

112 soil samples were processed by ICP-MS for total uranium and other elements.

This includes 66 surface soils and 46 soil profiles. Including duplicate samples, approximately 170 samples were run.

Plant Sample ICP-MS preparation

Plant samples were digested following EPA method 3052. This digests 0.4 g plant sample + 5 ml H₂0, 5 ml NO₃, 2 ml H₂O₂ in a pressurized vessel at 210 degrees for 20 minutes. After cooling, under a fume hood, the sample is depressurized, filtered and diluted to 50 ml volume. 171 individual plant samples from the two mine sites were prepared for the microwave digestion. Including laboratory duplicates, approximately 400 plant samples were prepared.

ICP-MS data

These samples were analyzed by an Agilent 7500i ICP-MS (Inductively Coupled Plasma-Mass Spectrometer) for total uranium concentration and other elements present.

Elements reported varied by analysis day, but included at different times Be, B, Na, Mg, Si, K, Ca, Ti, V, Cr, Mn, Co, Cu, Zn, Fe, Ni, As, Se, Sr, Mo, Ag, Cd, Sn, Sb, Ba, Hg, Ti, Pb, Th, U. This data is listed in the appendix. Including duplicates, >1000 samples were reported.

ICP-MS data was reported in ppb (ug/ L) solution. This was converted to ppm (mg/ kg) element of plant or soil matter by the calculation:

For the sequential extraction and early 2003 ICP-MS analyzed samples, residual standard deviation (RSD) values were reported for all elements. The ICP-MS measures each sample multiple times, and generates an average of these measurements for the reported sample value. The residual is the sum of deviations from a best-fit curve of all ICP-MS measurements of that sample. The residual represents the variance of these repeated measurements. A high RSD could mean that the sample that the sample reported poorly on the ICP-MS. If a sample had very little uranium, any variation would be exaggerated and the RSD becomes less useful. The RSD values were also used to identify the appropriate dilution.

The final data included elements Na, Mg, Si, K, Ca, V, Mn, Fe, Cu, Zn, As, Se, Pb, Th, U, and was prepared considering the uranium concentration, the sample dilution, and the RSD value. The specific steps used for preparing this data for analysis are listed in Appendix H.

SOIL ANALYSES

The fine soil material was split for particle size, carbonate, organic carbon, pH, and uranium analyses. Between samples, the splitter was cleaned using pressurized air, a bristle brush, kimwipes, and /or Ottawa sand. For all soil analyses except pH, the soils were oven dried for 24 hours at 105° C, and split again to obtain the exact weight for the procedure. pH soil samples were split from reserve air-dried samples.

Organic carbon

Organic carbon (OC) percent was determined by loss on ignition (LOI). Oven-dried soils are heated to 400° degrees C for 2 hours. This temperature burns off the organic carbon but not inorganic carbon. The weight difference was taken as the percent organic carbon (Rone, 2001). The LOI data presented in the results assumes that the weight loss of the samples is attributable to the total amount of OC present. It is calculated by the formula:

% LOI = ((sample weight before (g) -tin wt)- (sample weight after (g)- tin wt))*100 (sample weight before (g) - tin weight (g))

CaCO₃

The Chittick procedure was used to determine the amount of calcium carbonate in the soils (Machette, 1986). This procedure uses glacial (6N) hydrochloric acid to convert carbonate solid into carbon dioxide gas. The amount of hydrochloric acid added, and the amount of carbonate in the soil affect the amount of carbon dioxide gas generated by the procedure (figure 21). Taking into account the barometric pressure, and the volume of the generated gas, percent carbonate in the soil can be calculated: (Machette, 1986):

wt of carbon in CO₃ I correction factor from table: I
$$CO_2$$
 evolved I $\underline{.3866}$ I barom. pressure v. temp I $\underline{(ml)}$ I \underline{I} = y I sample wt (g)

This y value was then substituted into the equation y = mx+b where m and b were taken from a line generated by four daily carbonate standards. The final value x is given as the calcium carbonate content of the soil.

The Chittick method is typically calibrated to work for samples with 3% carbonate or above. In order to allow for these low carbonate values, lower value standards (1%, 5%) were used, as well as duplicates of most S27 and some S36 samples.

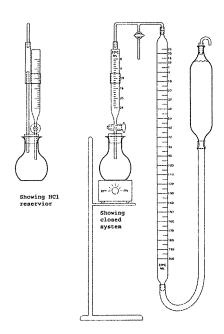


Figure 21. Chittick apparatus for measuring evolution of carbon dioxide gas from sample of soil carbonate (Machette, 1986).

Particle Size Distribution Analysis (PSDA)

Particle size was determined by removing the gravels (particles >2mm) from a sample, and then oven drying it. 20 grams of sample was added to a 250 ml Erlenmeyer

flask with 50 ml of 10% sodium pyrophosphate as a clay deflocculater. After at least 4 hours of shaking to disperse the clays, the sample was wet filtered to 63 um. The residue from this filtration was the sand fraction, which was dried and weighed. The < 63 um filtered sample was added to a 1200 ml settling tube and shaken for 45 seconds. At the appropriate settling interval, 20- 25 ml of clays in suspension were sampled at 10 cm depth, dried, and weighed. Additional clays were extracted in preparation for the clay type determination (Janitzky, 1986).

pH

Soil pH was obtained by dissolving an air-dried sample in a 1:1 reverse osmosis water solution and placing on a reciprocating shaker for 24 hours. The samples were then centrifuged and the pH of the clear liquid was taken at the Bureau of Geology's wet chemistry lab (Janitzky, 1986; SSSA, 2003).

Clay Mineralogy

Clay mineralogy was determined by x-ray diffraction analysis using a Rigaku D/Max II. Chris McKee of the NM Bureau of Geology conducted this analysis. The clay is suspended in water, then placed on a glass slide with an eyedropper, and allowed to dry. A more detailed method description is given in Appendix A. The analysis determined clay type with 10% error.

SEQUENTIAL EXTRACTION

The goal of this procedure was to identify uranium bound with different soil fractions: exchangeable, carbonate, Fe-Mn oxides, organic carbon, and residual metals (Tessler, Campbell, and Bisson, 1979). This procedure was conducted at NMSU's

Department of Agronomy & Horticulture Soil Chemistry lab, and is listed in detail in Appendix A. The procedure uses specifically targeted chemicals to extract the uranium bound to different soil fractions of the same soil sample (Ramos, 1994). For the first three steps, the chemical is added and the samples are agitated for one hour or more. The samples are then centrifuged and the supernatant is removed. Each of the first three steps is repeated to ensure the complete extraction of the associated metals. Tube, cap, and sample weights are necessary at each step to account for water and soil carryover between the tests.

The first step analyzed for exchangeable or soluble cations. 25 ml of 1 M magnesium chloride (MgCl₂) were added to each tube. The samples were shaken, centrifuged, and the supernatant solution poured off for uranium analysis.

Carbonate bound uranium was analyzed for next. 25 ml of 1 M sodium acetate (NaOAc; pH 5) was added to each sample. The sample was shaken and centrifuged, the pH was measured, and the supernatant fluid poured off for analysis.

In the third step, the oxide bound fraction was analyzed for with 25 ml of 0.4 M NH₂OH- HCl (in 25% acetic acid). The sample was again shaken and centrifuged, and the supernatant poured off for analysis.

The fourth fraction analyzed for the organic bound uranium. This used 5 ml of 0.1 M Nitric Acid (HNO₃), and then 1 ml of 30 % H₂O₂. These samples were left uncapped for several hours, and then another 1 ml of 30% H₂O₂ was added. After effervescence ended, the sample tubes were heated in a water bath at 50° C until bubbles disappeared. At this point 20 ml of DI water was added, the sample was centrifuged, and the resulting fluid was poured off for analysis.

The last fraction looked for any residual uranium in the soil. What was left of the original soil sample was washed into an aluminum container, dried and weighed. A total soil digest procedure was conducted that mirrored the above microwave soil digestion for ICP-MS analysis. All of these samples were then diluted 1:5 and run for uranium content on the NM Tech ICP-MS.

STATISTICS

This study aims to identify new uranium accumulating plants, and to identify the effects of semi-arid soils on uranium uptake in plants. Previous parts of this methods section identified land use type, soil uranium content, soil pH, texture, and OC and CaCO₃ content as well as plant uranium content as potentially important variables. Relationships between these variables can be meaningfully tested using correlation and linear regression.

CORRELATION ANALYSIS

Correlation assigns a number approaching 1 as the degree of linear relationship increases between two variables (Ramsey, Schafer, 2002). It does not identify independent or dependent variables. A correlation matrix can quickly be generated from a table of data, looking at every combination and identifying significant ones for further consideration. However, correlation analysis cannot account for nonlinear relationships, such as $y = x^2$.

In this study the final data included 15 elements and 7 soil properties. Correlation was used as a summary measure to suggest relationships between variables. At both

mine sites, pH, organic carbon, silt, clay, and land use have normally distributed data sets. Gravels, clay, and uranium data are skewed towards low numbers. In order to create a numerical relationship, land use types were ranked with respect to disturbance:

undisturbed	1
lowland/drainage	2
disturbed plain	3
waste pile	4

Correlation relationships are then further tested with regression analysis. The relationship between soil properties and uranium was tested in this way.

REGRESSION ANALYSIS

Regression analysis describes the distribution of values of one variable (the *response*) as a function of other *explanatory* variables (Ramsey, Schaefer, 2002). It defines a linear relationship where one variable is dependent upon, and can be predicted by other independent variables. Regressions can support inference about nonrandom relationships. It is a useful way of summarizing a relationship between variables that may be suggested but not conclusively obvious from a scatterplot of the data.

The significance of regression relationships is tested by the p-value and the r-squared value. The p-value tests the equation's ability to accurately account for all given data. The r-squared value is very useful for interpretation of regression equations. It quantifies the degree of variation of the response variable (for example, U) that can be predicted by the explanatory variables (for example, clay content and organic carbon). For example, the r-square value of an equation U = 2.3 + 0.79 OC - .33 clay % is 53 %. This suggests that 53% of the uranium concentration is explained by, or affected by, the soil organic carbon and soil clay content, taken together.

Simple regression looks at the influence of a single explanatory variable. Multiple regression models the response variable as a function of several explanatory variables (Ramsey, Schaefer, 2002). A 'Best Subsets' regression can be generated from multiple variables. This shows different combinations of explanatory variables as predictive equations of the same response variable, and each equation's significance and explanatory effectiveness. In a stepwise regression, the operator sets the variables to be considered. The program Minitab then determines which of the designated explanatory variables are significant, and generates an equation with the response variable.

Multiple regressions are used here to model relationships between the soil properties of interest (uranium concentration, depth, land use type) and other soil properties. Predictive equations (soil properties predicting uranium value) were then generated in the format y = b + mx1 + mx2 +, where y is the dependent variable. The dependent variable is the outcome to be explained in these regression analyses. Any change in the dependent variable is viewed as a function of changes in the independent variable.

RESULTS

LAND USE TYPES

LAND USE MAPS

Land use types were mapped in the field at the two major sampling locations. These maps were used to test the differences in soil properties and uranium distribution. The Section 27 sampling area covered a range of 2-8 points in each land use area, while the Section 36 grid sampling area covered 3-16 points in each land use area (Table 3).

Section	Undisturbed	Lowland	Disturbed plain	Waste pile	TOTAL
27	8	2	8	7	25
36	16	16	3	4	36

Table 3. Sampling Points by Land Use type

Figure 22 shows a view from atop the S27 waste pile looking east, viewing disturbed plain and unsurveyed, undisturbed land. Figures 23 and 24 show two land use areas of S36; the lowland area and the waste pile, as well as their soil profiles. The following figures (figures 25 and 26) map out the S27 and S36 land use types. First the

following figures (figures 25 and 26) map out the S27 and S36 land use types. First the land use types are presented, and in Figures 25b and 26b the land use types are overlain on aerial photographs.



Figure 22. Waste pile and undisturbed area, looking west, S27.

Stars on figures 25 and 26 show the sampling points overlain on the grid pattern and the aerial photographs of each sampling site. These photos (figures 25b, 26b) show the higher vegetation and less bare ground of the lowland land areas, and the slightly lighter undisturbed areas. The waste pile and disturbed plain land use area have more bare ground and lower percent vegetation cover. On Figure 25b, showing Section 27, the difference between the disturbed plains and waste piles versus the lowland and undisturbed areas is shown in the darker color of the latter areas. On Figure 26b,

showing Section 36, the differences between land use types are less obvious on the aerial photos. The lowland area still has more vegetation and ground surface cover, resulting in a darker photo of that area. The waste pile, current road through the area, and current Uranium milling operations to the east of the photo all have less vegetative cover and thus more albedo on the aerial photo.

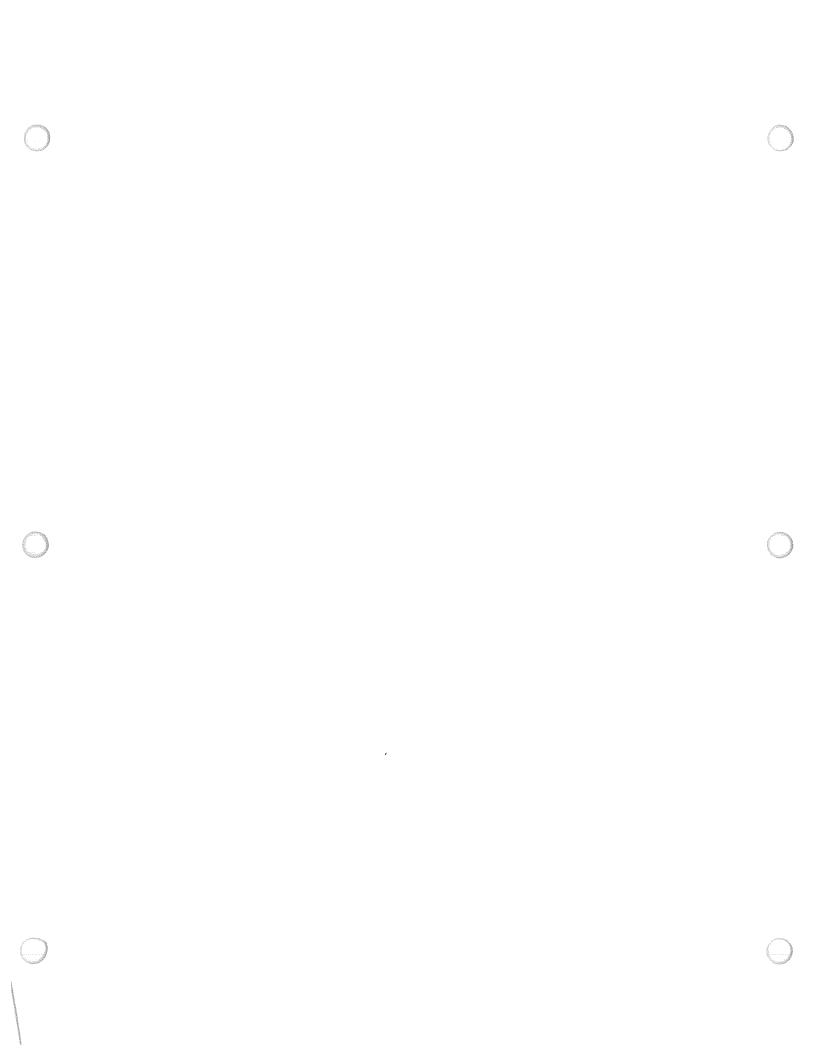


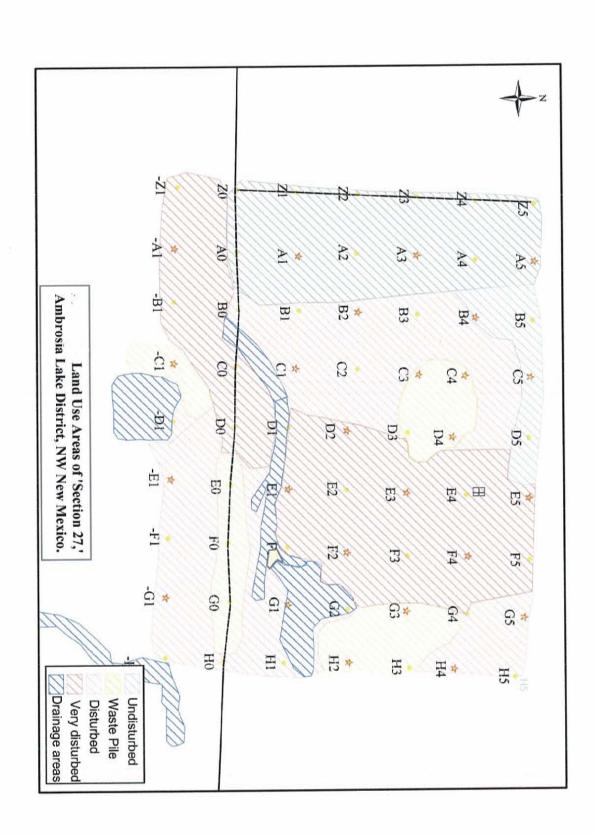
Figure 23. S36 northern end of lowland area and lowland soil profile.

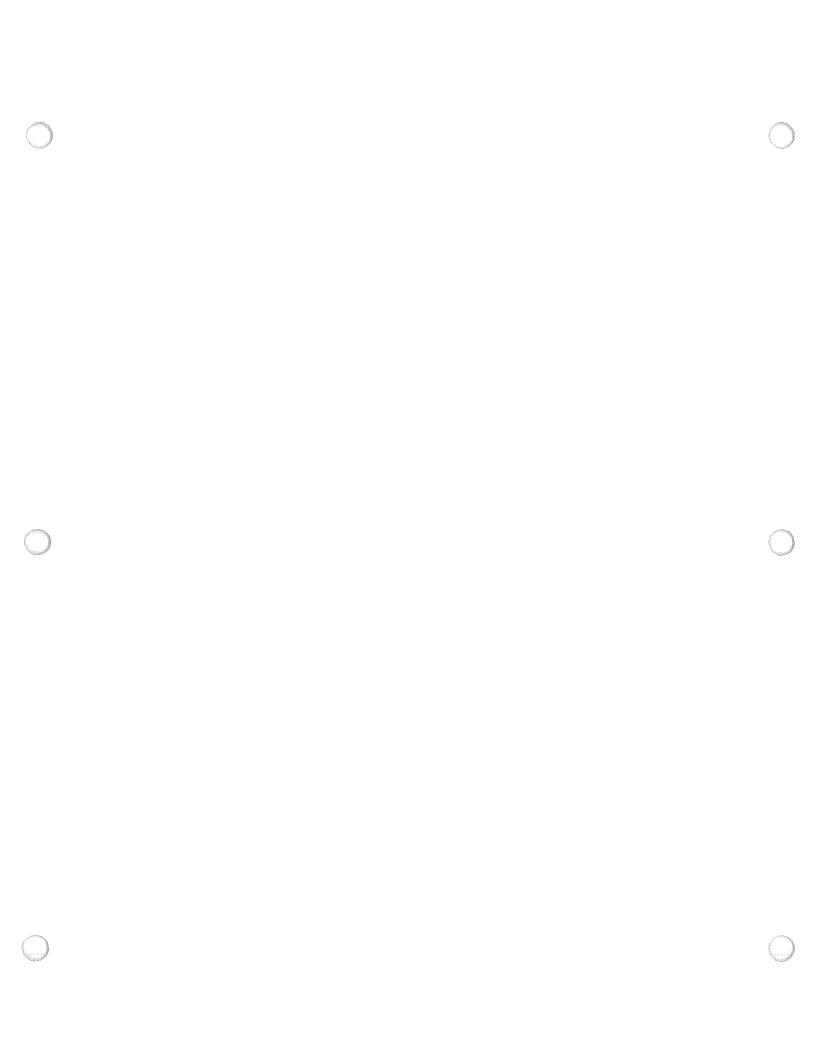


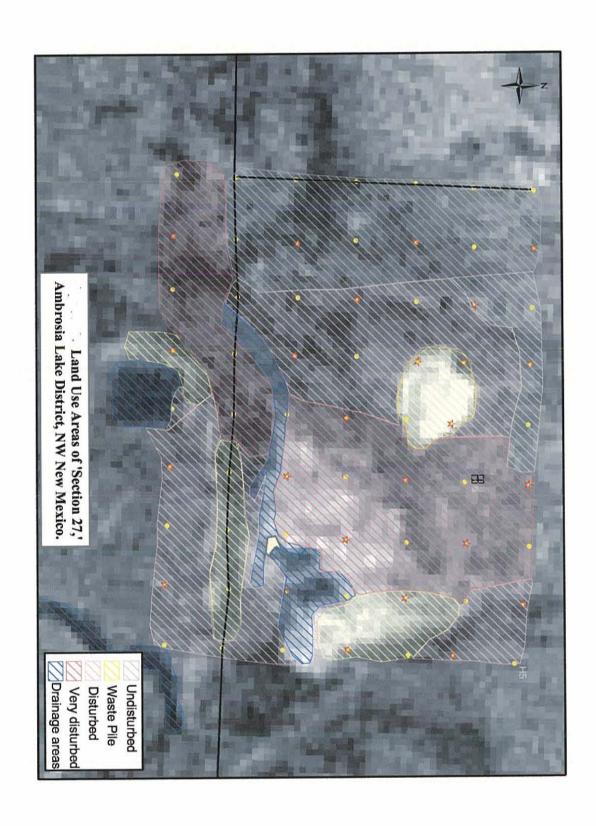


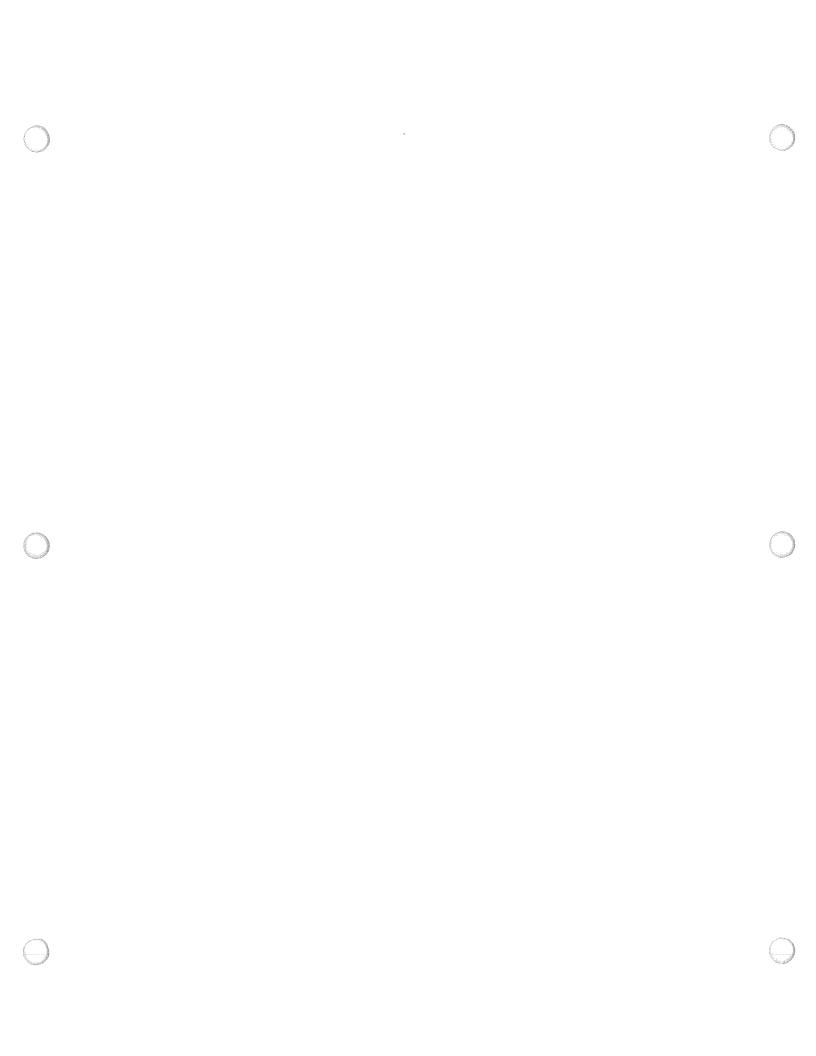
Figure 24. S36 Waste pile and soil profile.

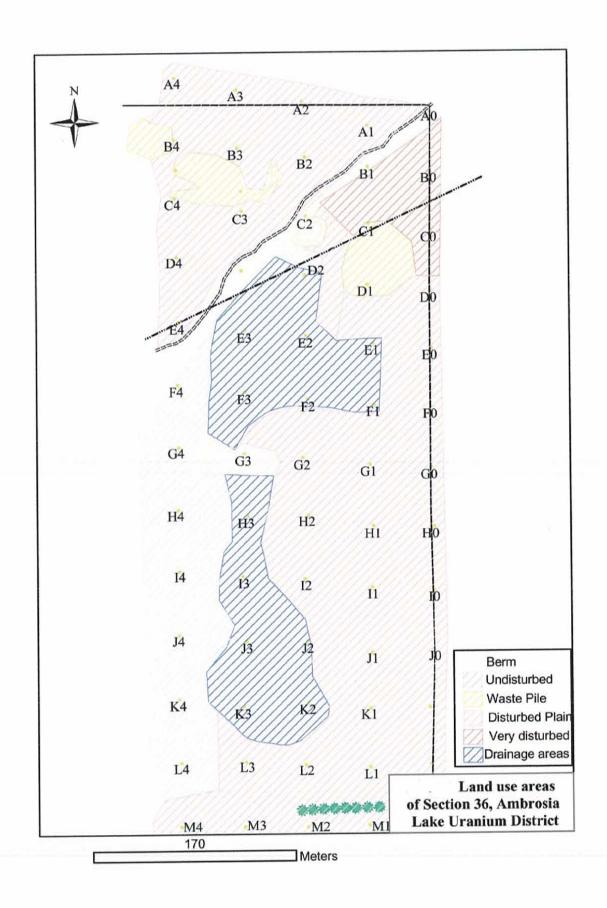












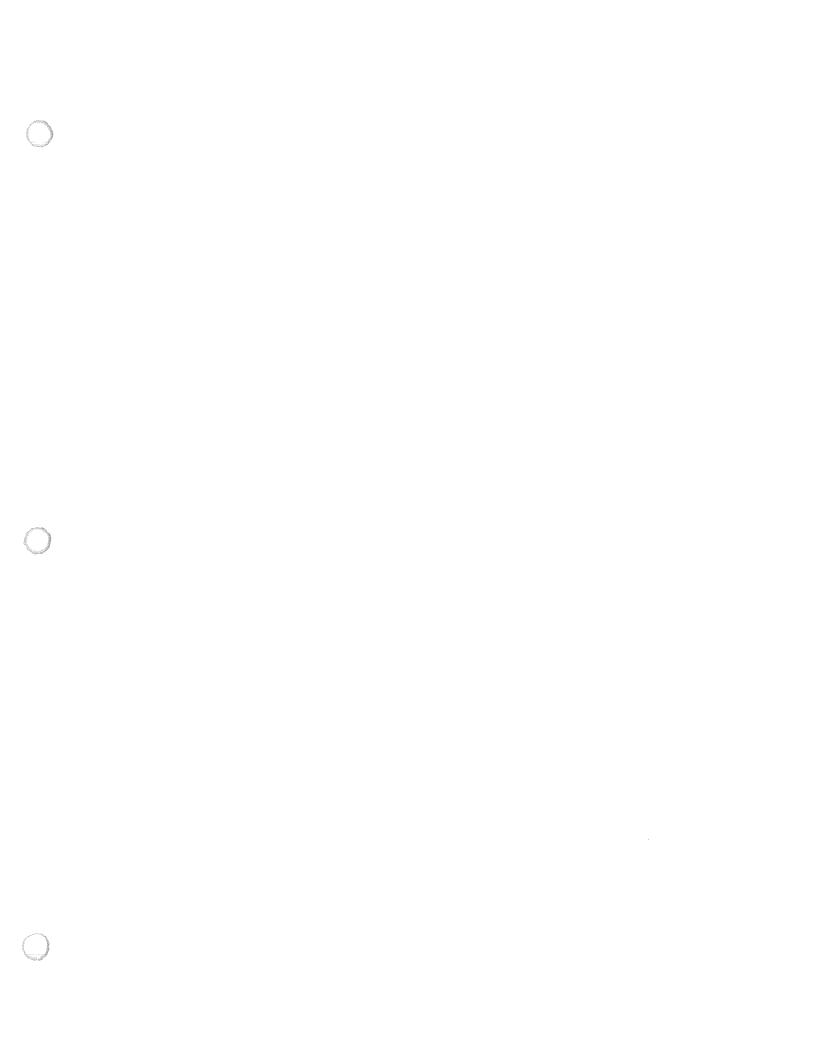
At Section 36, the presence of kaolinite suggests a highly weathered environment; however the presence of illite and mixed layered clays at this site also documents some resistant material (Birkeland, 1999). While the soils here have in general less kaolinite than S27, there is almost no smectite, meaning that the CEC is greatly reduced. Because both sites contain clay minerals with low CEC, other methods of uranyl sorption, such as organic matter, may take on increased relative importance in the soil.

Section 36 Surface	<u>Illite</u>	<u>Kaolinite</u>	<u>Smectite</u>	Mixed Layered Clays
Drainage	25	75	negl	Negl
Disturbed Plain	25	75	negl	Negl
Waste Pile	~2.5	80	~2.5	~15

Table 6. Section 36 Surface clay mineralogy, estimated at 10% per Chris McKee and duplicate samples.

pH

Soil pH varied very little at either site, S27 or S36. The range of pH values at S27 was ~7.6-8.1. The range of pH values at S36 was ~ 7.4-8.0. At both locations, the undisturbed land use areas (marginally) had the highest pH. The drainage areas at both locations were relatively intermediate, and the disturbed plain and waste pile locations had the lowest pHs. All of the average pH values between land use types had standard deviations large enough to suggest that there is no significant variation between land use type (figure 30).



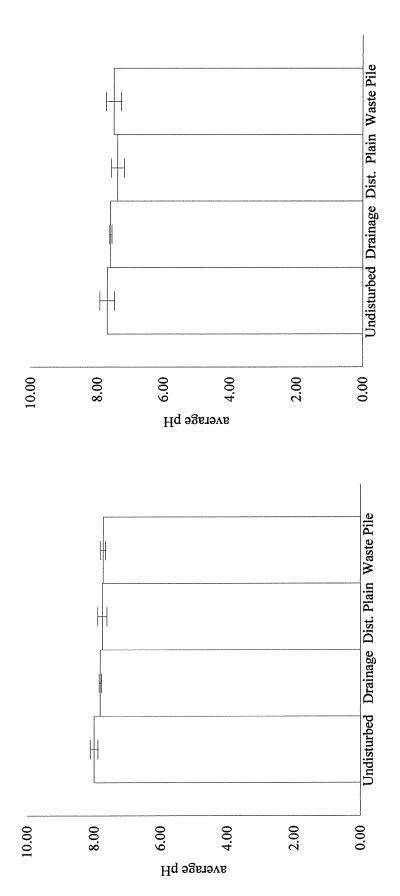


Figure 30b. S36 surface soil pH, averaged by Land Use type Figure 30a. S27 0-5 cm soil pH, averaged by Land Use type

Surface Soil Uranium Samples

S27

Very little difference can be seen in the surface soil uranium values of the undisturbed, drainage, and waste pile land use areas. Average surface soil uranium differentiated the disturbed plain by 120 ppm. However, this large difference was captured in 25% (2) of the sample points in the disturbed plain area (8 total). The only difference of these two point is in their uranium value (Figure 31a). However, the variability of the uranium concentration of the disturbed plain land use type can be seen in its' low average value when those two points are excluded:

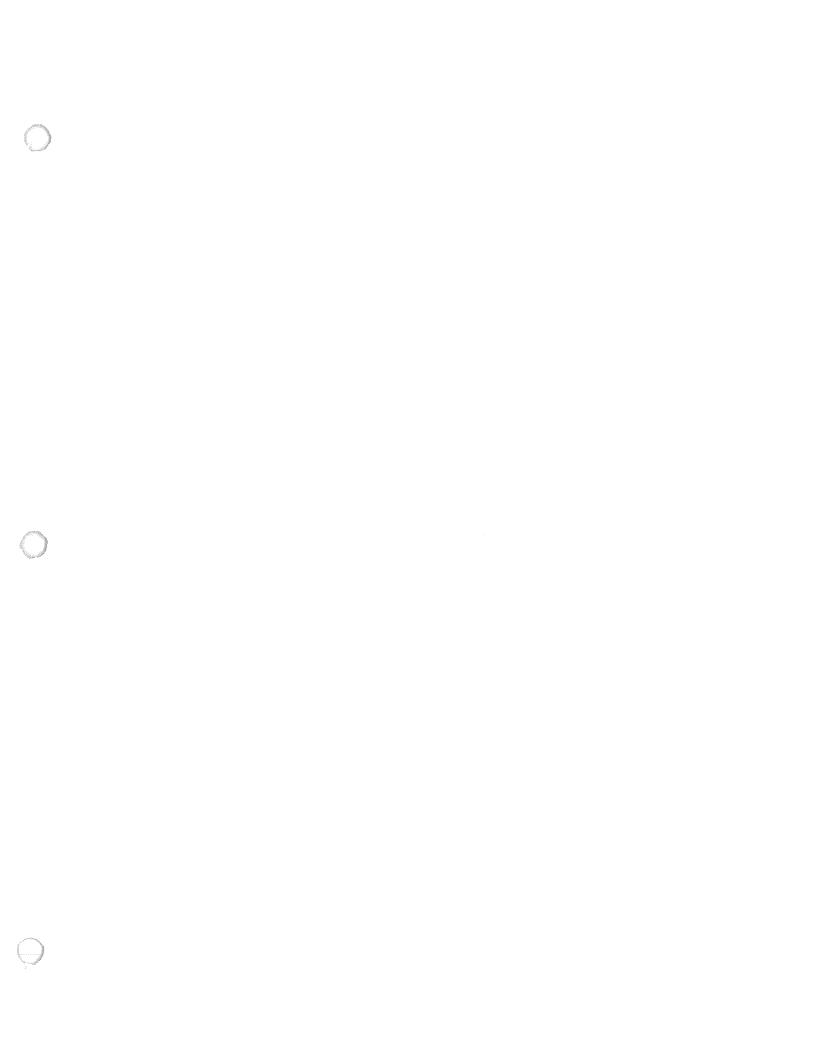
All S27 surface	pts	S27	surface	excl.	F2,	D4

Land Use	U avg	U stdev	U avg	U stdev
Undisturbed	61.37	62.6		
Drainage	73.77	92.88		
Dist Plain	253.12	393.43	31.73	26.08
Waste Pile	78.71	59.66		

Table 7. S27 Surface soil uranium value, averaged by land use type.

S36

Overall surface soil uranium content was much lower than section 27 in section 36. While S27 did not have obvious differences between the land use types in surface soil uranium content, in S36 the undisturbed and drainage soils have soil uranium content more than one standard deviation lower than the soil uranium content of the disturbed plain and waste pile surface soils. All of this uranium content is very low, below 15 ppm (figure 31b).



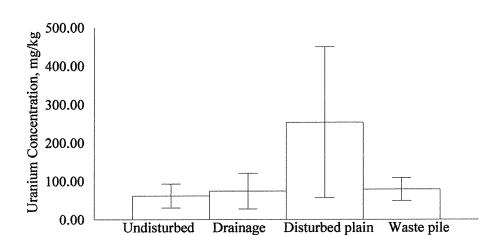


Figure 31a. S27 0-5 cm soil Uranium averaged by Land Use

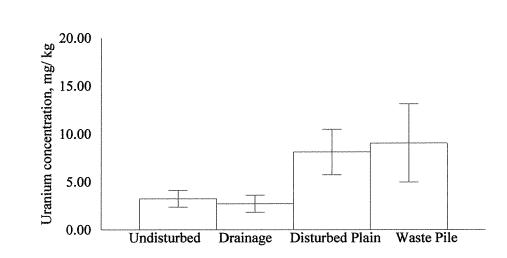


Figure 31b. S36 0-5 cm soil Uranium averaged by Land Use

Surface Soil Uranium measurement

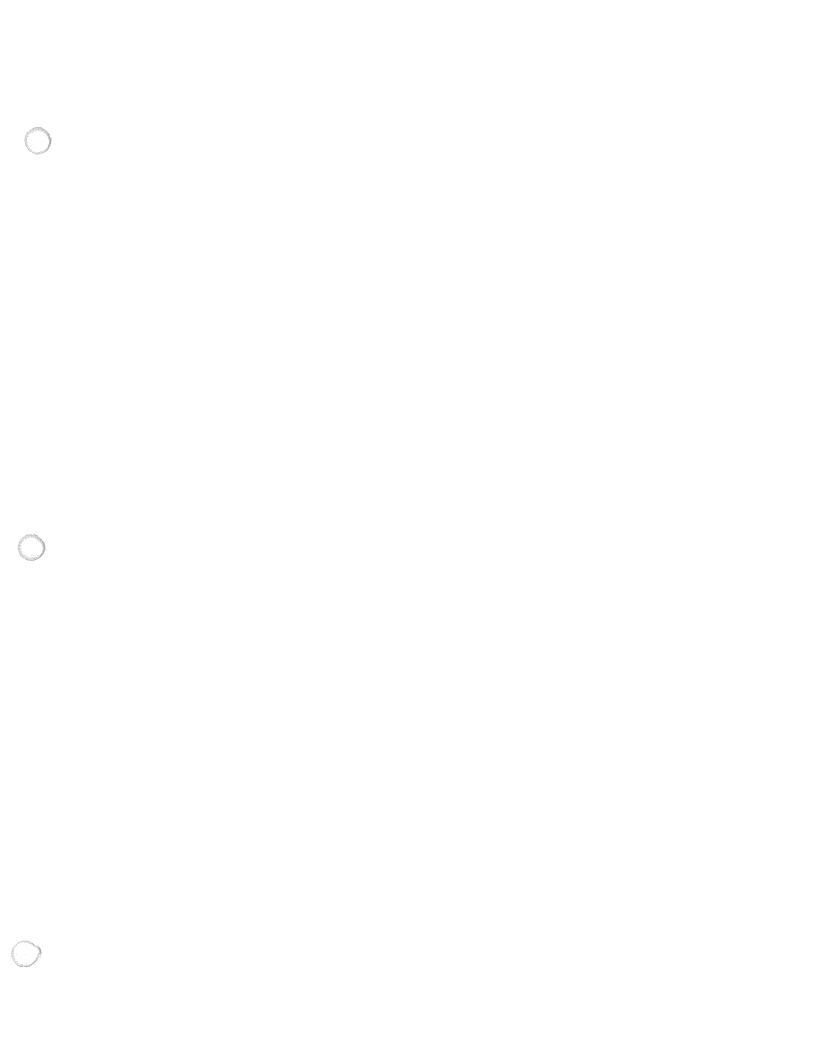
Surface soil uranium concentrations were originally measured with a gamma ray meter. These measurements helped define the uranium concentrations in the field, and varied from 0~1500 uRem/ hr. Surface soil uranium concentrations by ICP-MS analysis varied from 0-1050 ppm. These uranium concentrations did not correlate in all cases with the gamma ray readings, primarily at the S36 site, which only had high gamma ray readings on top of the waste pile, and nowhere else. The waste pile soil profile later had a ICP-MS uranium concentration of 47.6 ppm. The surface soil uranium (ppm) at S36 shows high uranium readings at 3 locations (approximately 20 ppm).

Uranium is primarily mined for the low-concentration isotope U-238. This isotope is the main source of gamma rays. U-235 and U-234 constitute ~95% of naturally occurring uranium ore. They do not emit gamma rays. For this reason concentrations of uranium -235, and U-234 in the soil may not be accurately measured by a gamma ray meter. All uranium isotopes are important targets for soil remediation. The S36 waste pile may have had more mine tailings and U-238, which is why it had a high gamma ray reading. Less disturbed locations that may have been contaminated by windblown dust from an adjacent processing facility did not have elevated gamma ray readings, perhaps because the soil contained different relative concentrations of uranium isotopes. This could have been caused by wind-blown uranium dust, possibly from the nearby processing facility. Because of these concerns, the ICP-MS uranium concentration information is used when analyzing the surface contours of uranium concentrations for both the S27 and the S36 study sites.

Contour maps of the ICP-MS uranium values were made to further examine the surface distribution of uranium. These contour maps, in both locations, did not help to distinguish between the four land use types. For simplicity, the contour maps of uranium concentration are presented here without additional overlays. Both contour maps are oriented north in the upper left-hand corner, and are plotted using the same 50-m separated grid points as figures 25 and 26.

At S27, the disturbed plain is in the west-central and southeast portions of the grid. The undisturbed area is around the edges of the grid, and the waste piles also in the west-central and southeast portions of the grid. Considering this land use information, the S27 contours on figure 32 can help distinguish the disturbed plain land use type and not the three other types.

At S36, the central portion of the grid is drainage area. Disturbed plain is primarily in the northern part of the grid, with the waste pile central in the northern grid. The undisturbed portion is along the west side of the study area. In the S36 contour map, the contours do not match closely to any land use type (Figure 33).



Please Note contar maps are onited Never suffer file up t point on older suffer software on laptop! in

SOIL PROFILE ANALYSES

Organic matter

S27

The S27 soil profiles varied by land use type in their organic carbon content. The undisturbed soil had 3-4% organic carbon, which did not change significantly with depth (figure 34). The disturbed plain and waste pile profiles had less than 1% organic carbon throughout their soil profiles.

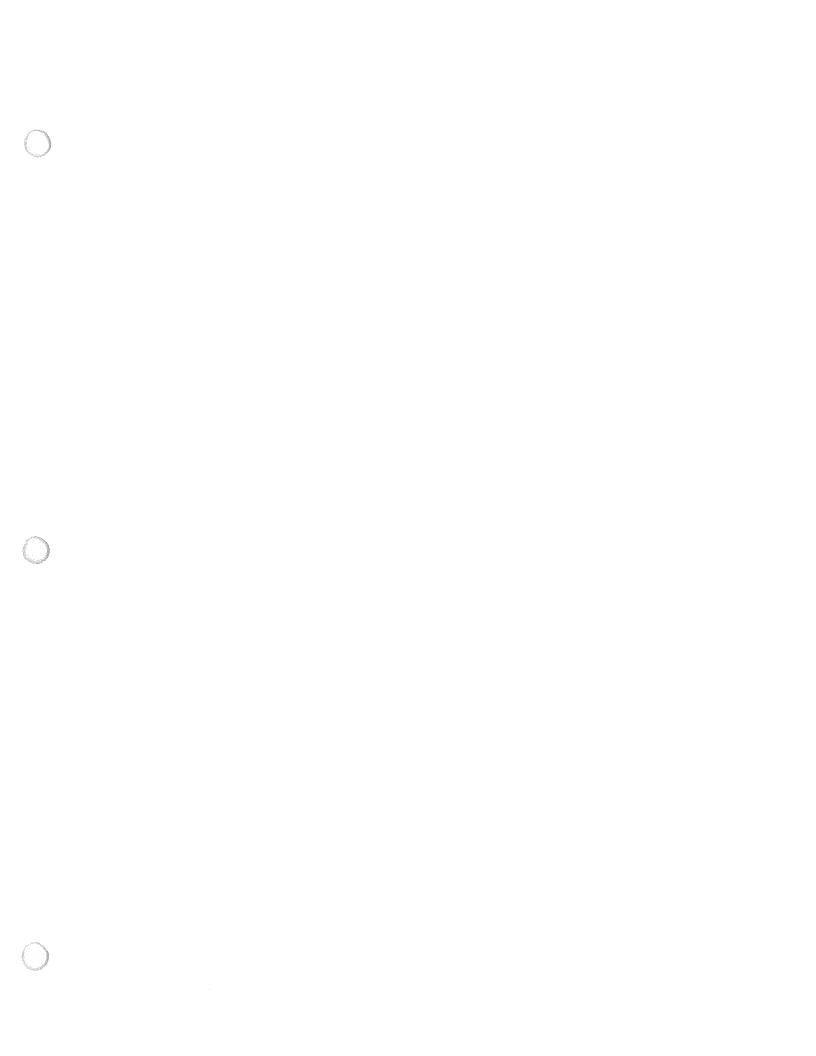
S36

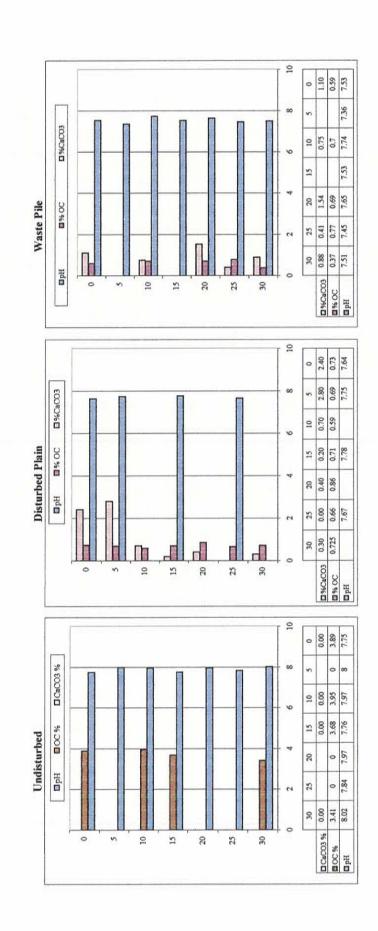
The S36 soil profiles varied by land use type in their organic carbon content. Here, in contrast to S27, the undisturbed profile had the least organic carbon, 2% or less throughout the profile (figure 35). In the drainage land use type soil profile, OC was very high at the top of the profile (8%) and decreased to 3.7 % at 70 cm. The waste pile land use type soil profile had organic carbon increase with depth to 3% at 70 cm. In the top 30 cm the waste pile profile had < 2% organic carbon. Study area S36 could have had more water available to develop the drainage land use type soil profile. The waste pile soil profile organic carbon at depth is probably affected by the tailings layers at 60-70 cm.

Calcium Carbonate

S27

The S27 soil profiles contained very little carbonate. The disturbed plain had up to 2.8% in the surface layers. However, because the overall content of these profiles was so small, there are no significant differences between the profiles (figure 34).





S36

The S36 soil profiles contained up to 3.3% calcium carbonate (figure 35). This is also very little carbonate, although it is slightly higher than the carbonate at S27. The undisturbed profiles had carbonate above 3% in the bottom three layers. These depths were not sampled at S27. This suggests a small amount of soil development at both sites. Again, these carbonate contents are very small and it is difficult to draw major conclusions from these minor variations in carbonate content.

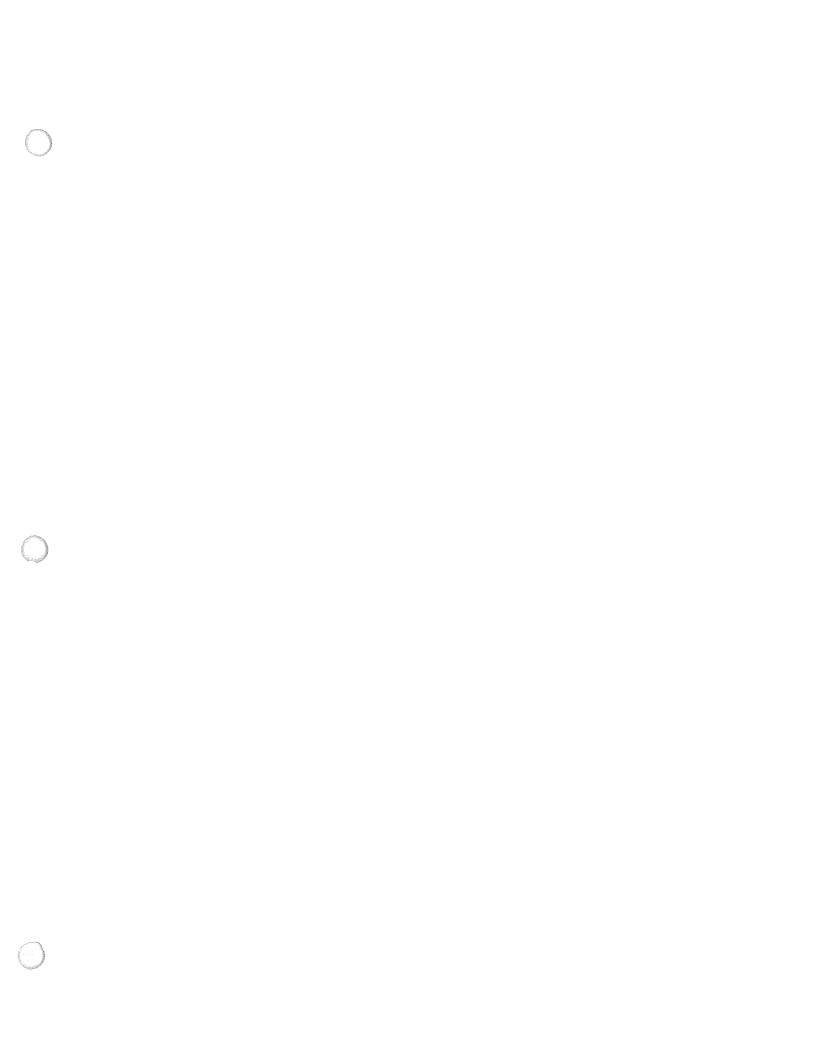
pH

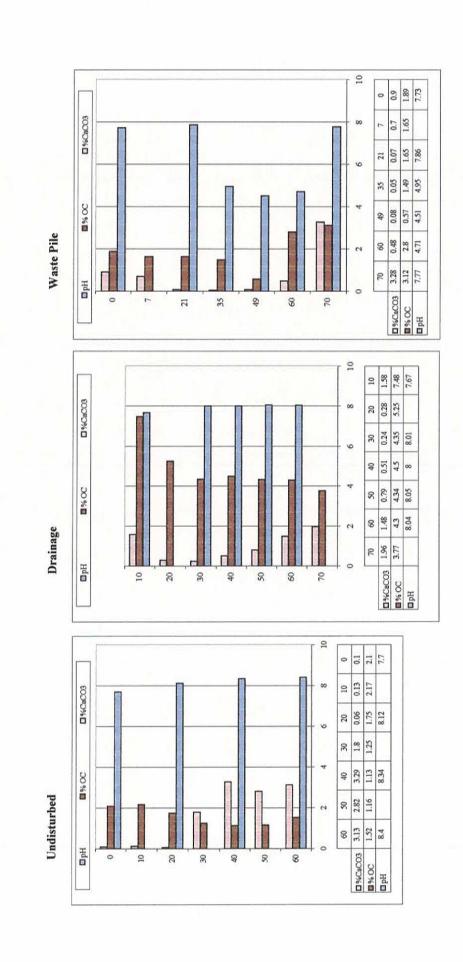
S27

The pH content of the S27 soil profiles also had very slight differences between the land use types' soil profiles (figure 32). The undisturbed profile had 4/7 samples near pH 8; the disturbed plain had an average pH 7.7; and the waste pile soil profile had 6/7 samples near pH 7.5. The small variations in pH are probably due to the relative soil development and parent material differences of these three soil profiles. In this case, the undisturbed soil would be slightly more developed, as its pH is slightly higher and the soil profile has been left under stable condition for a longer period of time.

S36

The pH content of the S36 soil profiles had very minor variations, similar to the S27 soil profile pHs (figure 33). However, the S36 pH variations also had the same slight decreasing-with-disturbance trend as the S27 soil profiles. The S36 undisturbed soil profile pH increased with depth to pH 8.4 at 60 cm. The S36 drainage soil profile had pH 8 with the 30-60 cm soils. The S36 waste pile soil profile had very low pHs at 35-60 cm





(pH 4.5-5). This is probably due to the buried tailings layer at 60 cm depth in the S36 waste pile. The slight increasing-with-disturbance trend in pH probably also reflects the relative age of these soils. The undisturbed is the oldest, the drainage soil profile younger, and the waste pile definitely less than 100 years old.

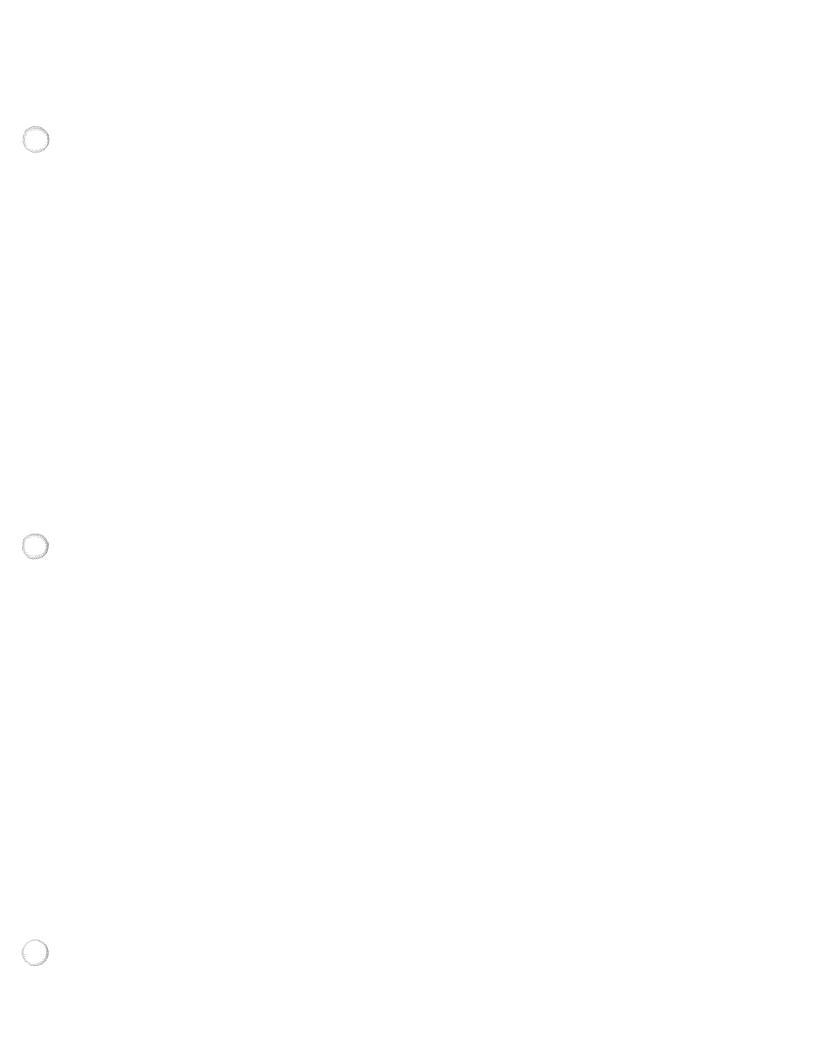
Particle Size Distribution Analysis

S27

At S27, the undisturbed soil profile is distinct from the other two soil profiles (figure 36). The disturbed plain and waste pile soil profiles are defined by their high sand content (approximately 80% sand). This sand is most likely a byproduct of mining the uranium from a sandstone ore. The undisturbed profile has almost equal amounts of silt and clay (38- 48% each) and less than 20% sand. Clay and silt presence in the undisturbed profile show the effects of weathering and eolian transport on the undisturbed soil profile development.

S36

The S36 soil profile particle size values vary between land use types (figure 37). The drainage soil profile texture is very different from the undisturbed and waste pile soil profiles' soil textures. While the waste pile and undisturbed soil are predominated by sand (55-87%), the drainage soil profile has 33-79% silt. The waste pile also has significant amounts of clay that increase with depth. The difference between the undisturbed and drainage soils could be attributed to the variability of soil formation across a landscape (catena), and the effects of soil formation in a small natural drainage with additional water.



nth												
mehrm	Gravel	Sand	Silt	Clay	Gravel	Sand	Silt	Clay	Gravel	Sand	Silt	Clay
0	13.38	15.84	-	-	5.26	76.57	10.78	12.65	14.96	79.5	11.6	8 93
2	0.57				15.25				7.47			
9	3.59	12.75	39.75	47.3	19.24	80.49	11.8	7.71	7.83	82.3	10.61	7.09
15	2.75				16				8.76			
20	0.27	12.95	38.31	48.94	22.77	65.9	10.27	23.84	10.24	75.45	13.36	11.19
2	0				20.3				29.61			
٥	24.56	10.83	39.63	44.53	11.93	79.62	10.1	10.28	10.93	78.06	12.41	9.53
	ve.ng % ■	□% gravels ■% sand □% silt □% clay	d 🗆% silt 🗅	1% clay	■% gravels	vels 18% sand	□% silt	□% clay	■ % gravels	pues %	%D #5%D	O % class
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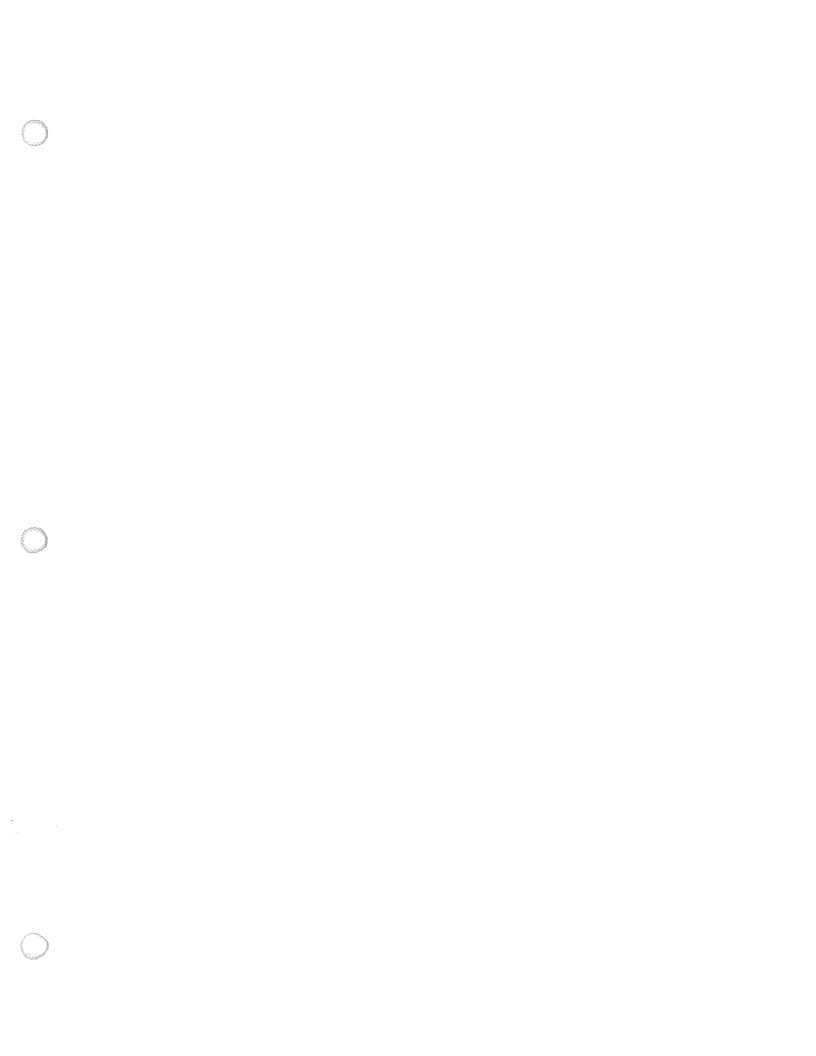
The uppermost part of the soil horizons of the undisturbed and waste pile soil profiles appear very similar in texture. However, this similarity of the waste pile and undisturbed profiles does not continue at depth. The waste pile has a well defined, deep red-brown, fine-grained and high uranium layer at 60 cm depth. This is probably buried mine tailings. At this depth, the waste pile soil profile's sand content drops >37%, and the gravel content increases 4%. The undisturbed layer reduces its sand content by approximately 17% at 60 cm depth, which does not match the change in the waste pile soil profile at that depth.

It is possible that the shallow soil horizons of the waste pile are composed of surface soils removed from an adjacent area, and used to bury the tailings layer. This could help explain some of the similarities in texture between the undisturbed and waste pile soil profiles at S36.

Clay Mineralogy

S27

At S27, the disturbed plain soil profile was selected for clay mineralogy analysis based on its high uranium content (figure 38). This profile contains mainly kaolinite, at the surface and at 30 cm depth. For a < 40 ya soil, it is very weathered. There is slightly more weathering with a small smectite increase at 30 cm depth.



	Clav	8.17	9.85	10.35		9.47	4.95	12,91	19.68	O% clay
le	HIS	13.63	15.62	15.65		14.68	7.92	37.68	46.83	alite 940
Waste Pile	Sand	78.2	74.53	74	9	75.85	87.13 49.41 33.49	19% gravels 19% sand		
	Gravel	=	1.48	1.53		1.86	0.79	3.08	7.77	
	WP depth	0	7	21		35	20	09	70	
3K	Clav	1	18.15	31.89	ı	24.2	3.86	35.23	49.98	clay
DIAMAGE	Silt	i	47.79	46.19	1	57.85	79.18	49.4	33.21	O % wilt O % clay
3-1	Sand	Î	34.06	21.92	1	17.95	16.96	15.37	18.91	% gavels 8% sand
	Gravel	ı	3.41	5.94	6.38	7.41	6.33	7.53	6.55	
	Clay	15.1	13.51	13.22	12.58	12.52	14.14	15.67		19% c.lay
peq	Silt	21.33	16.55	14.78	15.47	11.04	14.09	29.74		2% gravels © % sand 0 % sit 0 % clay
Undisturbed	Sand	63.57	\$6.95	72	71.95	76.44	71.76	54.59		Travels 9 % sa
	Gravel	1.63	2.23	2.17	1.79	1.46	1.53	1.96		
Land Use	depth	0	10	20	30	40	90	09	70	

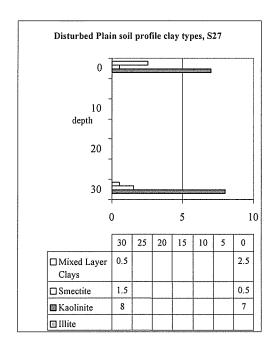


Figure 38. Clay Mineralogy of the S27 Disturbed plain soil profile.

S36

The S36 waste pile soil profile was selected for clay mineralogy analysis based on its relatively high uranium content. The clay mineralogy of this soil profile is predominantly kaolinite (Figure 39). There is a slight increase in illite, a 2:1 layer clay,

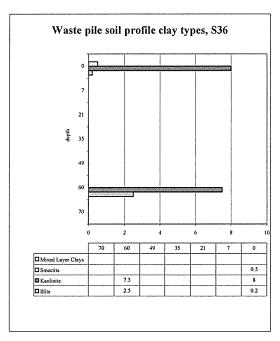


Figure 39. Clay mineralogy of the S36 Waste Pile soil profile.

at 60 cm depth. This corresponds with a marked increase of uranium (200 ppm) at this depth.

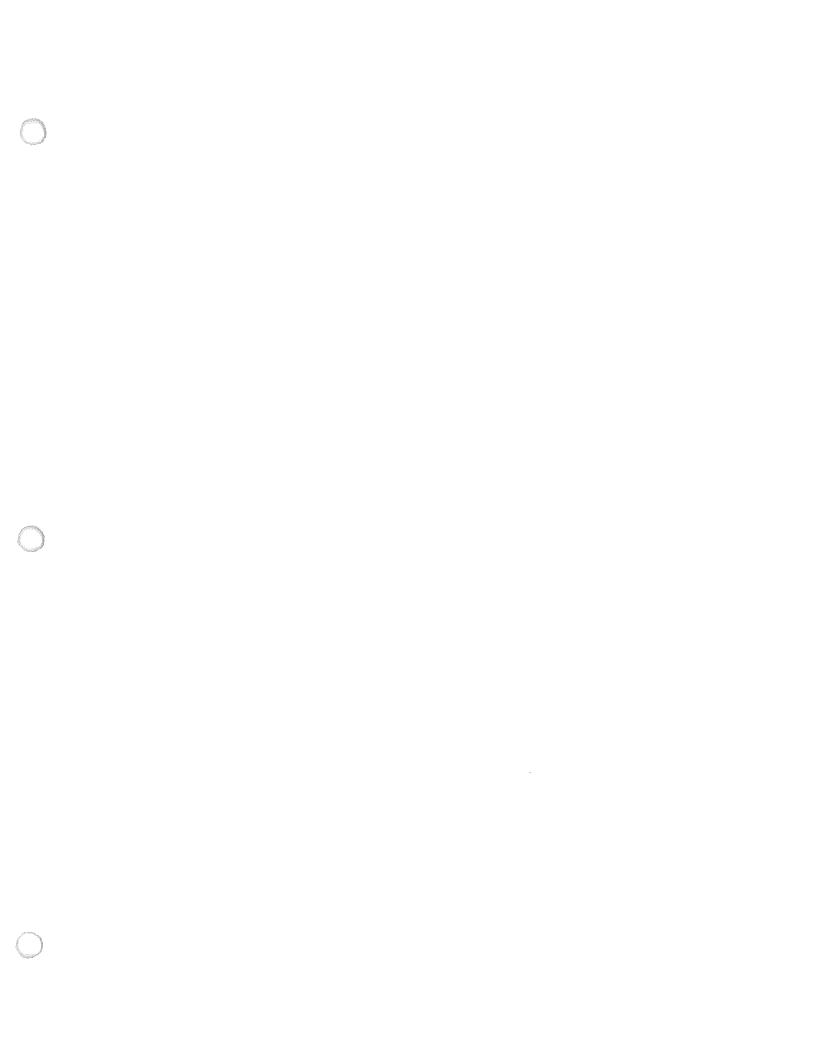
Soil profile uranium data

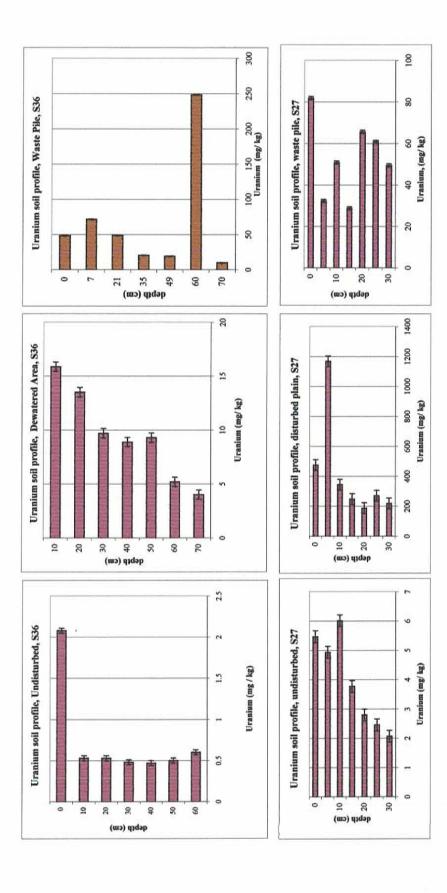
S27

The S27 soil profile uranium content varies in magnitude between the different land use area soil profiles (figure 40). While there is no clear trend of uranium with depth, each of the land use types can be identified based on the magnitude of the uranium content in each profile. The S27 undisturbed soil profile contains uranium from 2-6 ppm. The S27 disturbed plain soil profile contains uranium from 200-500 ppm, with one sample containing 1200 ppm uranium. The S27 waste pile soil profile contains uranium from 28-80 ppm, making it intermediate and distinguishable from the other two soil profiles.

S36

The same definition of land use types based on average uranium content in the soil profile is possible at S36. There are no clear trends of uranium with depth; however, the total uranium content of the land use types varies as shown by the soil profiles (figure 41). The S36 undisturbed soil profile contains from 0.5- 2 ppm uranium. The S36 drainage soil profile contains from 4-16 ppm uranium, and the S36 waste pile soil profile contains 15-70 ppm uranium, with the 60 cm sample containing 250 ppm uranium. The uranium concentration differences between each land use types' soil profile make it possible to distinguish land use type based on soil profile uranium content.





SEQUENTIAL EXTRACTION

'Surface' soil and soil profile samples were selected for Sequential extraction analysis based on the ICP-MS uranium content and field location. The samples' identifying information is listed in table 8. Because of high uranium values, the disturbed plain soil profile for S27 and S36 were selected.

Site	Sample	Land Use	U (ppm)	%gravels	% OC	% CaCO3
27	0 cm	disturbed plain	527.35	5.3	0.7	2.4
27	10 cm	disturbed plain	344.9	19.2	0.6	0.7
27	20 cm	disturbed plain	187.7	22.8	0.9	0.4
27	30 cm	disturbed plain	218.8	11.9	0.75	0.3
27	C1	lowland	174.4	3.3	1.1	0.35
27	G1	lowland	139.5	2.3	0.6	1.3
27	D2	disturbed plain	621.9	5.7	1.5	0
27	F2	disturbed plain	1040.45	2.2	0.4	0
36	0 cm	Waste pile	7	1.1	1.89	0.86
36	21 cm	Waste pile	3.39	1.53	1.65	0.07
36	49 cm	Waste pile	0.53	0.79	0.57	0.08
36	60 cm	Waste pile	6.21	3.08	2.80	0.48
26	D 1	Waata nila	1.20	n/avail	1.58	1.54
36	B1	Waste pile	1.39			
36	Н3	Lowland	16.72	n/avail	5.47	1.20

Table 8. Background information on selected samples for Sequential Extraction.

The sequential extraction information reported uranium values somewhat different from those listed in table 8. After dilutions and blanks were taken into account, the data is reported below in terms of a ratio of each uranium value to the others. This relationship emphasizes the role of the calcium carbonate soil fraction in binding uranium. In general, the organic fraction was the second most important source of uranium, with the exchangeable fraction binding more uranium at depth.

	average	average	average	average	average
	·		·		
	Exchangeable	Carbonate	<u>Oxide</u>	<u>Organic</u>	Residual
	F1 %	F2 %	F3 %	F4 %	F5 %
<u>27-2-0</u>	2.88	80.29	3.38	12.91	0.55
	0.17	4.95	0.59	4.49	0.04
<u>27-2-10</u>	5.36	74.41	5.97	13.66	0.60
<u>27-2-20</u>	22.51	47.90	8.42	20.05	1.12
27-2-30	14.57	42.03	10.18	31.72	1.50
	STATE OF THE STATE				
<u> 36-1-0</u>	4.12	52.33	21.04	21.84	0.67
<u>36-1-21</u>	6.68	65.17	15.19	11.73	1.23
<u>36-1-42</u>	29.72	45.11	11.48	12.60	1.09
<u>36-1-60</u>	54.29	35,53	5.22	4.72	0.24

<u>27+C1</u>	10.44	46.34	11.82	30.12	1.28
<u>27 + D2</u>	13.46	51.05	13.16	20.02	2.31
	0.39	1.28	1.69	3.37	0.01
27+G1	3.64	67.27	5.82	21.74	1.53

Table 9. Percent uranium for each Sequential Extraction fraction.

It is not intuitively obvious that the carbonate fraction of these soils, which is such a minor part of these soils, would be the major source of uranium bonds in these soils. At high pHs uranyl carbonates are more easily formed; and < 3% total CaCO₃ in the soil is still enough carbonate to bind < 1000 ppm uranium. The same is true with the small amounts of organic material in these soils, which were the second most important source of uranium bonds.

Sample	U (ppm)
NMSU Deionized water	0
Exchangeable fraction blank	0.04
Carbonate fraction blank	0.04
Oxide fraction blank	0.01
Organic fraction blank	0.04
Residual fraction blank	0.02
BRS Standard	0.64

Table 10. Sequential Extraction blanks are valid.

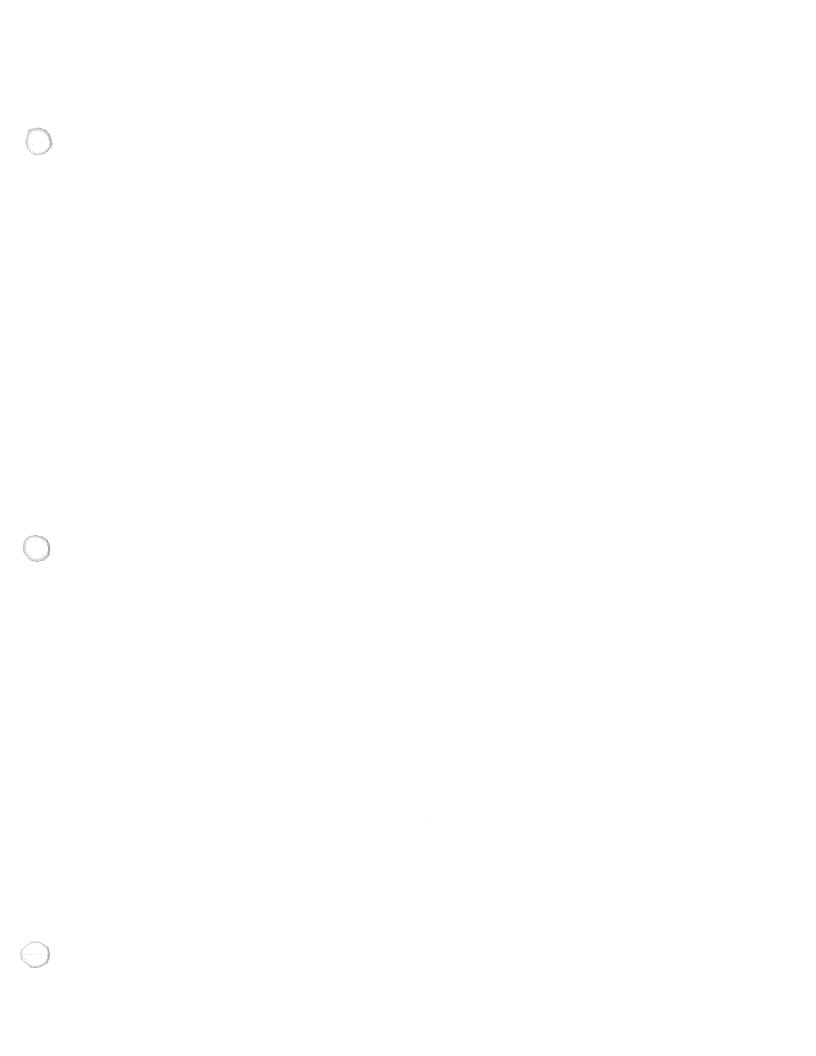
PLANT ANALYSES

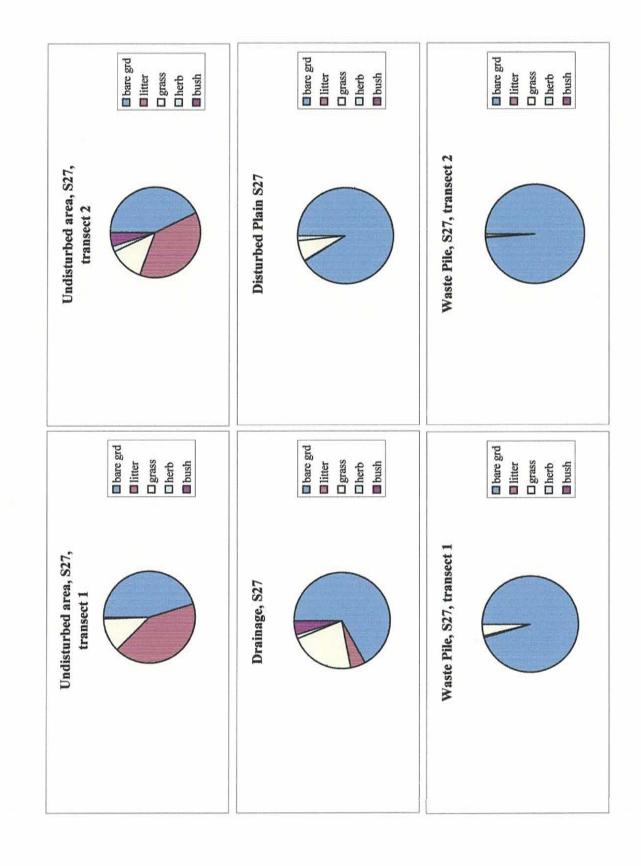
PLANT TRANSECTS

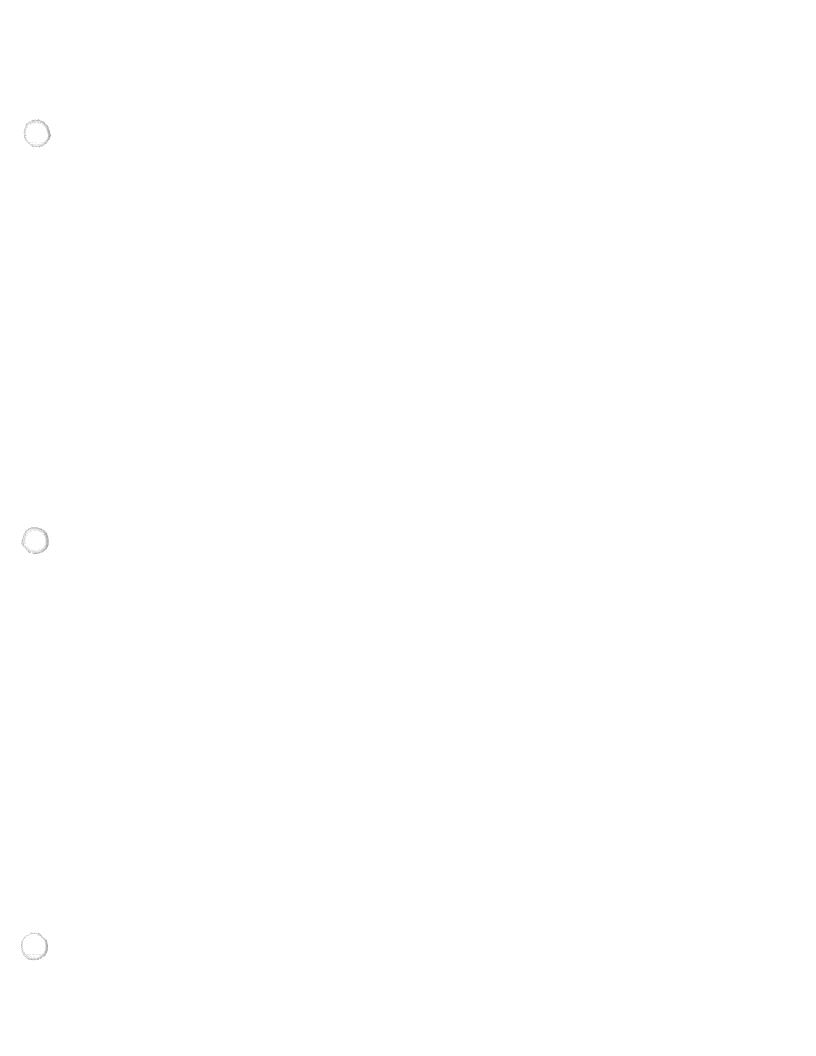
Plant transects were conducted to compare the ground cover and plant types of the different land use types (figure 42). At S27, the two undisturbed plant transects show that the undisturbed areas had litter covering half of the unvegetated soil surface (approximately 40% litter and total 84% unvegetated area). Grass covered 12% of the undisturbed soil surface.

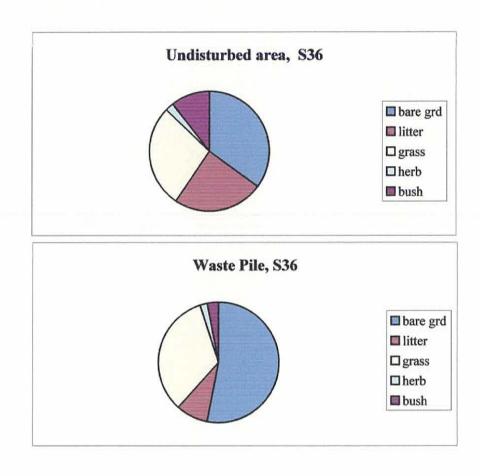
Both the litter and the grass content distinguish the undisturbed plant transect from the other land use types' plant transects. The drainage land use area had more grass (21%), but much less litter (5%) than the undisturbed land use area. The drainage area also had almost 5% bushes, and 1% herbaceous plants. The disturbed plain and the waste piles were predominatly bare ground (92-99%). The disturbed plain had almost 7% grass and 1.7% herbaceous plants. The waste piles had 0.1-4% grasses, and 0- 0.8% herbaceous plants. There were also differences between plant species in the different land use areas. For example, Indian Rice Grass was the one grass species found on the waste piles. This grass had twice the patch size of the other species and land use types-25 cm versus 8-13 cm.

At S36, two plant transects were recorded--one undisturbed and one across the waste pile (figure 43). Both had more plant cover, and more species variety than the S27 transects. The undisturbed plant transect was almost evenly split between grass cover, soil litter, and bare ground (25.8%, 22.7%, and 32.6% respectively). Blue grama grass predominated the grass patches (269/ 281 grass points recorded). The S36 waste pile plant transect is different from the S36 undisturbed area with its increased bare ground









(52.8%), decreased litter (8.6%) and decreased bush cover (3.3%). This waste pile vegetation transect has more vegetation and more variety than the S27 waste pile transects. This is probably due to time since disturbance--S36 had been abandoned at least 20 years prior to S27. The waste pile at S36 also has a central depression which may serve to collect precipitation and promote plant growth.

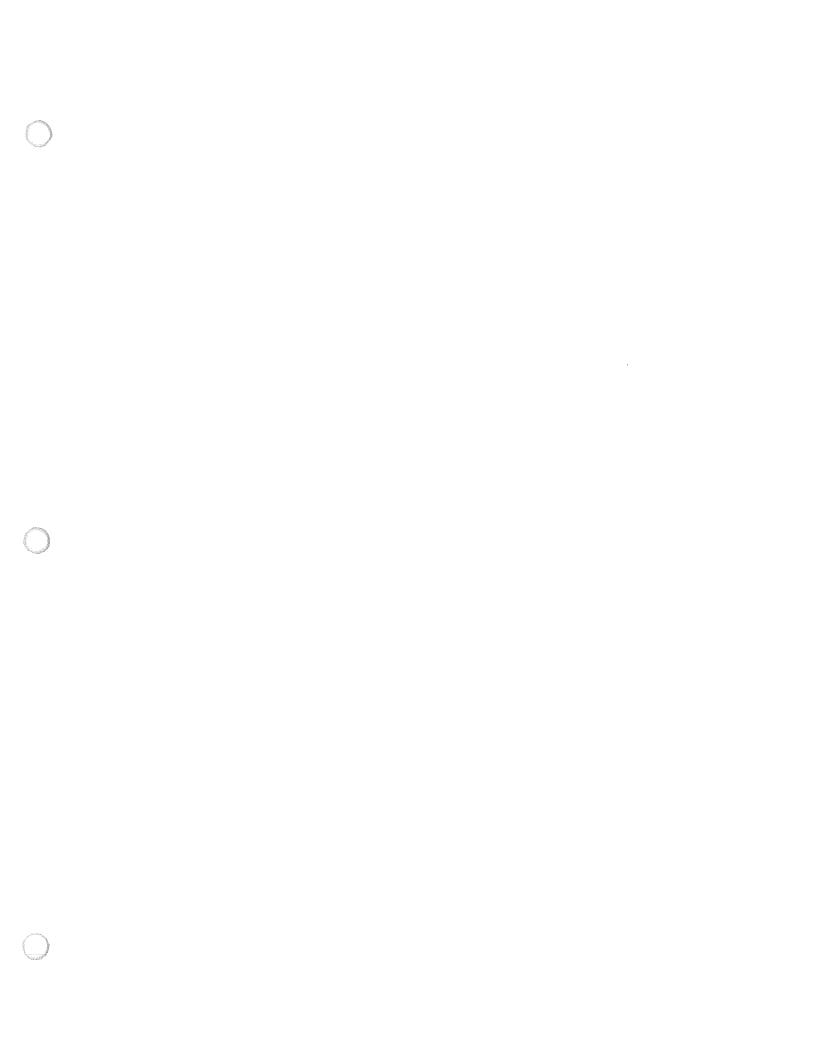
PLANT URANIUM CONTENT

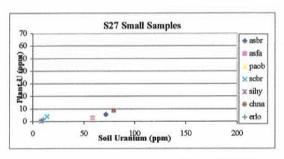
S27

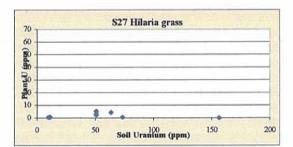
Three plants were taken at the established grid sampling points. These three plant samples included three different species at most points, and occasionally duplicate plant samples of the same species at the same point. These samples were also duplicated in the laboratory (Table 11).

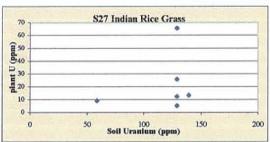
Plant Type	<u>Species</u>	# Field Pts	# Fld Samples	Analyzed	Graphed
Grasses	Tobosa grass	8	10	16	6
	Vine Mesquite	1	1	2	1
	Burro grass	1	1	1	1
	Squirreltail	2	2	2	1
	Sand Dropseed	4	4	7	3
	Indian Rice grass	3	3	3	6
	Blue Grama	1	1	3	0
Herbaceous	Wooly Buckwheat	2	2	5	1
	Tansy Mustard	3	3	5	3
	Stickleaf Blazing Star	2	4	6	2
	Curly Cup Gumweed	1	1	2	0
	Heath Aster	1	1	3	1
	Milkvetch	1	1	2	1
Shrubs	Rabbitbrush	1	1	2	1
	Fourwinged Saltbush	6	7	35	5
	Snakeweed	7	9	17	7
Weeds	Tumbleweed	5	6	12	4
	Kochia weed	9	13	17	8

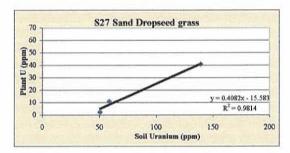
Table 11. Frequency of plant occurance at S27 sampling points, and of field sampling and ICP-MS analysis per plant species.

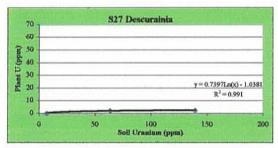




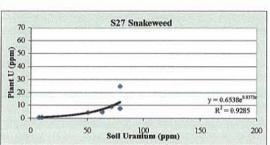


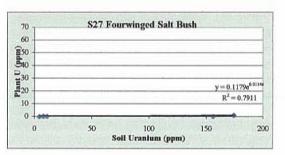


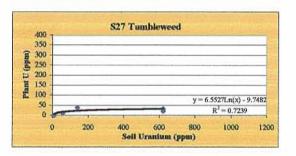












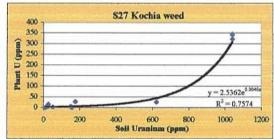


Figure 43 shows the relationship of plant uranium with soil uranium for 16 species at S27. S27 had higher soil uranium values (0-1000 ppm) than S36. Because of the higher soil uranium, the plant response to uranium is more indicative of potential phytoremediation applications. Eight of the ten graphs in figure 44 are at the same scale. These graphs indicate that there is a difference between species in plant uptake of soil uranium. A high ratio of plant U: soil U is a useful indicator for further phytoremediation studies. In the top eight graphs of figure 43, this high ratio is shown most clearly in the Stickleaf Blazing Star herb samples, which have a >100% (>1) plant uptake: soil uranium ratio. The high samples of the Indian Rice grass, Snakeweed and Sand Dropseed grass also have 0.46, 0.33 and 0.27 plant uranium concentration ratios. Most plant samples in these top eight graphs of figure 43 do not show significant uranium uptake.

The bottom two figures in figure 43 have scales approximately six times smaller than the above graphs in that figure. Tumbleweed's concentration ratio decreases with increasing soil uranium. Below 200 ppm soil uranium, tumbleweed accumulates up to 25% of soil uranium. At 600 ppm, it accumulates approximately 8.3% of soil uranium. Kochia weed appears to accumulate more plant uranium with increasing soil uranium. At the soil uranium high value (1050 ppm), Kochia weed accumulated approximately 31% of soil uranium in the plant material.

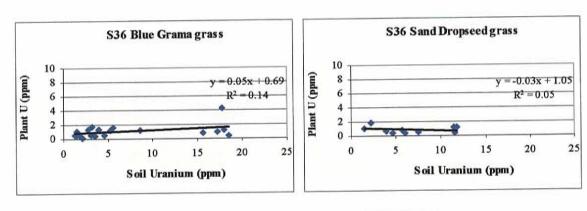
S36

More plant species were sampled at S36. Some species, such as Blue grama grass, Tansy mustard, Kochia weed, and Winterfat shrub occurred in abundance. Other species were sampled only a few times. The sampling duplication is listed in table 12.

Plant Type	Species	# Field Pts	# Fld Samples	Analyzed	Graphed
Grasses	Blue Grama	19	19	20	19
	Mountain Muhly	3	4	4	3
	Sand Dropseed	10	10	10	10
	Threeawn grass	2	2	2	2
	Tobosa grass	4	4	6	4
	Squirreltail	2	2	2	2
Herbaceous	Cleome serrulata	2	2	5	0
	Goosefoot-C. lepidium	3	3	6	3
	Gilia	2	4	6	0
	Scarlet Globemallow	1	1	2	1
	Mustard-D. pinnitifida	9	10	11	9
Shrubs	Fourwing Saltbush	1	1	3	1
	Willow	1	1	1	1
	Rabbitbrush	5	5	10	5
	Winterfat	10	11	35	10
	Snakeweed	2	2	4	2
	Fringed Sage	1	1	3	1
Weeds	Tumbleweed	1	1	1	1
	Kochia weed	11	15	15	11
Other	Lichen	2	2	2	2
	Bulrush	1	1	1	1

Table 12. Frequency of plant occurance at S36 sampling points, and of field sampling and ICP-MS analysis per Plant Species.

Because of the additional species and smaller average sample size per species at S36, more species were grouped together on single graphs. S36 also had much less soil uranium than S27. Up to 3 ppm can be considered "background" soil uranium values (reference). This allows fewer conclusions about plant uranium uptake and suggestions for phytoremediation.



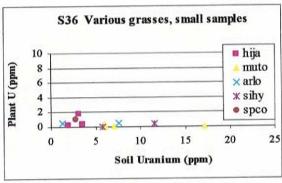


Figure 44. S36 Plant uranium concentration versus soil uranium for 7 species.

Figure 44 shows S36 grass uranium uptake. Three-awn, Mountain Muhly, Squirreltail and Spike dropseed grasses accumulated very little uranium. While none of these grass samples has "elevated" grass uranium concentrations, a few samples did show uptake at background soil uranium concentrations. Blue Grama, Tobosa, and Sand Dropseed grasses all had a point or a few points which accumulated 2 ppm plant U for less than 5 ppm soil U. Both the Blue Grama and Sand Dropseed grasses were frequently sampled and this 40% plant uranium concentration ratio did not continue with increasing soil uranium. In the Tobosa grass, only one of four graphed points showed this level of uranium uptake.

Six herbaceous species, and one sedge, were sampled at S36. Only one of these species, Tansy Mustard, had enough samples to allow trend analysis. The plant and soil uranium values for these samples are listed in figure 46.

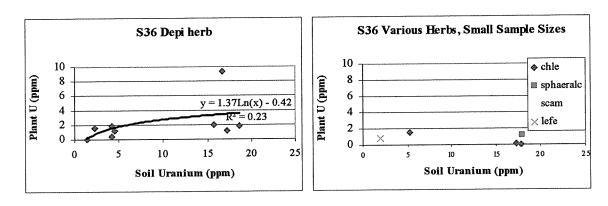
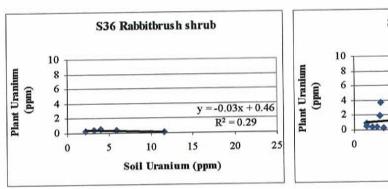
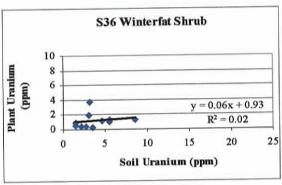


Figure 45. S36 Plant Uranium versus soil U concentration for five herb species.

Tansy Mustard was the only herbaceous species to accumulate more than 2 ppm uranium (figure 45). One Tansy Mustard sample accumulated 9 ppm plant uranium per 17 ppm soil uranium, a concentration ratio of 0.53. However, no linear or other plant uptake trend for Tansy Mustard could be established, and most points accumulated less than 2 ppm uranium.





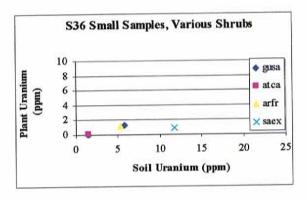


Figure 46. S36 Plant uranium uptake versus soil uranium for six shrub species.

Six shrubs were sampled at S36; these plant and soil uranium values are listed in figure 47. All shrubs had plant uranium values below 2 ppm. The Winterfat shrub showed a slight decrease of accumulated plant uranium with increasing soil uranium.

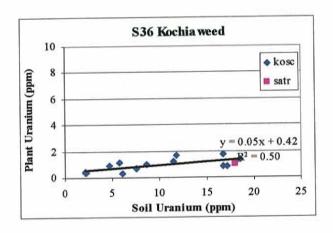


Figure 47. S36 Plant Uranium uptake versus soil uranium for two weed species.

Two weedy species were also sampled at S36: Kochia weed and Tumbleweed (figure 48). Both accumulated very little soil uranium at S36. Kochia weed, which had some high uranium uptake at S27, increased 1 ppm plant uptake over a 17 ppm soil uranium spread. Kochia weed did not show indications of high uranium uptake potential at S36.

S36 Waste Pile Plant Sampling

Nine species were additionally sampled along the waste pile plant transect line. This was done because of the low uranium values across most of S36, and the high values within the waste pile. These plant samples had slightly higher uranium values than the S36 grid samples (table 13). The shallowest sample of the waste pile soil profile contained approximately 48.6 ppm uranium. Assuming this concentration is constant across the waste pile transect, the Red Three-awn grass and Blue Grama grass have accumulated the most uranium of the plants in this table. These two samples had concentration ratios of 0.19 and 0.27. These ratios are higher than almost all grid samples.

sample point	Plant Species	U (ppm)	avg U ppm	<u>stdev</u>
W10	Blue Grama grass	2.26	5.65	4.79
W10	Blue Grama grass	9.04		
W15	Threadlead Groundsel	0.37	0.19	0.26
W15	Threadlead Groundsel	0.00		
W25	6-wks Three-awn grass	4.38	4.89	0.72
W25	6-wks Three-awn grass	5.40		
W25	Spike Dropseed grass	0.50		
W30	Red Three-awn grass	13.14		
W30	Indian Rice grass	2.14		
W35	Indian Rice grass	2.65		
W40	Russian Tumbleweed	1.79	1.32	0.66
W40	Russian Tumbleweed	0.86		
W40	Herbaceous Stickleaf	2.64		
W45	Winterfat Shrub	3.78	3.29	0.64
W45	Winterfat Shrub	2.36		
W45	Winterfat Shrub	3.47		
W45	Winterfat Shrub	3.56		
n/a	std	0.00		

Table 13. Uranium content of Waste Pile plant samples, S36.

DISCUSSION

DIFFERENCES BETWEEN THE LAND USE TYPES

Surface soil properties, soil profiles, vegetation transects, and vegetation samples were all used to test for differences between the land use types. The surface soil properties --particle size, pH, calcium carbonate, organic carbon, pH, and clay type--in almost all cases did not significantly distinguish the land use types. There were descriptive differences between the land use types in the soil profiles, however.

Land use types were also distinguishable topographically and with differing vegetation density. The waste pile and the lowlands can be distinguished based on respective topographic highs and lows. The disturbed plain and waste pile can be distinguished based on decreased vegetation, a lack of surface soil color, and an increase in relative surface soil sand content from waste rock and mining activity.

SURFACE SOILS AND SOIL PROFILES

Most of the soil sampling for this study was done at shallow depths (0-5 cm), in order to sample the exact rooting soil of the plants. One difference between arid and temperate soils is the higher activity and vertical movement of surface particles in the semi-arid soil. Certainly one insight from this study is that surface soil samples, for the purposes of phytoremediation, do not give a complete insight into the soil properties at depth. This is probably due to the active soil surface in this semi-arid area. This is further supported by the strong winds common to the area, and experienced during fieldwork.

URANIUM IN SURFACE SOILS

At S27, the most soil uranium content occurs along an old road included in the disturbed area. A small drainage channel now follows part of this road. Uranium is slightly lower here than on the waste pile surface samples. One disturbed area surface sample had 500+ ppm U. One undisturbed surface sample also had 50 ppm uranium. These two points illustrate some of the variability of the surface soils, and the difficulty using the surface soils to distinguish land use types. Ore loss from trucks and eolian transport may be two different surface processes confusing the picture of uranium occurrence across this site.

Uranium in the S36 surface soils distinguished between disturbed and less disturbed areas. The undisturbed and lowland areas had lower surface soil uranium than the disturbed plain and waste pile areas. However, this difference was approximately 2 ppm between the less and more disturbed surface soils over a range of 18 ppm.

SOIL PROFILE DIFFERENCES

While having much more limited sample sizes, the soil profiles provided more insight into the differences between land use types. Based on the soil profiles, the different land use types are distinguishable within each mine site, but not comparable between mine sites. The undisturbed soil profiles at S27 had higher relative organic carbon. The S36 undisturbed soil profile had higher relative CaCO₃ that increased with depth. Both undisturbed soil profiles had typically slightly higher pH values. The disturbed profiles typically had slightly lower pHs, low CaCO₃ content and high sand content.

S27 Soil Profiles

The undisturbed soil profile has gravels from 0-24%, predominately below 5%. It also contained mostly silt and clay, and had 3-4% organic carbon, but no CaCO₃. The disturbed plain and waste pile soil gravels, by contrast, are typically above 10%. These two profiles have organic carbon < 1% and high sand content, which suggests burial and little plant growth on these two disturbed soils.

S36 Soil Profiles

The undisturbed soil profile had gravels below 5% in all samples to 60 cm. There was ~2% organic carbon throughout this profile, and soil carbonate increased with depth to 3.1% at 60 cm. The S36 lowland and waste pile soil profiles had more relative carbonate at the surface and less relative carbonate at depth. The carbonate at the surface suggests the short development time of these two disturbed profiles. The S36 drainage soil profile has low sand and high organic carbon relative to all the other soil profiles, including both undisturbed profiles. This could be because of the effects of additional mine release water that flowed over this area while the mine was active and dewatering the underground uranium ore.

URANIUM CONTENT IN SOIL PROFILES

In the soil profiles, total uranium concentration differs for each land use type. As with the above soil profile samples, the sample sizes here are small. Highly variable urnaium concentration in some of the soil profiles suggests that the samples may represent highly variable uranium concentrations throughout the study area. However, the profiles suggest some differences between land use types.

The undisturbed profiles at each location had uranium concentrations below 6 ppm. Uranium decreased with depth at both undisturbed sites. The disturbed plain soil profile (S27) varied from 200-1100 ppm with most values ~350 ppm U. Both the S27 disturbed plain soil profile and the S36 drainage area soil profile had uranium decreasing with depth. The two waste piles also had patterns of uranium decreasing with depth. This was highly variable at the S27 waste pile soil profile. In the S36 waste pile soil profile, uranium decreasing with depth is interrupted by a high-uranium layer at 60 cm. This layer contains fine-grained tailings material, and is not a naturally developed soil layer.

VEGETATION AMOUNTS

The amount of vegetation is a good indicator of past land use. The more heavily disturbed the area, the less total vegetation was recorded by the vegetation transects. Vegetation communities, as measured by the vegetation transects, also differentiated the land use types. The undisturbed vegetation transects are characterized by equal amounts of bare ground and litter, while all other transects are dominated by bare ground. The S36 lowland area has a high diversity of species, but still lots of bare ground.

It is interesting that both the vegetation transects and the soil profiles helped to define the land use areas. There is not enough data here to support a direct link between the soil profile and vegetation transect of one land use area. However, it is possible that the variations in the soil profiles between each land use type affect the vegetation of each land use type. This suggests that perhaps vegetation here is more affected by variations in subsurface soil properties than the surface soils.

SEMI ARID AREA PLANTS AND URANIUM UPTAKE

In these samples, few plants appeared to be accumulating uranium. Of the plants with enough samples to plot on a graph, most did not increase in uranium concentration with increasing soil uranium.

Of the uranium that was found in the plants, it was often found at twice the concentrations in the leaves than the stems of the plants. Leaves grow faster and have a higher 'osmotic potential' than stems, because they are the primary site of transpiration. The leaf area within the plant could therefore be the site where uranium enters plant cells, as uranyl ions dissolved in water. This water flows from the plant stem xylem into leaf cells for transpiration and photosynthesis. This process may cause the uranium to be stored at a higher rate in the leaf cell vacuoles as plant waste.

Uranium concentrations in the plants were low in general, except for two Kochia samples at S27. The surface soils taken to relate to the plant uranium concentrations may in some cases not be the best measurement of available soil uranium. For example the rooting depth of large shrubs such as the saltbush or rabbitbrush may make deeper soil uranium available to the plant. However, even without the measurement of that deeper soil uranium, in the samples given in this study, most plants did not show elevated uranium concentrations. These species do not show special promise for phytoremediation.

In many cases, plants do not show linear uptake of plant uranium with soil uranium. This could be because these plants are genetically programmed to limit uranium uptake. Selection of uranium tolerant plant samples in the field may yield a uranium accumulating variant of that particular wild species.

Plants that did show uranium uptake, in this study, did not follow a consistent pattern. At S27, Sand Dropseed grass and Indian Rice grass both had some plant uranium uptake at soil concentrations ~140 ppm. However, the Sand Dropseed appeared to follow a linear uptake pattern, while the Indian Rice Grass sample was just one of six samples, 5 of which were not significant accumulators. The herb Stickleaf Blazing Star accumulated lots of uranium at a low soil concentration. For sheer uranium removal, this plant could be rated the best overall, with a CR of >2. However, this may be because the soil uranium was not measured accurately on the waste pile relative to this plant, and should have been measured at greater depth. Or, it could mean that the Stickleaf herb, is especially good at catching eolian dust particles, with some possible uranium content.

S36, which has been left undisturbed for ~ 20 years longer than S27, had more species sampled. It also had less overall uranium, and fewer species with any indications of uranium uptake. The Tansy Mustard and the Winterfat Shrub both had singular samples from the population which had CRs of ~0.5 and ~1 respectively. Kochia weed did not show uranium uptake at this mine site.

PLANT URANIUM UPTAKE RELATED TO SOIL PROPERTIES

. Six plant species sampled at the two study sites had large enough sample sizes for statistical comparison of plant uranium uptake with soil properties, including the relevant 'surface' soil properties. These species were Kochia weed, Sand Dropseed grass, Snakeweed, Tumbleweed, and Galleta grass.

Soil characteristics of the 0-5 cm surface soil samples were compared with the concentration ratio of plant:soil uranium. These plant samples were related to the soil properties pH, OC, CaCO₃, particle size, and uranium content.

These analyses only use the soil properties of 'surface' soil samples. Surface soils were previously proven to not have significant differences between land use types. For these comparisons, the land use type designations were set aside.

For all species, plant uranium uptake was related to pH:

Kochia	S27 U CR = -8.27 + 1.08 pH	<u>r-square</u> 75.5 %
receile	S36 CR = -100.1 + 15.2 pH	45.3%
Snakeweed	S27 U CR = 0.399 - 0.393 pH	4.4 %
Tumbleweed	S27 U CR = 1.81 - 0.21 pH	7.2 %
Sand Dropseed grass	S27 U CR = 2.62 + 0.35 pH	66 %

The other soil properties affected the different species' uranium uptake differently. Best fit equations for the different plant species were found in many cases to incorporate more than one soil property. Tumbleweed S27 U CR was controlled by organic carbon and calcium carbonate:

Tumbleweed S27 U CR = 0.15 - 0.07% OC - 0.1% CaCO3

$$(p = .11, .14; r-sq = 86.5\%).$$

Galleta grass's uranium uptake responded to organic carbon and silt in the soil:

Hija S36 U CR =
$$6.94 - 1.3$$
 OC $- 0.05$ silt p = 0.03 , 0.07 , r-sq = 99.93%

Uptake of uranium in winterfat, a small shrub responded to soil silt content:

Winterfat S36 U CR = 2.23 - 0.015 silt
$$p = 0.089$$
, r-sq = 31.82%

Sand dropseed grass occurred frequently at both S27 and S36. At S27, the CR regresses with calcium carbonate:

Sand Dropseed S27 CR = 0.42 - 0.2 % CaCO3 (p = 0.055, r-sq = 89.31%).

At S36, sand dropseed grass CR regressed with organic carbon:

log Sand Dropseed S36 CR = 2.12 - 0.275 OC (p = .155, r-sq = 30.6%).

Soil pH rises with calcium carbonate and drops with the presence of organic carbon. The uranium concentration ratio of Sand Dropseed grass at these two study sites appears to form a negative relationship with both calcium carbonate and organic carbon presence. This may seem counterintuitive; however, uranium does form different ionic complexes at different pHs. But between these two sites, the pH does not vary greatly. This plant species' uranium uptake may be reacting to soil property interaction effects. As one property (CaCO3) increases, another (OC) decreases. So the uranium uptake of this plant may be competing (negative relationship) with the dominant form of soil carbon at a particular site.

Snakeweed is a very common, low-growing (to ~ 2 feet) perennial shrub. It has long pinnate leaves and persistent yellow blossoms. At S27, scatterplots of total uranium plant CR and leaf CR did not suggest any relationships with measured soil characteristics. Plant stem CR data also does not regress significantly with soil variables. The best relationship suggests that pH can explain 4.4% of Snakeweed's uranium concentration.

SUMMARY

Significant influences of soil properties vary by plant species and mine site. Kochia weeds' uranium uptake was influenced by soil pH variations at both sites. Sand dropseed grass's uranium uptake was influenced by soil calcium carbonate content at S27. Also at S27, Tumbleweed's uranium uptake was influenced by both organic carbon and

calcium carbonate. At S36, the Galleta grass and the winterfat shrub's uranium uptake were influenced by soil silt content. Galleta grass was also influenced by organic carbon.

pH is an important factor in soil chemistry and in phytoaccumulation. Except for Kochia weed, it is not the predominant factor affecting these plant's uranium uptake. Carbon forms in the soil --organic carbon or calcium carbonate--seem to have more extensive influence on plant uranium uptake.

RAMIFICATIONS FOR PHYTOREMEDIATION

This study specifically investigates diffuse surface uranium contamination. At background levels of uranium concentration, a number of species uptake small amounts of uranium. Species for further investigation, and possible genetic selection studies include Kochia weed, and Galleta, Sand Dropseed, Red Three-awn and Indian Rice grasses. The Winterfat shrub and Tansy Mustard, Stickleaf herbs may also have certain plants within the species that are more tolerant of uranium and could be cultivated for possible phytoaccumulation.

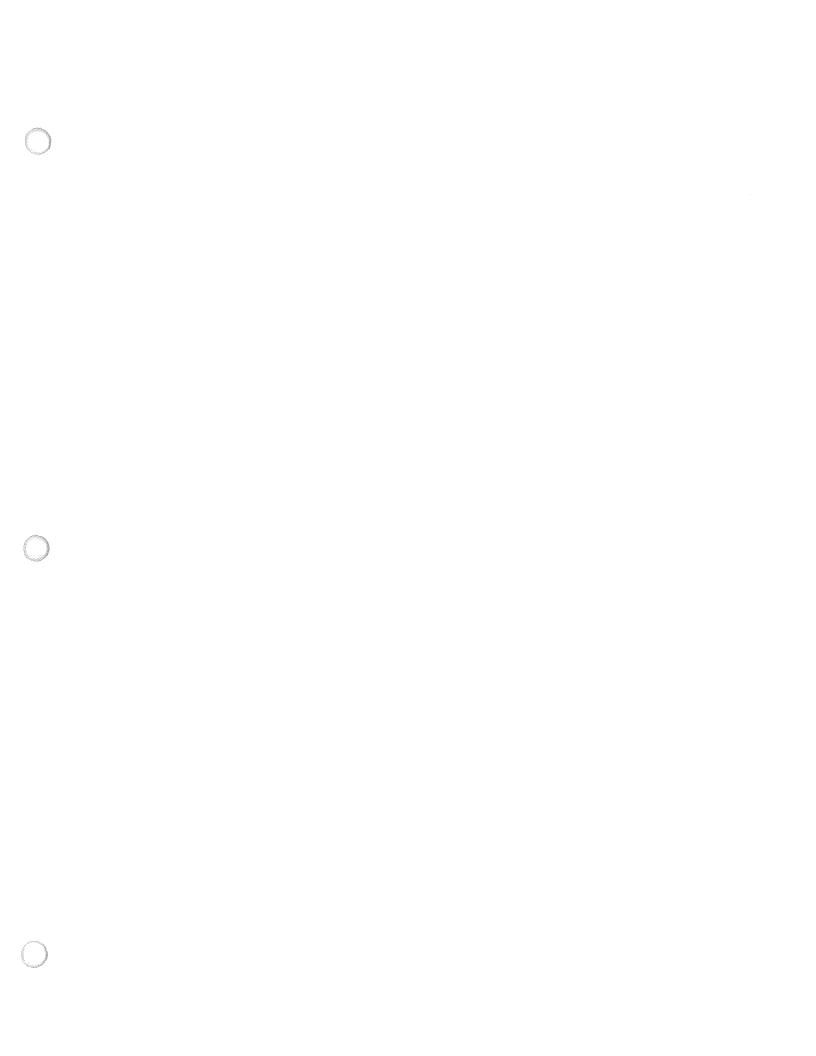
Land use type influences plant species distribution across these two sites. An overall lessening of plant growth on the more disturbed land use areas was seen in this study. Phytoremediation approaches could benefit by considering the various land use types of semi-arid areas proposed remediation sites. The land use types can influence the success of vegetation, the soil texture, and the movement of uranium through the soil profile. Soil profiles are useful for phytoremediation as well because some of the plants considered for phytoremediation were shrubs with rooting depths of up to 1 m.

URANIUM PHYTO-UNDER-ACCUMULATION IN SEMI-ARID SOILS

The soil profiles suggest that non-surface soils can be defining characteristics of the differences between land use types. The land use types also reflect differences in the vegetation communities. Based on this information, we can suggest but not prove a link between the two. If the two were linked, soil horizons could possibly affect uranium movement in semi-arid soils in different ways in disturbed and undisturbed soils (Figure 49). Undisturbed soils might allow little uranium availability to plants because of their relatively higher water infiltration and resultant uranium transport deeper into the profile, away from plant roots. Disturbed soils would allow little uranium uptake because of the harsher conditions for plant growth.

For example, undisturbed soils in this study have typically more grass content and more total vegetation cover. This will allow relatively more water infiltration on a small scale (Rone, 2001). These relatively higher amounts of water infiltration may carry uranium to deeper depths within the soil profile (as seen in figure 40, S36 drainage profile and S27 disturbed plain profile). This greater depth of uranium in the soil profile may make it less available to plants for potential uptake. While the area probably has more total plant biomass, it may have less uranium concentration in plants because of the deeper sequestration of uranium in the soil profile.

Disturbed soils will exhibit less soil development (CaCO₃ content), and have more shrub growth and bare ground on the soil surface. This results, typically, at smaller scales, in less water infiltration and more runoff (Rone, 2001). Less water infiltration into the soils would create less uranium movement into deeper soil horizons, but plant



NW NM U-contaminated lands

Disturbed soil

More bare ground, shallow rooting depth to catch avail. water

Less small-scale infiltration

Less uranium movement in soil profile

More relative uranium available to fewer plants in rooting zone

Undisturbed soil

Less bare ground, shallow rooting Depth of grasses

More small-scale infiltration

More uranium movement in soil profile

Less relative uranium available to plants in rooting zone

Low plant accumulation of uranium

uptake of uranium in disturbed soils would still be low, based on the lower amounts of plant cover, and (potentially) shallower rooting depth of these plants. Fruitful future work could concentrate on intraspecies variations in uranium phytoaccumulation. A focus on root zone definition and description relative to soil properties, soil uranium content, and plant uranium uptake could also be insightful.

POTENTIAL CAUSES FOR VARIABILITY

Because of the grid sampling pattern, the number of samples varied in each land use type, as well as for each plant species sampled. These sampling size considerations limit the strength of the conclusions. Future sampling should be targeted on one specific question of investigation in order to increase the strength of the conclusions.

Alternative sampling strategies could be completely random sampling, completely stratified sampling, or stratified random. Stratified random (based on land use type) would be the best to test the differences between the land use types. Non-grid, nonrandom sampling (based on plant species) would be the best to test the differences between the plant species. The combination of grid sampling and non-grid land use type sampling used here allows both land use type and plant sampling to be conducted as part of a unified study. Because of these different lines of inquiry, the sample sizes were overall large, but barely sufficient for the plant/ soil properties comparison. Future studies might benefit from a narrowing of the questions of investigation, and targeting the sample sizes to answering one or two questions.

Because the number of plant species sampled was not limited, but instead maximized, many of the plant species have small sample sizes. This makes statistically

valid conclusions difficult. One way to estimate the variability of a population is through the standard deviation measurement.

The plant samples were put through a number of steps; sampling in the field, preparation in the lab, and analysis on the ICP-MS. Standard deviation (σ) can be measured for field samples where two plants of the same species were sampled at the same grid point. Numerous duplicates were also prepared in the laboratory. The ICP-MS also analyzes each sample multiple times and provides an average of these samples, as well as a residual standard deviation (RSD) value. The total standard deviation for a sample can be calculated as:

$$\sigma_{\text{Total}} = \sigma_{\text{Field}} + \sigma_{\text{Laboratory}} + \sigma_{\text{ICP-MS}}$$

Unfortunately field and laboratory measurements can only be reported after they have been measured on the ICP-MS. Therefore the above equation becomes

$$\sigma_{\text{Total}} = \sigma_{\text{Point (ICP-MS values)}}$$
.

For example, the high uranium Kochia weed in Section 27 had three plant samples at the same point. These two plants had uranium values of 323.6, 343.6, and 347.7. The total standard deviation for these plant samples is 12.91. A more typical, lower uranium point at section 27 had plant values of uranium 5.9, 6.4, and 16.4 and standard deviation 5.9. A typical, low uranium point at S36 had plant values of uranium 0.9, 1.8 and standard deviation 0.64 (Keith, 1991).

SOIL SAMPLING

Western U.S. state Soil Surveys (Wyoming, Oregon) typically advise sampling a soil by taking multiple samples (< 1 kg) in an area, mixing them together, and then splitting out a subsample for analysis. In this study, single samples were typically larger than 1 kg. These samples were then split into one or more subsamples for analysis. While the study might benefit from multiple blended soils into each sample, this is difficult to accomplish for different plant sizes, with different rooting radiuses and depths, without entire excavation of each sampled plants' rooting soil.

The soil samples split for analysis for uranium analysis split a ~0.2 g dried soil sample from a sample > 1 kg. This analysis was subsequently done by using grinding, instead of splitting, in order to do the analysis. For simplicity and duplication of the sample, ground soil preparation is probably a preferable method to choose in the future.

CONCLUSIONS

LAND USE TYPES

Land use types show differences in their uranium content. These differences are reflected in increased uranium concentrations in increasingly disturbed soil profiles. Land use type differences in uranium concentration are not seen in surface soils.

The soil profiles and plant transects show differences between land use types. The undisturbed transects of both locations showed much more soil litter than the disturbed transects. Both undisturbed soil profiles had slightly higher soil pH's. The S27 undisturbed soil profile had higher OC and clay content than the disturbed soil profiles. The S36 undisturbed soil profile had more carbonate at depth than the disturbed soil profiles.

Surface soil sampling did not reflect differences between land use types. Sample sizes were much smaller in the soil profiles. Soil profile sample sizes limit the significance of the conclusions.

URANIUM IN SOILS

Uranium concentration did not vary consistently in proportion to changes in soil properties. While uranium activity in the soil and vegetation appears to be affected by

soil properties, uranium concentration is probably influenced more by previous disturbance.

URANIUM IN PLANTS

Some plants show more uranium accumulation than others, but intraspecies variations also exist. Kochia weed at S27 had two samples with 30% uranium accumulation where the soil uranium was 950 ppm. All other Kochia samples showed much less uranium accumulation. Conclusions about any species are limited because of the small number of samples for each species. At S27, Indian Rice Grass, Sand Dropseed grass, and Snakeweed shrub show promise based on their plant: soil uranium ratio. No plants at S36 accumulate uranium beyond background levels. Some plant species appear to accumulate uranium relative to different soil properties for each species.

REFERENCES

- Baumgartner, D. J., E. P. Glenn, et al. (2000). "Effect of Irrigation Water Contaminated with Uranium Mill Tailings on Sudan Grass, Sorghum vulgare var. sudanense, and Fourwing Saltbush, Atriplex canescens." Arid Soil Research and Rehabilitation 14: 43-57.
- Birkeland, P. W. (1999). "Soils and Geomorphology: Third Edition." Oxford University Press, New York: 430 pp.
- Cannon, H. L. (1951). "The Effect of Uranium-Vanadium Deposits on the Vegetation of the Colorado Plateau." American Journal of Science 250(October): 735-770.
- Chaney, R. L. (1995). "Metal-scavenging Plants to Cleanse the Soil." Agricultural Research: 4-14.
- Chaney, R. L., Yin-Ming Li, Sally L. Brown, Faye A. Homer, Minnie Malik, J. Scott Angle, Alan J.M. Baker, Roger D. Reeves, Mel Chin (1999). Improving Metal Hyperaccumulator Wild Plants to Develop Commercial Phytoextraction Systems: Approaches and Progress. Phytoremediation of Contaminated Soil and Water. N. T. a. G. Banuelos, Lewis Publishers: 85-108.
- Chenoweth, W.L., Harlan K. Holden, 1980, "Exploration in Grants Uranium Region since 1963" in Geology and Technology of the Grants uranium region 1979, Christopher Rautman, compiler: New Mexico Bureau of Mines and Mineral Resources, Mem. 38, p. 17-21.
- Chenoweth, W.L., E. A. Learned, 1979, "Stratigraphic section, Ambrosia Lake area, McKinley and Valencia Counties, New Mexico" in Geology and Technology of the Grants uranium region 1979, Christopher Rautman, compiler: New Mexico Bureau of Mines and Mineral Resources, Mem. 38, p.400.
- Connors, K.F., T.W. Gardner, G.W. Petersen. (1987). "Classification of Geomorphic Features and Landscape Stability in Northwestern New Mexico Using Simulated Spot Imagery." Remote Sensing of Environment 22:187-207.

- Dewitt-Ivey, (1995). "Flowering Plants of New Mexico, third edition." Published by the author: 504 p.
- Dhoum, R.T., G.J. Evans. (1998). "Evaluation of uranium and arsenic retention by soil from a low level radioactive waste management site using sequential extraction." Applied Geochemistry, 13:4: 415-420.
- Duenas-Parshley, B., R. Kenny. (2000). "Reconnaissance Investigation of Equivalent Uranium in Soil, Grants, NM." New Mexico J. Sci. 40 (1): 1-11.
- Dodge, (1985).
- Duff, M. C., C. Amrhein, P.M. Bertsch, D.B. Hunter. (1996). "The chemistry of uranium in evaporation pond sediment in the San Joaquin Valley, California, USA, using X-ray fluorescence and XANES techniques." Geochemica et Cosmochemica Acta, 61:1:73-81.
- Duff, M. C., D. E. Morris, et al. (2000). "Spectroscopic characterization of Uranium in evaporation basin sediments." Geochimica et Cosmochimica Acta 64(9): 1535-1550.
- Elless, M. P. and S. Y. Lee (1998). "Uranium solubility of carbonate-rich Uranium-contaminated soils." Water, Air, and Soil Pollution 107: 147-162.
- Fitch, D.C. (1979). "Exploration for Uranium Deposits, Grants Mineral Belt" in Geology and Technology of the Grants uranium region 1979, Christopher Rautman, compiler: New Mexico Bureau of Mines and Mineral Resources, Mem. 38, p. 40-51.
- Francis, C. W., Timpson, M.E., Lee, S.Y., Elless, M.P., Wilson, J.H. (1998). "The use of carbonate lixiviants to remove uranium from uranium-contaminated soils."

 Journal of Radioanalytical and Nuclear Chemistry 228(1-2): 15-20.
- Francis, A.J., C.J. Dodge. (1998). "Remediation of Soils and Wastes Contaminated with Uranium and Toxic Metals." Environ. Sci. Technol. 32: 3993-3998.
- Galloway, W.E. (1979). "Deposition and Early Hydrologic Evolution of Westwater Canyon Wet Alluvial-Fan System" in Geology and Technology of the Grants uranium region 1979, Christopher Rautman, compiler: New Mexico Bureau of Mines and Mineral Resources, Mem. 38, p. 59-68.
- Gay, I. M. (1963). Uranium Mining in the Grants Uranium District. Geology and Technology of the Grants Uranium District. V. Kelley. Socorro NM, New Mexico Bureau of Mines and Mineral Resources. Memoir 15: 244-246.

- Hossner, L. R., H. J. Woodard, et al. (1992). "Growth and Selenium Uptake of Range Plants Propagated in Uranium Mine Soils." Journal of Plant Nutrition 15(12): 2743-2761.
- Huang, J. W., M. J. Blaylock, et al. (1998). "Phytoremediation of Uranium-Contaminated Soils: Role of Organic Acids in Triggering Uranium Hyperaccumulation in Plants." Environmental Science and Technology 32(13): 2004-2008.
- Ibrahim, S. A. and F. W. Whicker (1992). "Comparative Plant Uptake and Environmental Behavior of U-Series Radionuclides at a Uranium Mine-Mill." Journal of Radioanalytical and Nuclear Chemistry, Articles 156(2): 253-267.
- Janitzky, P. (1986). "Particle Size Analysis." in Field and Laboratory Procedures used in a Soil Chronosequence Study. M.J. Singer and P. Janitzky, editors. Denver, Co, U.S. Geological Survey Bulletin 1648: 11-15.
- Janitzky, P. (1986). "Determination of Soil pH." in Field and Laboratory Procedures used in a Soil Chronosequence Study. M.J. Singer and P. Janitzky, editors. Denver, Co, U.S. Geological Survey Bulletin 1648: 19-20.
- Jurinak, J. J. and K. K. Tanji (1993). "Geochemical Factors Affecting Trace Element Mobility." Journal of Irrigation and Drainage Engineering 119(5): 848-867.
- Keith, L.H. (1991). "Chapter 1: Planning and Sampling Protocols." in Environmental Sampling and Analysis: A practical guide. Chelsea, Mi, Lewis Publishers: 7-24.
- Knight, P.J. (1992). "Vegetation and Plant Communities of the San Juan Basin. in San Juan IV. Spencer Lucas, Barry Kues, Thomas Williamson, Adrian Hunt. Socorro, NM., New Mexico Geological Society:34-37.
- Landon, M. (1991). Personal Communication. New Mexico State Land Office Field Representative.
- Langmuir, D. (1978). "Uranium Solution-Mineral Equilibria at Low Temperatures with Applications to Sedimentary Ore Deposits." Geochimica et Cosmochimica Acta 42: 547-569.
- Laverty, R. A., W.R. Ashwill, W.L. Chenoweth, D.L. Norton (1963). Ore Processes. Geology and Technology of the Grants Uranium District. V. Kelley. Socorro NM, New Mexico Bureau of Mines and Mineral Resources. Memoir 15: 191-204.
- Litaor, M. I. (1995). "Uranium Isotopes Distribution in Soils at the Rocky Flats Plant, Colorado." Journal of Environmental Quality 24(2): 314-323.
- Loftin, S. (1999). "Use and Application of Community Structure Analysis plant survey approach." Personal communication and uncited paper.

- Luthiger, P. (2001). Personal communication on site visit, 3/15/01, Quivera Mining Company (Rio Algom), Grants, NM.
- Luthiger, P. (2002). "Mining technique." Unpublished essay, Rio Algom, Ambrosia Lake, NM:10 p.
- Machette, M. (1986). "Calcium and Magnesium Carbonates." in Field and Laboratory Procedures used in a Soil Chronosequence Study. M.J. Singer and P. Janitzky, editors. Denver, Co, U.S. Geological Survey Bulletin 1648: 30-32.
- Melancon, P.E. (1963). "History of Exploration." in Geology and Technology of the Grants Uranium District. V. Kelley. Socorro NM, New Mexico Bureau of Mines and Mineral Resources. Memoir 15: 3-5.
- Meyer, M. C., T. McLendon, et al. (1998). "Evidence of Depleted Uranium-Induced Hormesis and Differential Plant Response in Three Grasses." Journal of Plant Nutrition 21(11): 2475-2484.
- Mortvedt, J. J. (1994). "Plant and Soil Relationships of Uranium and Thorium Decay Series Radionuclides." Journal of Environmental Quality 23(4): 643-650.
- National Resource Conservation Service, 2003. "Penistaja--New Mexico State Soil."

 ftp://ftp-fc.sc.egov.usda.gov/NSSC/StateSoil Profiles/
 nm soil.pdf July, 2004. 1 p.
- Pfeifer, H.-R., M. Vust, et al. (1994). "Uranium-enrichment in soils and plants in the vicinity of a pitchblende vein at La Creusaz/ Les Mare'cottes (W of Martigny, Valais, Switzerland)." Ecologae geol.Helvetica 87(2): 491-501.
- Rabenhorst, M.C. (1988). "Determination of Organic and Carbonate Carbon in Calcareous Soils using Dry Combustion." Soil Sci. Soc. Am. J. 52: 965-969.
- Ramos, L., L. M. Hernandez, M.J. Gonzalez. (1994). Sequential Fractionation of Copper, Lead, Cadmium, and Zinc in Soils from or near Donana National Park." J. Environ. Qual. 23: 50-57.
- Ramsey, F.L., Schaefer, D.W. (2002). "The Statistical Sleuth: A course in Methods of Data Analysis." Pacific Grove, Ca, Duxbury Thomson Learning: 743 p.
- Rone, R. G. (2001). "A Comparison of Sediment Production on Chemically Treated and Untreated Sagebrush Rangeland in the Rio Puerco Headwaters near Cuba, New Mexico." New Mexico Institute of Mining and Technology, unpublished thesis: 186 p.

- Santos, E. S. (1963). Relation of Ore Deposits to the Stratigraphy of the Ambrosia Lake Area. Geology and Technology of the Grants Uranium Region. V. Kelley. Socorro, NM, New Mexico Bureau of Mines and Mineral Resources. Memoir 15: 53-59.
- Saric, M., M. Stojanovic, et al. (1995). "Uranium in Plant Species Grown on Natural Barren Soil." Journal of Plant Nutrition 18(7): 1509-1518.
- Schilk, A. J., K. H. Abel, et al. (1995). "Characterization of Uranium Contamination in Surface Soils." Journal of Environmental Radioactivity 26: 147-156.
- Smith, G.D., M. McFaul. (1998). "Paleoenvironmental and geoarchaeologic implication of late Quaternary sediments and paleosols: North-central to southwestern San Juan Basin, New Mexico." Geomorphology 21, no 2., 107-138.
- Soil Conservation Service. (1993). "Soil Survey: Cibola area, New Mexico." :129-135.
- Soil Science Society of America. (2003). green method book. available uranium procedure.
- Sposito, G. (1989). The Chemistry of Soils. New York, Oxford University Press: 277 p.
- Tessler, A., P.G.C. Campbell, and M. Bisson. (1979). "Sequential Extraction Procedure for the Speciation of Particulate Trace Metals." Analytical Chemistry, vol 51, no 7:844-850.
- Tzschetzsche, S. (2003). Personal communication. Soil Scientist, NRCS: Grants District, NM.
- Turney, W. R. (1995). Remediation of Uranium-Contaminated Soils by Use of Carbonate Heap Leach: Fernald Materials Production Center. Engineering, University of New Mexico: 197.
- U.S. EPA (1994). Method 3051: Microwave assisted acid digestion of Sediments, Sludges, Soils, and Oils. http://www.epa.gov/epaoswer/hazwaste/test/pdfs/3051.pdf July, 2004. 14 p.
- U.S. EPA (1996). Method 3052: Microwave assisted acid digestion of Siliceous and Organically Based Matrices. http://www.epa.gov/epaoswer/ hazwaste/test/pdfs/3052.pdf July, 2004. 20 p.
- Vaininetti, J. (1996). Uranium Sorption on calcite and calcareous soil. Soil Science. Logan, Ut, Utah State University: 89.
- Watt, P. M. (1996). Landscape-Evolution and Soil Genesis On the Pajarito Plateau and the Impact of Soil Chemical Physical Properties on Contaminant Uranium

- Migration, Los Alamos National Laboratory, New Mexico. Earth and Planetary Sciences, University of New Mexico: 353.
- Wells, S.G., L.D. Potter, "Chapter 2: Applications of Geomorphology to Reclamation." in Applications of Geomorphology.
- Willett, I. R. and W. J. Bond (1998). "Fate of manganese and radionuclides applied in uranium mine waste water to a highly weathered soil." Geoderma 84: 195-211.
- Willett, I. R. and W. J. Bond (1995). "Sorption of Manganese, Uranium, and Radium by Highly Weathered Soils." Journal of Environmental Quality 24: 835-845.
- Yoshida, S., Yasuyuki Muramatsu, Keiko Tagami, Shigeo Uchida, Tadaaki Ban-nai, Hidenori Yonehara, Sarat Sahoo (2000). "Concentrations of uranium and 235/238 U ratios in soil and plant samples collected around the uranium conversion building in the JCO campus." Journal of Environmental Radioactivity 50: 161-172.

APPENDIX A

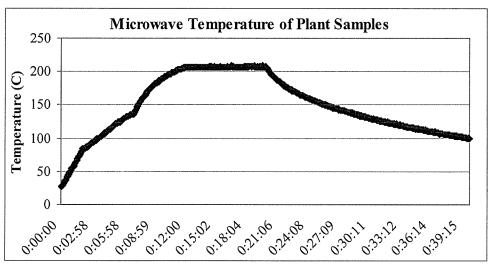
Additional Laboratory Methods

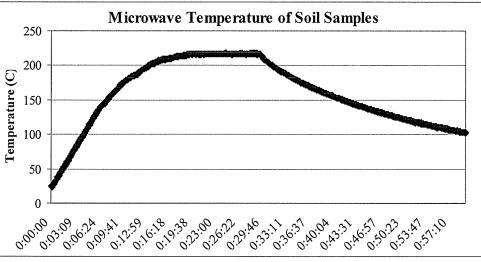
XRD CLAY TYPE ANALYSIS

Procedure for preparation of oriented clay mineral aggregates

- 1. Place a small sample (20 to 25 g) in a 100 ml beaker with distilled water. Mix and wait 5 minutes.
- 2. If the clay flocculates or settles out, pour off clear water, add more water, and remix. If the clay does not disperse, repeat this step several more times.
- 3. If the clay still flocculates, add a few drops of dilute solution (50g/L) of sodium hexametaphosphate (Calgon) and remix. If the clay flocculates, repeat step 2.
- 4. Centrifuge for 4 minute, wash with distilled water, and centrifuge again as often as needed.
- 5. Once the clay is in a dispersed state, allow the beaker and its contents to remain undisturbed for 10 minutes. At the end of the period, use small pipette (1-2 ml) to draw off enough suspension from the surface to cover a glass slide completely. This decanted fraction is < 2um. Prepare at least two slides and allow to air dry.
- 6. Use petrographic glass slides that have a high melting point.
- 7. If clay slurry flocculates on the slide surface, remake slide.
- 8. Run the slide of oriented clay on diffractometer at 2° 2θ/minute from 2° to 35° 2θ with monochromatic or Ni-filtered Cu radiation. Subsequent runs (glycolated and heat tratment) will vary depending on the mineralogy and nature of the information needed.

MICROWAVE SAMPLE DIGESTION FOR ICP-MS ANALYSIS





ICP-MS DATA ANALYSIS

Dilution Selection

For each sample analyzed, the ICP-MS prepared two auto-dilutions, approximately 1:5 and 1:100. The ICP-MS then reported uranium values at these two different concentrations. For high uranium values, the more diluted concentration was typically more accurate. For low uranium values, the less diluted concentration was typically more accurate. For high uranium concentration in the soil or plant, (> 5ppm) the concentration was reported using the highly autodiluted sample (1:105.9) versus those samples with expected low uranium values (which were autodiluted 1:5). Where other elements were reported, the RSD was also checked to be below 10%. If the RSD was not below 10%, the other dilution was used.

Procedure to Prepare Data for Analysis

- a) Assemble appropriate information into one table. This includes ICP-MS data from different days, and the relevant laboratory data from different digestion runs.
- b) Calculate uranium ppm.
- c) Based on uranium ppm, choose appropriate dilution for final uranium concentration. For ICP-MS data after ~9/17/02, two dilutions of each sample were run --~ 1:5 and 1:100. Only one dilution for the final data assembly is desired. Where uranium is > 5 ppm, the 1:100 dilution is a more accurate measurement. Where uranium is < 5 ppm, the 1:5 dilution is a more accurate measurement.
- d) Check residual standard deviation (RSD) values for uranium and all other elements. The ICP-MS analyzes each sample multiple times (~12-24). Each value in the ICP-MS report is an average of these analyses. The residual is the difference between each individual analysis and the average. The residual

- standard deviation is the standard deviation of all residual values for that element, for that sample.
- e) Eliminate all RSD values above 10%. Each sample has an RSD reported for each element (after 9/17/02). Samples before 9/17/02 did not have RSD values reported. Each RSD for each element for each sample must be checked to be below 5%.
- f) Substitute ppb values from the other dilution, if the RSD value for that element is below 10%. The uranium values and RSD's were closely watched during the ICP-MS laboratory run of each sample. However, other elements can be 1000 times less or more than the uranium value. While one dilution for a sample was selected based on the Uranium value, other elements may indicate consideration of the other dilution's value for that element. Where necessary, this was done.
- g) Calculate ppm for all elements.
- h) Remove all RSD values from the table. Residual standard deviations are a data quality check. Once it has been ensured that all the data are of good quality, the RSD value is distracting to the analyses. These values are listed in the appendix.
- i) Calculate averages for duplicated samples. Calculate standard deviations for all elements for duplicated samples.
- j) Separate final data into tables of common soil elements and relevant soil elements and metals.

SEQUENTIAL EXTRACTION FOR HEAVY METALS PROCEDURE

Draft procedure expanded from M.J. Blaylock, Edenspace, N.J. May, 2001 Adapted from Ramos et al., 1994.

Goal: Identify metals bound with each soil fraction: Exchangeable, Carbonate, Oxide, Organic, and any residual metals. Used here specifically for uranium, but originally developed for lead.

Procedure: Use increasingly aggressive chemicals to extract metals from the same soil sample. For the first three steps, the chemical is added, the samples are agitated for 1 hour or more, and then the samples are centrifuged and the supernatant (remaining clear

liquid) is removed. These first three extraction steps are repeated once to ensure complete extraction of the associated metals. Tube, cap, and sample weights at each step are necessary to account for water and metal carryover between fractions.

Materials: per sample: 2.5 g oven dried soil sample

8 50 mL centrifuge tubes

50 mL 1 M MgCl₂ (Magnesium Chloride)

50 mL 1 M NaOAc (pH 5) (Sodium Acetate)

50 mL 0.04 M NH₂OH-HCl (in 25% Acetic Acid)

(Hydoylamine HCl)

5 mL 0.1 M HNO₃ (Nitric Acid)

6 mL 30% H₂O₂ (Hydrogen Peroxide)

10 mL 1:1 HNO₃

5 mL concentrated HNO₃

for procedure:

reciprocating shaker

automatic dispenser (0-50 mL)

1 mL and 5 mL pipettes

Vortex (automatic shaker)

centrifuge to 3,000 rpm

50 ° C water bath

glass funnels

filter paper

pH paper or pH probe

DI water

Steps:

1.0 Exchangeable/ Soluble Cations (F-1)

1.1 Mix each sample thoroughly to achieve homogeneity. For each digestion batch, a minimum of one sample should be duplicated and one NIST Standard Soil or

- other repeated sample should be included for every 20 samples. Samples may be finely ground or sieved to < 2mm. Sieve preparation may result in more floating (lost during procedure) organic matter.
- 1.18 Weigh sample to the nearest 0.01 g and transfer to a centrifuge tube 2.5 g of sample.

 Record the weights of the sample, tube and cap all together.
- 1.2 Alternatively, weigh and record the empty tube and cap, and then the sample, cap, and tube together.
- 1.3 Pouring down the side of the centrifuge tube, add 25 mL of 1 M MgCl₂ to each tube. Vortex samples for complete mixing.
- 1.4 Shake 2 hours on the reciprocating shaker. Use caution that the same approximate time is used throughout the procedure.
- 1.45 Centrifuge 2,000-3,000 rpm for 10 minutes. Watch the bottoms of the tubes. They may dimple. If necessary, the centrifuge can be run at lower rpms for a longer time, as long as the total is approximately 30,000 g-minutes.
- 1.5. Using funnels, separate supernatant solution into new, labeled vial (**F-1a** for the first run; **F-1b** for the repeated run). Use filter paper if necessary to separate floating organic matter.
- 1.6 For the original sample, repeat steps 1.2-1.5.

2.0 Carbonate Bound (F-2)

- 2.1 Pouring down the side of the centrifuge tube, add 25 mL of 1 M NaOAc (pH 5) to each sample.
- 2.2 Shake 2 hours on the reciprocating shaker.
- 2.25 Centrifuge at 2,000-3,000 rpm for 10 minutes.
- 2.3 Measure pH with pH paper or probe.
- 2.4 With funnels, separate supernatant solution into new, labeled vials (**F-2a** for the first run; **F-2b** for the repeated run). Use filter paper if necessary to separate floating organic matter.
- 2.5 Weigh and record the original sample with the tube and cap.
- 2.6 If pH is < 6, go to 3.0. If pH is > 6.0, repeat steps 2.1-2.5.

***when stopping for the evening, remove supernatant samples, including original soil tubes, to dark, cold room (40 C is preferable).

3.0 Oxide Bound (F-3)

- 3.1 Pouring down the side of the centrifuge tube, add 25 mL of 0.4 M NH₂OH-HCl (in 25% Acetic Acid).
- 3.2 Shake 2 hours on the reciprocating shaker.
- 3.25 Centrifuge at 2,000-3,000 rpm for 10 minutes.
- 3.3 With funnels, separate supernatant solution into new, labeled vials (**F-3a** for the first run; **F-3b** for the repeated run). Use filter paper if necessary to separate floating organic matter.
- 3.4 Weigh and record the original sample with the tube and cap.
- 3.5 Repeat steps 3.1-3.4.

4.0 Organic Bound (F-4)

- 4.1 Pouring down the side of the centrifuge tube, add 5 mL of 0.1 M HNO₃, then 1 mL of 30% of H₂O₂.
- 4.2 Vortex mix, then place the cap loosely on the tube and allow to stand several hours. If overnight, leave samples at room temperature and not in cold room.
- 4.3 Add additional 1 mL of 30% H₂O₂. When effervescence ceases, place tube in a beaker with water and heat at 50 o C until bubbles disappear. This can take upwards of an hour.
- 4.4 Add 20 mL of DI water.
- 4.5 Centrifuge (2,000-3,000 rpm for 10 minutes).
- 4.55 Using funnels, separate and save supernatant solution into new **F-4** marked vials. Filters are probably not necessary by this point.
- 4.6 Weigh and record the tube, cap and sample.

5.0 Residual Fraction (F-5)

5.1 Conduct 'Total' Metal Analysis beginning on step 2.

This method is adapted from EPA Method 3050, HNO₃/ H₂O₂ Acid Digestion.

- 5.15 Use DI or RO water to rinse sample from centrifuge tube into little aluminum bucket.
- 5.18 Set in oven at 110 ° C to dry until no water is present.
- 5.2 (same as step 2, TMA) Add 10 mL of 1:1 HNO3 to the sample.

Heat the sample to 95 ° C and reflux for 15 minutes without boiling.

Add 5 mL of concentrated HNO₃.

Reflux for 30 minutes.

Add 5 more mL of concentrated HNO₃ and reflux for 30 more minutes.

(This is to ensure complete oxidation).

Allow the solution to evaporate to 15 ml.

Note: 5 mL of concentrated HNO₃ may be added instead of 10 ml of 1:1 HNO₃. However, in some samples with high organic matter this results in a very vigorous reaction and the sample may overflow the tube. Evaporation of the excess water and the corresponding reduction in volume helps prevent loss of sample from excessive frothing when the peroxide is added in step 3. It is not absolutely necessary to evaporate the water but extra care is needed in step 3.

5.3 (TMA step 3) After the sample has cooled, add 1 ml of 30% H₂O₂.

Return the tube to the hot plate for warming and to start the peroxide reaction.

Care must be taken that losses do not occur due to excessively vigorous effervescence.

Heat until effervescence subsides.

Remove the tube from the hot plate.

Note: For samples with apparently high organic matter, it may be advantageous to reduce the aliquot volume of H2O2 to 0.5 ml. This will help prevent sample loss by effervescence. It is also sometimes helpful to allow the samples to stand at room temperature for several hours or overnight after the first peroxide addition. Then place them on the hot plate. This will decrease the speed of the reaction and lessen the chances of sample loss.

- 5.4 (TMA step 4) Continue to add 30% H₂O₂ in 1-ml aliquots with warming until the effervescence is minimal or until the general sample appearance is unchanged.
 Note: Do not add more than a total of 10 ml 30% H₂O₂.
- 5.5 (TMA step 5) Dilute the sample to 50 ml in the folin tube.
- 5.6 (TMA step 6) Particulates in the digestate that may clog the nebulizer should be removed by centrifugation at 2,000-3,000 rpm for 10 minutes or by filtration.
- 5.7 (TMA step 7) The diluted sample has an approximate acid concentration of 5.0% (v/v) HNO₃. The sample is now ready for analysis.

APPENDIX B

Poison Canyon study site description and data collection

VEGETATION ON URANIUM MINES IN THE POISON CANYON AREA, AMBROSIA LAKE, NM

Goal

The objective of this investigation was to find locations (natural or old mines) with high uranium concentration in this area southeast of Ambrosia Lake and northwest of Grants, New Mexico. Soils and plants would then be sampled in these high uranium areas.

This area was the first discovered and may have been the first abandoned during the uranium boom and bust of the 1960's through the early 1980's. As potentially some of the first abandoned uranium mining areas, some of these old mine sites may have had a larger vegetative recovery and possibly exhibit more plant diversity. Occurence of new, previously uninvestigated plant species could possibly yield a new native phytoaccumulator of uranium in semi-arid soils.

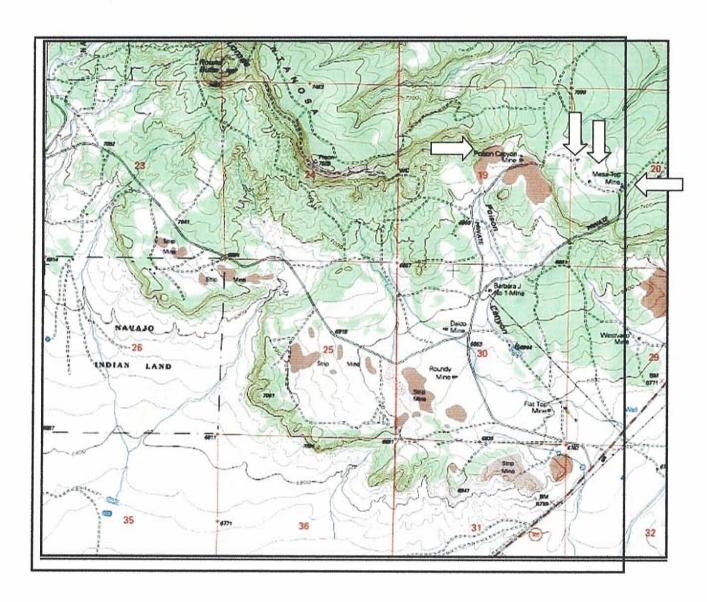
Methods

A gamma ray counter, GPS unit, and camera were used to identify and describe each site. Plant samples were taken and pressed in newspaper within 12 hours of sampling.

Results

Four mine sites were investigated: the Mesa top mine, two unnamed mines, and two adjacent Poison Canyon mine sites. GPS coordinates (in the UTM projection, NAD 1927 datum) for one corner of three areas are listed below.

Mine Site	Northing	Easting	corner
Mesa Top mine	13S02433920	3914189	southeast
unnamed	13S0243684	3914455	northeast
Poison Canyon S	13S0242835	3914524	south-southwest



A. The Mesa top mine had an extent of approximately 250 m by 400 m. The entire area sloped approximately 15 degrees to the northwest. It contained numerous little mounds of mixed tailings and ore/ waste rock. There was also one 3 m high waste rock pile, one iron mine ventilation shaft, one open adit (poorly fenced), and some scattered

wood and metal machine parts. The waste rock was an yellow-orange sandstone, and the ore a fine white-gray ash-like powder. Uranium readings in the area read ~10 uRem/ hr or less background; ~ 20 uRem/ hr around the edges; and 50-200 uRem/ hr within the mine area. Not all mounds had high readings, nor was there an obvious pattern between the mounds. One area approximately 2 m x 10 m had a high reading, of up to 400 uRem/ hr. This area was in a sandy arroyo 1 m deep running southwest downslope from the northeast corner of the mine. The area was also downslope of the old headframe and open pit. This area was not noticably vegetated.



Enhanced picture of Mesa Top mine, Poison Canyon area. Dog for scale is obscured in Pinon tree in right-center of picture.

There are quite a few Pinon and Juniper trees growing within the old mine site. While there are a few Indian Rice grass plants growing on the piles, there is a low grass species diversity across the area. Black and Blue grama grasses predominate, and ~20 - 30% of the soil surface is covered with vegetation. Opuntia cacti, Blazing star (stickleaf) and Muhly grass were also noted at the site, but low-growing shrubs such as snakeweed,

rabbitbrush or winterfat were absent. Anecdotal new species at this mine site are reported in the table below. Pictures, but no samples, were taken at this site.

Common name	<u>Species</u>	<u>notes</u>
Pine Spiderwort	Tradescanta pinetorum	unusual for area
Four-o-clock	Mirabilis multiflora	low-growing form
Spiny bush	Tetradymia spinosa	leaves in clumps on stem
Sanvitalia	S. abertii	<10 cm tall
Annual goldenweed	Machaeranthera gracilis	abundant
Spurge or Rattlesnake weed	Chamaesyce albomarginata	succulent leaves

B. The next two mine sites were located between the two named mines. The first unnamed mine site is approximately 75 x 75 m. A middle disturbed plain is surrounded by 2-3 x 2-3 x 1-2 m waste piles, with a small arroyo draining the area to the north. Uranium readings were 200-300 uRem/ hr over much of this site. In the 50 cm deep arroyo, outside of the main mine area, 100+ uRem/ hr was recorded. Vegetation in this area was not terribly diverse. Black grama and fourwing saltbush predominated, with some Indian rice grass, one annual Goldenweed, the same Spiny bush, and dead or tiny Snakeweed. One large Pinon tree grew on the west side of the mine (@ 100 uRem/ hr). Nine plant and three soil samples were taken at this site, but no pictures.

Common name	<u>Species</u>	U (uREm/hr)	notes
Four o'clock		90	also surface soil sample
Fourwing saltbush	Atriplex canescens	~800	also surface soil sample
Black grama		625	also surface soil sample
Hilaria		240	southeast mine
Sand dropseed	Sporobolus cryptandrus	200	southeast mine
Spiny bush		60	southwest mine
Pinon	Pinus edulis	100	southwest mine
XXXa		60	southeast of mine proper

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- C. This mine site was very small (30 x30 m) and probably consisted of waste rock drilled up for a ventilation shaft and dumped on the surface. The uranium readings were barely above background (20uRem/hr) and no vegetation was collected.
- D. There are two mine sites at the Poison Canyon mine location. The first site is much larger, at least 600 m long by 400 m wide. This site was all tailings that had been formed into a relatively flat plain. There were three 15 m x 15 m tanks at low points within this plain. All of the material was white powder and sand. The average uranium reading in this area was 30 uRem/ hr, with a range of 10-60 uRem/ hr. Minor arroyos and the tanks were not necessarily high points. The few high points (60) were apparently randomly distributed. Vegetation covered 10% or less of the surface and was not diverse. Primarily there was a grazed and short probably seeded grass, probably Kentucky bluegrass (*Poa praetensis*). Healthy Fourwing saltbushes also covered the site, but nothing else except a few small Indian rice grasses.



View from above of first Poison Canyon site. Note extent of disturbed area, lack of vegetation, and telephone poles for scale.

The second site at the Poison Canyon location includes a large mine pile (20 x 80 x 4 m) and three small depressions (10x 10m) adjacent to a cliff-forming sandstone. The site is much smaller, possibly up to 100 m x 250 m. The average uranium reading is 50 +/- 20 uRem/ hr. Some areas of outcrop, drainage and plain are up to 80 uRem/ hr--but it is spatially variable and not consistent w/in the landscape. One 30 cm square spot held up to 300 uRem/ hr. This spot was unvegetated and otherwise completely unremarkable. The outcrop itself was also within this uranium reading range (30-70 uRem/ hr). The site was generally predominated by Grama grasses and Fourwing saltbush. There were a few Indian rice grass, Annual Goldenweed, and Stemless Evening Primrose at this site as well as some New Mexico sunflowers, but not at significant levels of uranium concentration.



Second Poison Canyon mine location. Note telephone pole for scale, and waste pile. The waste pile obscures two small ponds between the outcrop and the pile.

ICP-MS Uranium Concentrations

At Poison Canyon, plants were sampled relative to Field gamma ray meter readings. Three soil samples were taken at the locations shown on figure __. Of the samples listed in Table __.

	Avg Plant U	Stdev
Brickel Bush	1.81	1.77
Big Leaf	1.47	
Pinon Pine	2.04	0.21
Saltbush	11.15	0.50
Pofe	0.99	0.58
Black grama	0.61	
Nyctag	1.295	0.76
5	0.76	
Tobosa Grass	2.27	
Oxalis	7.6	
<u>Point</u>	Soil U (ppm)	<u>stdev</u>
T1	1921.1	13.9
T2	236.2	27.9
Т3	191.5	27.3

Table __. ICP-MS Uranium content of plant and soil samples, Poison Canyon.

Discussion and Conclusion

The goal of this field investigation was to identify whether new and different plants grew on high uranium areas in Poison Canyon. Single or rare occurrences of plant species new to this study have been identified here. However, these mines, at different stages of being grown over, did not exhibit first-order differences in vegetation cover from the other two sites (with the exception of the Pinon-Juniper). Any first order differences were more in missing species diversity instead of additional diversity. These sites had no Russian thistle, Kochia, Snakeweed, Winterfat, little Rabbitbrush, and very little grass diversity.

Additional areas could be investigated, as outlined in the appendix. However, it is likely that these areas experienced disturbance at the same time as the mines investigated here, and in mining the same geologic units. Therefore, one might expect the same vegetation at additional sites in the immediate area.

Appendix

Land access permission was obtained from the Schmitt brothers, especially Bob Schmitt, 505-287-2266. Bob Schmitt and Terry Fletcher also provided instructions as to where to look in Poison Canyon. Paula Watt, Earth Science Instructor for UNM-Gallup, provided initial field suggestions (pwatt@gallup.unm.edu). Her suggested location was not apparent until the end of the field session.

She suggested looking for a noticeable landmark rock spinnacle on the left at the mouth of Poison Canyon. This was as one entered a private land from the south via a gully. In the lower part of the outcrop on the left side of the mouth of Poison Canyon, there are areas of low grade uraninite and pitchblende in sandstone. Adits and shafts and associated activity in the lower part of the canyon are all covered over. Higher in the geologic section, there is an oxidized zone with autinite as the principal uranium-bearing member. In this flat area, there is a short adit. Paula Watt suggested that there might be high readings for a small area surrounding this adit.

This adit is upslope stratigraphically and topographically from the rock spinnacle. It is in the Red Brushy Basin (RBB) member of the Morrison formation. The RBB also has uranium minerals that will fluoresce with black light (in the adit, where natural light is diffused). This rock spinnacle is visible from the Poison Canyon mine. It is 1 mile

west. The mesa top where Paula Watt's suggested adit is found is not marked as having a mine; it should be stratigraphically similar with the Mesa top mine that was investigated here. Paula Watt also suggested that carnotite could be found in the Todilto Formation Limestone, on the other side of a faint dirt road.

APPENDIX C

Grid Layout Description

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100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 </td><td> 1 </td><td> 1 </td><td> Total Color March March</td><td> 1 </td><td> </td><td> 1 </td><td> 1. </td><td> </td><td> The column The</td></td></td></td></td> | 52 -107/788507 55.4107285 107 46 36.7 35 24 38.62 13S 24/790 3922184 13S 2478398 3921881.25 53 -107/786357 35.4102325 107 46 36.81 35 24 36.81 13S 247780 3922054 13S 2478298 3921830.25 54 -107/786947 35.4093127 107 46 37.01 35 24 35.18 13S 247780 3922034 13S 2478298 3921830.25 55 -107/786377 35.4093437 107 46 52.83 35 24 33.61 13S 247430 3921994 13S 2478298 3921830.25 55 -107/786373 35.4093475 107 46 52.83 35 24 33.61 13S 247480 3921994 13S 2478298 3921790,25 57 -107/780873 35.4093475 107 46 48.85 35 24 33.61 <td>21 -107/70809 33411106Z 107 46 36.73 35 24 40.27 123 247/790 3922140 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100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 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107 46 38.47 35 24 40.17 135 247740 3922240 135 247788 3921852.25 46 -10777868 35.411625 107 46 38.47 35 24 43.19 135 247740 3922240 135 247788 3921852.25 51 -10777680 35.409737 35 107 46 38.47 35 24 43.59 135 247780 3922240 135 247788 3921852.25 52 -10777680 35.409737 35 107 46 38.49 35 24 43.59 135 247780 3922280 135 247789 3921852.25 52 -10777680 35.409737 107 46 38.49 35 24 43.59 135 247780 3922280 135 247789 3921852.25 53 -10777680 35.409737 107 46 38.49 35 24 43.59 135 247780 3922280 135 247789 3921852.25 54 -10777680 35.409737 107 46 38.49 35 24 33.69 135 247789 </td><td> 1077782810 35.411040 107 46 42.75 35 24 40.11 135 247640 3922190 135 247698 3921986.25 35</td><td> 23 1017718443 154 154 155 247660 292240 155 247698 29226525 23 1017718516 25410679 107 46 42,75 25 24 41,4 155 247640 292219 155 247698 29218525 23 1017718516 25410679 107 46 42,58 23 24 25 24 24 25 24 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 2</td><td> 10177184578 354129712 107</td><td> 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100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 </td><td> 1 </td><td> 1 </td><td> Total Color March March</td><td> 1 </td><td> </td><td> 1 </td><td> 1. </td><td> </td><td> The column The</td></td> | 45 -107.77142 35.4107056 107 46 38.71 35 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354129712 107 | 10177790146 254120545 107 | The contribute Schling Column C | 22 | | 25 | Text Text | Text Text | 22 1017796402 54410725 107 | 21 | 20 | 10.1017/99/11/2 53.11/2002 1077 46. 46.75 58. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 24. 25. 24. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 24. 24. 25. 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107 64 46.5 35 24 25 25 25 25 25 25 2 | 1. | 1. | 1 1 1 1 1 1 1 1 1 1 | 10 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100 100
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APPENDIX D

Laboratory Soil Analyses Data

	A	В	С	D	Е	F	G	Н
1			Sec 27 sam	ples analyze	d by 400 d	oven, 120 min		
2								
3		sample #	<u>% OC</u>	<u>stdev</u>		sample #	<u>% OC</u>	<u>stdev</u>
4		1-0	3.89			-A1	2.31	
5		1-5				A1	1.99	0.15
6		1- 10	3.95			A3	2.97	
7		1- 15	3.68			A5		
8		1-20				-C1	2.20	
9		1-25				C1	1.12	0.00
10		1-30	3.41			C3	5.23	
11		2-0	0.73			C5	3.06	
12		2-5	0.69			-E1	3.58	
13		2-10	0.59	0.18		E1	0.46	
14		2- 15	0.71			E3	1.12	
15		2-20	0.86			E5	1.98	
16		2- 25	0.66			-G1	1.79	
17		2-30	0.72	0.24		G1	0.55	
18		3-0	0.59			G3	0.90	0.18
19		3-5				G5	1.81	
20		3-10	0.70	0.12		B2	2.80	
21		3- 15				D2	1.47	0.05
22		3-20	0.69			F2	0.37	0.03
23	·	3- 25	0.77			H2	0.39	
24		3-30	0.37	0.52		B4	2.67	
25						C4	0.77	
26						D4	0.24	
27						F4	2.72	
28	· · · · · · · · · · · · · · · · · · ·					H4	1.69	

R	20%	ifter 400	5.47	1.89	1.65	1.65	1.52	1.46	0.57	2.80	3.12	2.10	2.17	0.17				
0		Depth			7				49		70							
P		Pit#	-		_		_			1	-	2	7					
0		locu	27?	36	36	36	36	36	36	36	36	36	36	blank				
Z																		
M	20 %	fter 400	1.75	1.25	40 1.08	1.18	1.16	1.52	7.48	5.25	4.35	4.50	4.34	4.30	3.77	0.10		
L		Depth	20	30	40	40	20	09	10	20	30	40	50	09	70			
K		Pit#	2	2	2	2	2	2	3	3	3	3	m	3	3			
J		locu	36	36	36	36	36	36	36	36	36	36	36	36	36	blank		
I																		
H	% OC loss	after 400	2.79	3.54	2.45	1.58	3.94	2.51	2.31	3.90	2.92	2.24	5.18	3.09	2.22	80.0		
G		Point	Al	A2	A3	B1	B2	B3	CI	CZ	ຮ	DI	D2	D3	C1 dub			
Ŧ		locu	36	36	36	36	36	36	36	36	36	36	36	36	36	blank		
E									THE A STORY STATE THE STREET, AND THE STREET,				THE PROPERTY OF THE PROPERTY O					
D	% OC loss	after 400	2.16	2.81	4.56	2.27	2.51	2.46	1.98	3.00	2.34	3.02	1.38	5.47	89.9	0.00	1.52	
С			E1	E2	E3	F1	F2	33	GI	C5	33	HI	H2	H3	H3 dup		A5	
В			36	36	36	36	36	36	36	36	36	36	36	36	36	BLANK	27	
	3	4	5	9	7	8	6	10	Ξ	12	13	14	15	16	17	18	19	20

	K	L	M	N
20		<u> </u>	IVI	IN BÁS
28	400 for 12		1	
29	5.47	27	11	20
30	1.52	27	A5	
31	1.89	36	1	0
32	1.65	36	1	7
33	1.65	36	1	21
34	1.52	36	1	35
35	1.46	36	1	35 dup
36	0.57	36	1	49
37	2.80	36	1	60
38	3.12	36	1	70
39	2.10	36	2	00
40	2.17	36	2	10
41	1.75	36	2	20
42	1.25	36	2	30
43	1.08	36	2	40
44	1.18	36	2	40 dup
45	1.16	36	2	50
46	1.52	36	2	60
47	7.48	36	3	10
48	5.25	36	3	20
49	4.35	36	3	30
50	4.50	36	3	40
51	4.34	36	3	50
52	4.30	36	3	60
53	3.77	36	3	70
54	2.79	36	A1	
55	3.54	36	A2	
56	2.45	36	A3	
57	1.58	36	B1	
58	3.94	36	B2	
59	2.51	36	B3	
60	2.31	36	C1	
61	2.22	36	C1 dup	
62	3.90	36	C2	
63	2.92	36	C3	
64	2.24	36	D1	****
65	5.18	36	D2	
66	3.09	36	D3	
67	2.16	36	E1	
68	2.81	36	E2	
69	4.56	36	E3	
70	2.27	36	F1	
71	2.51	36	F2	
72	2.46	36	F3	
73	1.98	36	G1	
74		36		
75	3.00 2.34		G2	
_		36	G3	
76	3.02	36	HI	
77	1.38	36	H2	
78	5.47	36	H3	
79	6.68	36	H3	
80	0.10	blank		
81	0.00	blank		
82	0.08	BLANK	· I	
83	0.17	blank		

	A	В	С	D	Е	F	G	Н	I	J	K	L
T		Chittick M	leasuremen	t of Section	27 Surface	Soil Carb	onate					
2				Sample	CO2			Correction		w/barometric		
3			Dish	Wt.	Evolved	Temp.	Pressure	Factor	CaCO3	pressure		
4	Date	Label	#	(g)	(ml)	(C)	(inches)		(%)	adjustment		
5									=((0.3866*H5*E5)/D5)	=((I5)-1.7381)/0.8797	Point	Average
6	29-May-02	Al-	33k	5.5609	30	25.5	30.08	1.0288	2.15	0.46		
7	30-May-02	A1-		5,5028	33	27	30	1.01741	2.36	0,71		
8	30-May-02	Al		7.5656	63	28	30	1.01741	3.28	1.75		
9	29-May-02	Al	681	7.1368	52	27	30.08	1.02018	2.87	1.29		
10	29-May-02	A3	608	6.2483	19	25.5	29.97	1.02323	1.20	-0.61		
11	30-May-02	A3		6.6105	30	27	30	1.01741	1.79	0.05	Al-	0.706
12	29-May-02	B2	619	5.4061	32	25.5	30.08	1.0288	2,35	0.70	Al	1.747
13	30-May-02	B2		5.5893	35	25.5	30	1.026	2,48	0.85	A3	0.533
14	29-May-02	B4	634	5.4803	33	26	30.08	1.02594	2,39	0.74	B2	0.848
15	30-May-02	B4		5.4827	40	25.5	30	1.026	2.89	1.31	B4	1.314
16	29-May-02	Cl	640	6.1190	31	25	29.97	1.02626	2.01	0.31	-cl	1.24
17	27-Jun-02	C1	616	19.001	100	27.5	30	1.0145	2.06	0.37	cl	0.37
18	29-May-02	C1-	635	4.5803	22	25	30.08	1.02594	1,91	0.19	c3	0.00
19	27-Jun-02	C1-	215	15.1004	109	27.5	30	1.01450	2.83	1.24	c4	1.09
20	29-May-02	C3	653	6.0849	24	25.5	29.97	1.02323	1,56	-0.20	c5	2.63
21	27-Jun-02	c3	624	5.7578	23	25.5	30	1.026	1,58	-0.17	d2	0.00
22	29-May-02	C4	616	8.4059	46	26	30.08	1.02594	2.17	0.49	d4	0.40
23	27-Jun-02	c4	620	8.6412	59	26.5	30.08	1.02306	2.70	1.09	E1-	1.601
24	29-May-02	C5	620	3.5653	24	26	30.08	1.02594	2.67	1.06	El-	0.368
25	27-Jun-02	c5	640	3.5344	36	25.5	30,08	1.0288	4,05	2,63	E3	1.606
26	29-May-02	D2	624	7.1938	23	26	30.08	1.02594	1,27	-0.53	E5	3,49
27	27-Jun-02	d2	33k	7.1427	25	25.5	30	1.02318	1,38	-0.40	F2	1.605
28	29-May-02	D4	621	4.4022	27	25.5	29.97	1.02323	2.43	0.78	F4	1.864
29	27-Jun-02	d4	634	13.4246	71	26.5	30.08	1.02306	2.09	0.40	G1-	-0.1302
30	30-May-02	El-		6,3995	48	26	30	1.02318	2.97	1.4	G1	1.285
31	30-May-02	El-		6,0641	51	27	30	1.02318	3.33	1.81	G3	1.915
32	30-May-02	El		8.2937	42	26	30	1.02318	2	0.3	G5	3.779
33	30-May-02	E1		8.3917	45	26	30	1.02318	2.12	0.44	H2	0.56
34	30-May-02	E3		8.9569	72	27	30	1.02318	3.18	1.64	H4	1.79
35	30-May-02	E3		8.8693	70	27	30	1.02318	3.12	1.57		
36	30-May-02	E5		6.2975	68	27	30	1,02318	4.27	2.88		
37	30-May-02	E5		6.2949	85	27	30	1.02318	5.34	4.1		
38	7-Feb-03	E5		4.8383	57	25.5	29.86	1.02047				
39	30-May-02	F2		10.1845	81	27	30	1.02318	3.15	1.6	<u> </u>	
40	30-May-02	F2		9.908	79	27	30	1.02318	3.15	1.61		
41	30-May-02	F4		6.2324	56	27	30	1.02318	3.55	2.06	l	
42	30-May-02	F4		5.561	45	26	30	1.02318	3.2	1.66		
43	30-May-02	G1-		6.6714	21	26	30	1.02318	1.25	-0.56		
44	30-May-02	G1-		6.7179	34	26	30	1.02318	2	0.3		
45	30-May-02	GI		8.5257	59	27	30	1.02318	2.74	1.14		
46	30-May-02	G1		8.0456	61	27	30	1.02318	3	1.43		
47	30-May-02	G3		7.7863	69	27	30	1.02318	3.51	2.01		
48	30-May-02	G3		7.3443	62	27	30	1.02318	3,34	1.82		
49	30-May-02	G5		6.8245	86	26.5	30	1.026	5	3.71		
50	30-May-02	G5		7.1182	92	26.5	30	1.026	5,13	3.85		
51	7-Feb-03	G5		7.1602	98	27	29.86	1.01188				
52	30-May-02	H2		7.8883	44	25,5	30	1.026	2.21	0.54		
53	30-May-02	H2		8.1128	46	25.5	30	1.026	2.25	0.58		
54	30-May-02	H4		6.8541	58	26.5	30	1.026	3.36	1.84		
55	30-May-02	H4		6.7966	56	26.5	30	1.026	3.27	1.74		
-												

z		-	ent values				STDEV																0.36	and deline the second of the s	0.15			0.11			0.21	0.33					
M		•	***barom. pres adjustment values				Average		0		0	0			0		2.35	2.75	0.73	0.18	0.36	0	0.25		1:1			0.75			1.54	0.4143	0.88				
T		1	***barom. p				Point		1-0	1-5	1-10	1-15	1-20	1-25	1-30		2-0	2-5	2-10	2-15	2-20	2-25	2-30		3-0	3-5		3-10	3-15		3-20	3-25	3-30				
区																																					
J		CO3	w/barometric	pressure	adjustment	=((16)-1.7381)/0.8797	-0.75	-0.74		-1.05	-1.06	-0.91	-0.83		-0.99		2.35	2.75	0.73	0.18	0.36	0.17	-0.07	-0.25	0.00	0.50	0.97	1.18	A Armenda de Armenda de Armenda de Armenda de Maria de Maria de Armenda de la Carte de Armenda de Armenda de A	0.84	69.0		1.39	1.69	0.65	0.18	0.88
1	ırbonate			CaCO3	(%)	=((0.3866*H6*E6)/D6)	1.08	1.08	1.26	0.81	0.81	0.94	1.01	1.17	0.87	1.30	3.81	4.15	2.38	1.90	2.06	1.89	1.68	1.52	1.73	2.18	2.59	2.78	3.09	2.48	2.35	2.90	2.96	3.23	2.31	1.89	2.51
Н	Soil Profile Carbonate		Correction	Factor			1.026	1.02318	1.02888	1.03444	1.03444	1.03723	1.03444	1.02608	1.03444	1.02888	1.01435	1.01435	1.02594	1.02594	1.03165	1.03165	1.03165	1.03165	1.03165	1.03165	1.02594	1.02594	1.02329	1.02594	1.03165	1.02329	1.02594	1.02306	1.02880	1.02880	1.01727
G				Pressure	(inches)		29.95	29.95	29.86	30.05	30.05	30.05	30.05	29.86	30.05	29.86	30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05	29.86	30.05	30.05	29.86	30.05	30.05	30.05	30.05	30.05
F	Section 27			Temp.	(C)		25.5	26	24	24.5	24.5	24	24.5	24.5	24.5	24	28	28	26	56	25	25	25	25	25	25	56	26	25	26	25	25	26	26.5	25.5	25.5	27.5
E	ement of	000	C02	Evolved	(ml)		17	17	22	11	11	14	15	21	26	18	160	189	88	65	35	35	30	29	33	41	09	29	99	52	48	28	58	65	46	38	103
D	Chittick Measurement of S		Sample	Wt.	(g)		6.2332	6.2050	6.9703	5.3994	5.4380	5.9818	5.9394	7.1157	11.9381	5.5101	16.4868	17.8414	14.6893	13.5630	6.7888	7.3968	7.1184	7.6222	7.5891	7.4962	9.1759	9.5666	8.7048	8.3193	8.1581	7.9191	7.7716	7.9676	7.9181	7.9778	16.1435
C	Chittick		Dish	#			32k	621		38f	8k	2a	ca		13a	47	113	112	9k	009	24f	9a	999	672	78	80	9/9	643		700	693		614	688	626	296	he
В			Label				1-0	1-0	1-05	1-10	1-10	1-15	1-15	1-25	1-30	1-30	2-0	2-5	2-10	2-15	2-20	2-20	2-25	2-25	2-30	2-30	3-0	3-0	3-5	3-10	3-10	3-15	3-20	3-20	3-25	3-25	3-30
A				Date			27-Jun-02	27-Jun-02	7-Feb-03	27-Jun-02	27-Jun-02	27-Jun-02	27-Jun-02	7-Feb-03	27-Jun-02	7-Feb-03	27-Jun-02	27-Jun-02	27-Jun-02	27-Jun-02	27-Jun-02	7-Feb-03	27-Jun-02	27-Jun-02	7-Feb-03	27-Jun-02	27-Jun-02	27-Jun-02	27-Jun-02	27-Jun-02							
	1	7	3	4	5	9	7	∞	6	10	11	12	13	14	15	16	12	18	19	70	21	22	23	24	25	79	27	28	56	30	31	32	33	34	35	36	37

S27 profile carbonate

	02d
1000 to	02
in and	Ł'

Σ			003	w/barometric	pressure	adjustment	=((L7))/1.1708	1.55	4.32		2.74		1.54		2.92		1.81	5.83	5.90		4.36	0.69	5.50		2.06	5.14	2.33	2.76	1.20	1.22		0.40	3.38	0.48	5.36	0.38	1.50	0.34	5.68	1.32	1.08
					CaCO3	(%)	=(0.3866*K7*H7)/F7	1.81	5.05	6.17	3.21	3.28	1.80	2.25	3.42		2.12	6.83	6.91	6.98	5.10	0.81	6.44		2.41	6.02	2.73	3.23	1.40	1.43		0.46	3.95	0.57	6.28	0.45	1.76	0.40	6.65	1.55	1.26
Y				Correction	Factor			1.05103	1.04829	1.98429	1.04829	1.01188	1.04556	1.02329	1.04556		1.04556	1.03444	1.02594	1.02329	1.03444	1.05103	1.03444		1.04556	1.04003	1.04556	1.04282	1.05103	1.05103		1.05103	1.03723	1.04829	1.02594	1.04829	1.04829	1.04829	1.03165	1.04829	1.04829
٦					Pressure	(inches)		30.05	30.05	29.86	30.05	29.86	30.05	29.86	30.05		30.05	30.05	30.05	29.86	30.05	30.05	30.05		30.05	30.05	30.05	30.05	30.05	30.05		30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05	30.05
_					Temp.	(၁)		21.5	22	26	22	27	22.5	25	22.5		22.5	24.5	26	25	24.5	21.5	24.5		22.5	23.5	22.5	23	21.5	21.5		21.5	24	22	26	22	22	22	25	22	22
I				C02	Evolved	(lm)		42	84	59	75	100	54	37	82		56	175	190	75	165	15	170		70	135	70	85	30	39		10	103	14	200	11	43	10	157	30	26
ŋ	onate				acid level			10	10	10	10	10	10	10	10		10	10	10.5	10	10	14	10		10.5	10	10	10	10	10.5		10	10.8	10	8.5	10.5	10	10	10	11	10
ı.	Surface Carbonate			Sample	Wt.	(b)		9.4262	6.7345	7.3359	9.4596	11.9114	12.0979	6.4995	9.6931		10.6563	10.2541	10.9044	4.2515	12.9316	7.5407	10.564		11.7574	9.0209	10.3557	10.6228	8.7121	11.0647		8.7777	10.4502	10.0211	12.6379	9.896	9.9203	10.2099	9.421	7.8551	8.3593
Е	on 36 Sur		sample	and dish	wt	(a)		11.215	8.5472	9.1435	11.257	13.7094	13.9299	8.2766	11.4862		12.4449	12.0895	12.6957	6.0691	14.7729	9.3197	12.4175		13.5521	10.8153	12.1646	12.4118	10.49	12.8683		10.5803	12.2234	11.8262	14.4207	11.659	11.6967	12.0036	11.2095	9.6262	10.1566
B C D E	nent of Section	THE PARTY OF THE P		tub wt				1.7888	1.8127	1.8076	1.7974	1.798	1.832	1.7771	1.7931		1.7886	1.8354	1.7913	1.8176	1.8413	1.779	1.8535		1.7947	1.7944	1.8089	1.789	1.7779	1.8036		1.8026	1.7732	1.8051	1.7828	1.763	1.7764	1.7937	1.7885	1.7711	1.7973
၁	Neasuren			dish wt		(g)		A1	A2	A2	A3	A3	B1	B1	B2		B3	Շ	ပ	ပ	C5	ငဒ	D1		D2	D3	E1	回	E2	E3		Σ	F2	F3	G1	G 2	63	H	H2	H3	H3
В	Chittick			Sample	Number			101	102		103		104		105		106	107	dnp		108	109	110		111	112	113	dnp	114	115		116	117	118	119	120	121	122	123	124	dnp
Α					Date			2-Nov-02	2-Nov-02	7-Feb-03	2-Nov-02	7-Feb-03	2-Nov-02	7-Feb-03	2-Nov-02		2-Nov-02	2-Nov-02	2-Nov-02	7-Feb-03	2-Nov-02	2-Nov-02	2-Nov-02		2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02		2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02	2-Nov-02
	-	2	က	4	2	9	7	8	6	10	7	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36			40		42

chittick_1

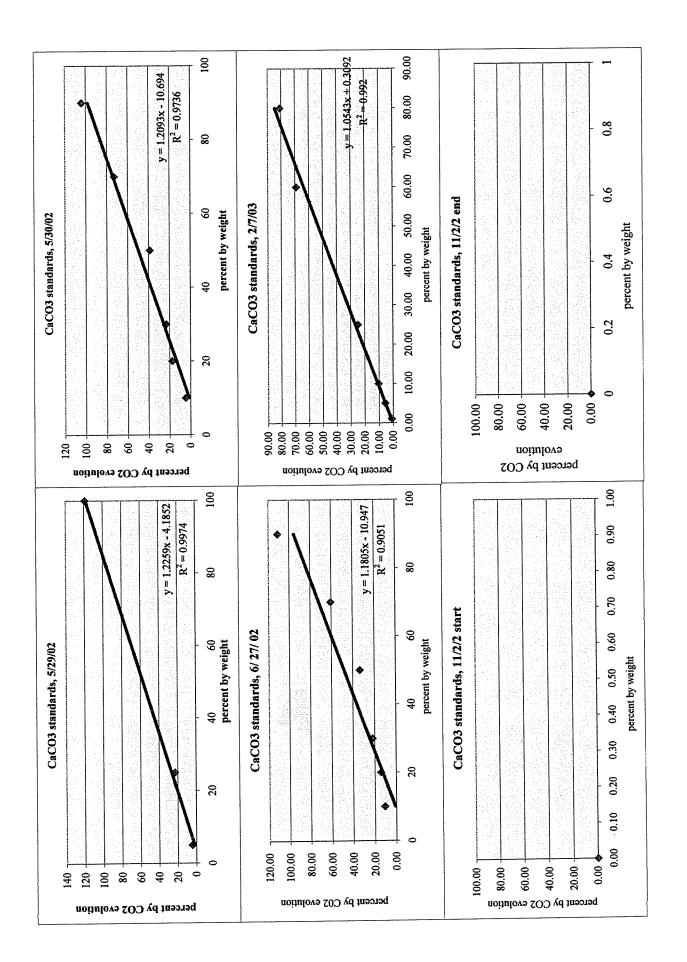
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A B C	D 8	0			E	± ::	9	H		ſ	쏘	-	Σ	z
Chittick Measurement of Section 36	Chittick Measurement of Section 3	Measurement of Section 3	nent of Section 3	ection 3	اند	Soil Pro	Soil Profile Carbonate	onate						Administration
						sample								CO3
Locn tub wt	Locn tub wt	tub wt	tub wt		O	and dish	Sample		C02			Correction		w/barometric
Date Number 36-soil pit depth	Number 36-soil pit depth	pit depth				wt	Wt.	acid level	Evolved	Temp.	Pressure	Factor	CaCO3	pressure
(b)						(g)	(g)		(lm)	(၁)	(inches)		(%)	adjustment
							=F6-E6						=(0.3866*L6*16)/G6	=((M6))/1.1708
2-Nov-02 80 1 0 1.8624 21.3	80 1 1 0 1.8624	1.8624	1.8624		21.2	21.2027	19.3403	11	48	22	30.06	1.04829	1.01	0.86
81 1 7 1.8302	81 1 7 1.8302	1.8302	1.8302		19.6	3309	17.8007	10	37	22	30.06	1.04829	0.84	0.72
82 1 21 1.8234	82 1 21 1.8234	1.8234	1.8234		20.6	272	18.8038	10	4	21	30.06	1.05376	60.0	0.07
1.8499	83 1 35 1.8499	1.8499	1.8499		22.00)74	20.1575	10	3	21	30.06	1.05376	0.06	0.05
84 1 49 1.8869	84 1 49 1.8869	1.8869	1.8869		19.96	372	18.0803	10	4	21.5	30.06	1.05103	0.09	0.08
85 1 60 1.781	85 1 60 1.781	1.781	1.781		19.00	83	17.2271	10.5	24	21.5	30.06	1.05103	0.57	0.48
1 70 1.7925	86 1 70 1.7925	1.7925	1.7925		22.51	26	20.7231	5	200	25.5	30.06	1.0288	3.84	3.28
7-Feb-03 1 70 1.805 6.905	1 70 1.805	1.805	1.805	-	6.90	2	5.1	6.5	240	29	29.86	1.00024	18.20	15.54
87 2 0 1.843	87 2 0 1.843	0 1.843	1.843		21.98	2	20.139	10.5	ၑ	21.5	30.06	1.05103	0.12	0.10
10	88 2 10 1.8685	10 1.8685	1.8685		23.03	32	21.1677	10.5	8	21.5	30.06	1.05103	0.15	0.13
89 2 20 1.9309	89 2 20 1.9309	20 1.9309	1.9309		23.81	79	21.887	10	4	21	30.06	1.05376	0.07	0.06
2 30 1.9112	90 2 30 1.9112	30 1.9112	1.9112	-	24.33	03	22.4191	10	117	23	30.06	1.04282	2.10	1.80
91 2 40 1.8952	91 2 40 1.8952	40 1.8952	1.8952		27.6	899	25.7716	10	250	26	30.06	1.02594	3.85	3.29
2 40 1.7683	2 40 1.7683	40 1.7683	1.7683		7.02	19	5.2536	10	59	25.5	29.86	1.02047	4.43	3.78
92 2 50 1.8714	92 2 50 1.8714	50 1.8714	1.8714		26.06	363	24.1949	10	200	25	30.08	1.03165	3.30	2.82
2 50 1.7684	2 50 1.7684	50 1.7684	1.7684	-	7.39	တ	5.6306	10	81	26	29.86	1.01765	5.66	4.83
93 2 60 1.9098	93 2 60 1.9098	60 1.9098	1.9098		23.6	894	21.7796	10	200	25	30.06	1.03165	3.66	3.13
2 60 1.8182	2 60 1.8182	60 1.8182	1.8182		7.29	29(5.4785	10	148	28	29.86	1.00612	10.51	8.97
94 3 10 1.8342	94 3 10 1.8342	10 1.8342	1.8342		19.62	569	17.7927	10	81	21	30.06	1.05376	1.85	1.58
3 20	95 3 20 1.8887	20 1.8887	1.8887	-	20.36	290	18.478	10	15	21	30.06	1.05376	0.33	0.28
96 3 30 1.8669	96 3 30 1.8669	30 1.8669	1.8669	-	24.0	131	22.1462	10	15	21	30.06	1.05376	0.28	0.24
97 3 40 1.8662	97 3 40 1.8662	40 1.8662	1.8662	\vdash	21.	21.499	19.6328	10	29	21	30.06	1.05376	09:0	0.51
3 50 1.8538	98 3 50 1.8538	50 1.8538	1.8538	<u> </u>	22	22.8849	21.0311	12	48	21	30.06	1.05376	0.93	0.79
99 3 60 1.7714	99 3 60 1.7714	60 1.7714	1.7714	-	22.	2978	20.5264	10	88	22.5	30.06	1.04556	1.73	1.48
100 3 70 1.8584	100 3 70 1.8584	70 1.8584	1.8584		21.3	908	19.5222	10	111	23	30.06	1.04282	2.29	1.96

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	А	В	С	D
1	27	1	0	7.75
2	27	1	5	8
3	27	1	10	7.97
4	27	1	15	7.76
5	27 27	1	20	7.88
6	27	1	20	8.06
7	27	1	25	7.84
8	27	1	30	8.02
9				
10	27	2	0	7.64
11	27	2	5	7.75
12	27	2	15	7.75
13	27	2	25	7.67
14				
15	27	3	0	7.53
16	27	3	5	7.36
17	27	3	10	7.74
18	27	3	15	7.53
19	27	3	20	7.65
20	27	3	25	7.43
21	27	3	30	7.5
22				
23				
24	36	1	0	7.73
25	36	1	14	7.85
26	36	1	28	4.95
27	36	1	42	4.51
28	36	1	55	4.74
29	36	1	65	7.77
30				
31	36	2	0	7.7
32	36	2	5	7.72
33	36	2	20	8.12
34	36	2	40	8.32
35	36	2	55	8.35
36	36	2	55	8.39
37	36	2	65	8.4
38				
39	36	3	40	8
40	36	3	50	8.05
41	36	3	60	8.03
42	36	3	а	7.67
43	36	3	Bk	7.99
44				

PH

	Α	В	С
1	36	A1	7.63
3	36	A3	7.44
3	36	B1	7.58
4	36	B2	7.65
5		B3	7.42
6	36	C1	7.73
7	36	C1 C2	7.72
8	36	C3	7.02
9	36	D1	7.96
10	36	D3	7.33
11	36	E1	7.68
12	36	E2	7.47
12 13	36	E3	7.37
14	36		7.37
15	36		7.46
16	36		7.45
17	36		7.73
18	36		7.73
	36		
19			7.6
20	36	H1	7.2
21	36		7.78
22	36	H3	7.24
23			
24	27	-A1	7.7
25	27	-C1	7.96
26	27	-E1	7.78
27	27	-G1	8.19
28	27	A1	7.93
29	27	A3	7.8
30	27	A5	8.1
31	27	B4	7.99
32	27	C3	7.71
33	27	C4	7.62
34	27	C5	7.77
35	27	D2	7.72
36		D2	7.76
37	27	D4	7.88
38		E1	7.75
39		E3	7.87
40		E5	8.04
41		F2	8.06
42		F4	7.2
43		G1	7.88
44		G3	7.57
45		G5	7.79
46		H2	7.79
-		п2 Н4	
47	21	114	8.37

	А	В	С	D	E	F	G
48	Section 2	7 Surface Soils					
49	Locn	sand % of total		silt % of total		clay % of total	
50	-A1	<u> </u>		333770 01 10 10.1		<u> </u>	
51	A1	70.44		15.18		14.39	
52	A3						
53	A5						
54	B2						
55	B4						
56	-C1	50.77		35.29		13.94	
57	C1	76.61		14.80		8.59	
58	C3	11.10		52.19		36.72	
59	C4	85.69	·	8.42		5.89	
60	D2	61.46		21.41		17.14	
61	D4	83.77		9.86		6.37	
62	-E1	24.85		63.45		11.70	***************************************
	E1					7.41	
63		81.25		11.34	0.00		0.00
64	E3 dup	52.34	40.44	38.74	0.23	8.92	0.23
65	E3 dup	52.34	13.14	38.42	13.07	9.24	0.07
66	E3	70.91		19.94		9.14	
67	E5	50.50		27.87		21.63	
68	F2	78.94		14.50		6.56	
69	F4	57.04		23.72		19.25	
70	-G1	55.38		32.89		11.73	
71	G1	104.61	19.13	-12.66	19.20	8.06	0.06
72	G1 dup	77.55		14.49		7.96	
73	G3	80.48		12.32		7.19	
74	G5	62.46		22.23		15.31	
75	H2	82.79		10.67		6.54	
76	H4	56.88		33.24		9.88	
77							14.114.14.14.14.14.14.14.14.14.14.14.14.
78							
-	Section 3	6 Surface Soils					
80	Locn	sand % of total		silt % of total		clay % of total	
				22.81		11.57	
81	A1 A2	65.62		46.19		11.49	
82		42.31				9.99	
83	A3	30.01		60.00			
84	B1	75.86		22.64		1.50	
85	B2	49.85		39.30		10.85	
86	B3	47.66		41.37		10.96	~ ~ ~ ~
87	F1	31.78	0.92	55.37	0.99	12.85	0.07
88	F1 dup	30.47		56.77		12.76	
89	C1	39.05	1.14	59.41	6.74	1.54	7.87
90	C1 dup	37.44		10.00			
91	C2			49.88		12.67	
92		32.01		59.03		8.96	
	C3	32.01 62.97		59.03		8.96	
93	C3 D1			59.03 53.42		8.96	
94	D1 D1	62.97 30.25		59.03 53.42 53.77		8.96 16.33 15.99	
	D1 D1 D2	62.97		59.03 53.42 53.77 39.92	0.25	8.96 16.33 15.99 25.20	0.25
94	D1 D1	62.97 30.25		59.03 53.42 53.77 39.92 40.27	0.25	8.96 16.33 15.99 25.20 24.85	0.25
94 95	D1 D1 D2	62.97 30.25		59.03 53.42 53.77 39.92 40.27 21.75	0.25	8.96 16.33 15.99 25.20 24.85 12.53	0.25
94 95 96	D1 D1 D2 D2 dup	62.97 30.25 34.88		59.03 53.42 53.77 39.92 40.27	0.25	8.96 16.33 15.99 25.20 24.85	0.25
94 95 96 97	D1 D1 D2 D2 dup D3	62.97 30.25 34.88 65.72		59.03 53.42 53.77 39.92 40.27 21.75	0.25	8.96 16.33 15.99 25.20 24.85 12.53	0.25
94 95 96 97 98 99	D1 D1 D2 D2 dup D3 E1 E2	62.97 30.25 34.88 65.72 34.40 17.39		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22	0.25	8.96 16.33 15.99 25.20 24.85 12.53 15.42	0.25
94 95 96 97 98 99	D1 D1 D2 D2 dup D3 E1 E2 E3	62.97 30.25 34.88 65.72 34.40 17.39 25.39		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78		8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39	
94 95 96 97 98 99 100 101	D1 D1 D2 D2 dup D3 E1 E2 E3 F2	62.97 30.25 34.88 65.72 34.40 17.39		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24	0.25	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74	0.25
94 95 96 97 98 99 100 101 102	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10		8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88	
94 95 96 97 98 99 100 101 102 103	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25	0.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25	
94 95 96 97 98 99 100 101 102 103 104	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23		8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32	0.61
94 95 96 97 98 99 100 101 102 103 104 105	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 F3 dup	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94	0.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61	0.61
94 95 96 97 98 99 100 101 102 103 104 105 106	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 F3 dup G1	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94 59.90	0.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61 0.00	0.61
94 95 96 97 98 99 100 101 102 103 104 105 106 107	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 F3 dup G1 G2	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44 40.10 43.96		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94 59.90 44.39	0.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61 0.00 11.65	0.61
94 95 96 97 98 99 100 101 102 103 104 105 106 107 108	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 F3 dup G1 G2 G3	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44		59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94 59.90 44.39 34.08	0.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61 0.00 11.65 14.69	0.61
94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 F3 dup G1 G2 G3 G3 dup	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44 40.10 43.96 51.23	0.46	59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94 59.90 44.39 34.08 40.60	0.61 0.50 4.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61 0.00 11.65 14.69 8.16	0.61
94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 F3 dup G1 G2 G3 G3 dup H1	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44 40.10 43.96 51.23	0.16	59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94 59.90 44.39 34.08 40.60 63.60	0.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61 0.00 11.65 14.69 8.16 8.28	0.61
94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 dup G1 G2 G3 G3 dup H1 H1 dup	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44 40.10 43.96 51.23 28.12 27.89	0.16	59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94 59.90 44.39 34.08 40.60 63.60 63.92	0.61 0.50 4.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61 0.00 11.65 14.69 8.16 8.28 8.19	0.61
94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110	D1 D1 D2 D2 dup D3 E1 E2 E3 F2 F2 dup D2 F3 F3 dup G1 G2 G3 G3 dup H1	62.97 30.25 34.88 65.72 34.40 17.39 25.39 20.03 34.50 59.44 40.10 43.96 51.23	0.16	59.03 53.42 53.77 39.92 40.27 21.75 50.18 58.22 53.78 64.24 65.10 45.25 30.23 30.94 59.90 44.39 34.08 40.60 63.60	0.61 0.50 4.61	8.96 16.33 15.99 25.20 24.85 12.53 15.42 24.39 20.83 15.74 14.88 20.25 10.32 9.61 0.00 11.65 14.69 8.16 8.28	0.61

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	l A	В	С	D I	E	T F	G
1		27 Soil Profiles	9			<u>'</u>	
2	Locn	sand % of total	std dev sand	silt % of total	std dev silt	clay % of total	std dev clay
3	1-0		Stu dev Sand	39.63	<u>sta dev siit</u>	44.53	Stu dev clay
		15.84		38.31		48.94	
4	1-10	12.75				47.30	
5	1-20	12.95		39.75	·	47.30	
6	1-30	10.83					
7		70 57		40.70		40.05	
8	2-0	76.57		10.78		12.65	
9	2-10	80.49		11.80		7.71	
10	2-20	65.90		10.27		23.84	
11	2-30	79.62		10.10		10.28	
12			0.65	44.04	0.50	0.44	0.04
13	3-0D	79.65	0.25	11.21	0.56	9.14	0.31
14	3-0	79.29		12.00		8.71	
15	3-10	82.30		10.61		7.09	
16	3-20	75.45		13.36		11.19	
17	3-30	78.13	0.11	12.49	0.11	9.38	0.22
18	3-30D	77.98		12.33		9.68	
19							
20							
21	Section 3	36 Soil Profiles					
22	Locn	sand % of total		silt % of total		clay % of total	
23	1 - 0	78.20		13.63		8.17	
24	1 - 7	74.53		15.62		9.85	
25	1 - 21	74.00		15.65		10.35	
26	1 - 35	75.85		14.68		9.47	
27	1 - 49	87.13		7.92		4.95	
28	1 - 60	49.41		37.68		12.91	
29	1- 70	33.49		46.83		19.68	
30							
31	2 - 0	63.57		21.33		15.10	
32	2 - 10	69.95		16.55		13.51	
33	2 - 20	72.00		14.78		13.22	
34	2 - 30	71.95		15.47		12.58	
35	2 - 40	76.44		11.04		12.52	
36	2 - 50	71.76		14.09		14.14	
37	2 - 60	54.59		29.74		15.67	
38							
39	3-10	34.06		47.79		18.15	
40	3-10	21.92		46.19		31.89	
41	3-30	21.02					
42	3 - 40	17.95		57.85		24.20	
43	3 - 50	16.96		79.18		3.86	
44	3 - 60	15.37		49.40		35.23	
45	3 - 70	16.81		33.21		49.98	
46	3-70	10.01		33.21		10.00	
47							
41		1				<u> </u>	

¥	E3A	U ppm	30.22	26.51	25.06	21.81		-	28.30	24.94	18.91	16.38		19.09	16.74		23.46	20.61		13.89	12.11	3.30	3.33		21.85	18.96	27.58	24.24		99.57	100.63			9.36	7.97		80.86	82.70						
7	F3A	RSD (%)	89.0		69'0	98'0			92.0	1.36	1.52	2.17		3.44	2.05		0.99	1.16		0.62	8.0	1.76	0.94		89'0	1.81	29'0	1.2		0.37	-			19'1	1.52		1.08	1.55						
<u> </u>	F3A	Total DF	5	50.7	5	50.7			2	50.7	5	50.7		5	50.7		5	50.7		5	50.7	5	50.7		5	50.7	5	50.7		5	50.7		-	5	50.7		ç	50.7						
×	E3A	U/ 238	1263	1108	1343	1169			1364	1202	9001	871.6		954.3	837.2		1201	1055		6.999	581.2	180.2	182		1062	921.3	1423	1251		5038	5092			468.2	398.5		3930	4019						
*	F34	Sample:	27-2-0	27-2-0	27-2-06	27-2-06			27-2-10	27-2-10	27-2-30	27-2-20		27-2-30	27-2-30		36-1-0	36-1-0		36-1-21	36-1-21	36-1-42	36-1-42		36-1-60	36-1-60	27+CI	27+CI		27-D2	27-D2			27-GI	27-G1	-	27-D2b	27-D26						
 	F2B	U ppm	80.02	58.80	95.26	70.93	111.92	82.76	74.23	55.50	23.38	18.13		18.84	14.64		20.55	16.09		14.91	13.72	3.85	3.93		29.67	22.35	30.10	33.95	_	92.67	142.67			23.90	18.37		106.79	84.69					1	
	F2B	RSD (%)	12.89	5.22	16.57	2.56	12.37	0.94	16.14	1.51	17.74	10.21		16.94	14.55		16.93	13.79		17.36	19.57	16.95	26.74		16.13	6.36	19.13	4.73		14.71	19.84			15.77	11.57		14.58	3.04					1	
-	F2B	Ŀ	20	1032.43	20	1032.43	20	1032.43	20	1032.43	20	1032.43		20	1032.43		20	1032.43		20	1032.43	20	1032.43		20	1032.43	20	1032.43		20	1032.43			20	1032.43		20	1032.43					1	-
^	F2B	-	3345	2458	5106	3802	5999	4436	3578	2675	1244	964.6		941.8	731.8	-	1052			715.6	658.5	-	214.4		1442	1086	1553	1752		\neg	7219				918.5		5190	4116					1	
2	F2B	Sample:	27-2-0	27-2-0	27-2-0b	27-2-0b	27-2-0b DUP	27-2-0b DUP	27-2-10	27-2-10	27-2-20	27-2-20		27-2-30	27-2-30		36-1-0	36-1-0		36-1-21	36-1-21	36-1-42	36-1-42		36-1-60	36-1-60	27+C1	27+C1		27+D2	27+D2			27+G1	27+G1		27+D2b	27+D2b						
7	F2A	U ppm	800.24	00.689	849.07	754.10			479.25	403.73	142.24	108.70		107.40	81.18		62.13	45.10		77.23	59.50	22.36	16.66		171.79	125.39	129.19	95.16		393.28	318.97	393.28	336.36	145.22	04.22		425.93	52.88					+	-
+	F2A	-		4.14 E	8.22	3.28 7	-		12.32 4	4.45 4	14.33	3.63	-		0.88			-		-	2.94	-	1.85	_	13,58 1	2.29 1	13.38 1	3.03	_		7		-	14.32 1	1.65		11 4	4.36					1	-
	F2A	Total DF R	1	1032.43	50	1032.43			20	1032.43	20	1032.43		20	1032.43			53		20	1032.43	20	1032.43		20	1032.43	20	1032.43		_	43	_	1032.43	20	1032.43		50	1032.43					+	
<u>-</u>	F2A	U/ 238 7	-		45510	40420 1			23100	19460 1	7567	5783 1	_	5370	4059 1		3181	2309 1		3707	2856 1		909.7		8349	6094 1	9999	4910 1			-	-		-	5211 1		20700	17150 1	_				+	
ξ.	F24	Sample:	27-2-0	27-2-0	27-2-0b	27-2-0b			27-2-10	27-2-10	27-2-20	27-2-20	_	27-2-30	27-2-30		36-1-0	36-1-0		36-1-21	36-1-21	36-1-42	36-1-42		36-1-60	36-1-60	27+C1	27+C1		27+D2	27+D2	27+D2 DUP	27+D2 DUP	27+G1	27+G1		27+D2b	27+D2b						
1	FIB	U ppm	10.48	8.63	10.74	9.28			13.05	11.57	24.30	21.47	21.73	15.84	13.62	13.94	1.23	1.61	2.90	2.80	2.34	4.02	3.18	3.27	76.52	70.29	11.38	9.44	10.35	47.49	41.32	7	-	3.38	2.74	2.96	50.86	44.86	45.06				1	-
4	FIB	=	Н	\dashv	-	0.89			3.04	-	-		1.74	-	6.0	-	1.89	-	-	-	-	-	3.92	1.37	-	7.70	4.84	-	5.97	\dashv	2.43		-		-	-	-	0.79	0.63				+	
-	FIB	Total DF	90	1032.43	20	1032.43			20	1032.43	20	1032.43	1032.43	20	032.43	1032.43	20	1032.43	1032.43	20	1032.43	20	1032.43	1032.43	20	1032.43	20	1032.43	1032.43	20	1032.43			20	1032.43	1032.43	20	1032.43	1032.43					-
	FIB	_	-	-		497.6		-	629.1	557.8	1293	\vdash				. 8.969	62.98				-				3719	3416	587.1		-	-	2091			168.9			2472	2180				ration)	1	-
	FIB	Sample:	27-2-0	27-2-0	27-2-0b	27-2-0b			27-2-10	27-2-10	27-2-20	27-2-20	27-2-20	27-2-30	27-2-30	27-2-30	36-1-0	36-1-0	36-1-0	36-1-21	36-1-21	36-1-42	36-1-42	36-1-42	36-1-60	36-1-60	27+C1	27+C1	27+C1	27+D2	27+D2			27+G1	27+G1	27+G1	27-D2b	27-D2b	27-D2b			(volume of liquids added and carryover not important for concentration)	Volume	ž
,	FIA	U ppm	21.41	17.91	23.53	19.78			25.98	22.22	48.72	42.24		25.60	21.60		4.49	3.83		6.34	5.40	12.60	10.93		192.80	188.70	23.53	20.52	-	96.76	75.32	76.42		4.88	4.61		85.35	73.60	_			cr not impo	Volume	r.3B
-	FIA	RSD (%)	6.2	\dashv	8.87	-		_	7.93	-	8.05	0.14		8.63			12.79	4.14		12.92	\dashv	8.08	-		\dashv	2.31	-		\dashv	5.21	+	+		6.49	8.04		4.53	1.46				and carryo	Volume	FJA
,	FIA	Total DF F	20	1032.43	20	1032.43			50	1032.43	20	1032.43		20	1032.43		50	1032.43		20	1032.43	20	1032.43		20	1032.43	20	1032.43		20	1032.43	1032.43		20	1032.43		20	1032.43				quids added	Volume	L7B
3	FIA	U/ 238	-		1261	-			1252		2592	2247	_	1280			229.9			304.5		687.7	-			9171		1059		7	+	3867		_	230.7			3577				volume of li	Volume Volume	LZA.
,		-	27-2-0	27-2-0	27-2-0b	27-2-0b			27-2-10	27-2-10	27-2-20	27-2-20		27-2-30	27-2-30		36-1-0	36-1-0		36-1-21	36-1-21	36-1-42	36-1-42		36-1-60	36-1-60	27+C1	27+C1		27+D2	27+02	27+D2		27+G1	27+G1		27-D2b	27-D2b					5	LID
		mass	2.09	2.09	2.68	2.68	2.68	2.68	2.41	2.41	2.66	2.66	2.66	2.5	2.5	2.5	2.56	2.56	2,56	2.4	2.4	2.73	2.73	2.73	2.43	2.43	2.58	2.58	2.58	2.53	2.53	2.53	2.53	2.5	2.5	2.5	2.43	2.43	2.43			"final total volume	Volume	LIA
		Sample:	27-2-0	27-2-0	27-2-0b	27-2-0b	27-2-0b	27-2-0b	27-2-10	27-2-10	27-2-20	27-2-20	27-2-20	27-2-30	27-2-30	27-2-30	36-1-0	36-1-0	36-1-0	36-1-21	36-1-21	36-1-42	36-1-42	36-1-42	36-1-60	36-1-60	27+C1	27+C1	27+C1	27+D2	27+D2	27+D2	27+D2	27+G1	27+G1	27+G1	27-D2b	27-D2b	27-D2b			-fin		
E	7	3	7	S.	٥	7	∞	6	2	Ξ	12	2	=	15	9	11	18	61	20	21	22	23	77	25	97	27	28	50	30	=	32	23	75	35	36	37	38	39	40	==	42	43	7 5	÷

Seqtlextn_! I nins

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ΑW			SUM	1132.88	985.40	1120.99	76.986			731.86	627.47	329.28	278.80		282.83	243.01		152.03	121.71		139.52	113.88	56.46	47.01		524.44	452.59	329.80	290.86		943.74	880.69			240.06	191.26		1029.81	901.30					
ΑV			F5 U ррт	7.58	4.74	6.35	4,62			4.20	3.96	3.46	3,34		3.94	3.90		76'0	98'0		1.68	4.1	0.73	0.42		1.47	68'0	3.99	3.93		31.46	11.42			3.90	2.73		31.23	14.14					
AU			F4 U ppm	170.26	168.90	102.54	102.18			92.03	92.49	59.74	61.20		82.58	83.22		32.09	27.48		15.98	13,69	7.06	5.96		24.81	21.32	92.46	93.64		159.92	161.44			45.50	46.92		213.37	217.08					
AT		= F3A + F3B	F3 U ppm	42.88	37.42	33.51	29.07			43.11	38.00	27.44	23.72		28.64	24.86		30.57	26.75		20.58	17.80	5.85	5,93		27.37	23.65	39.16	34.21		132.15	129.55			13.29	11.67		116.28	114.05					
AS		= F2A + F2B	F2 U ppm	880.26	747.80	944.33	825.04	111.92	82.76	553,49	459,23	165.62	126.83		126.24	95.82		82.68	61.18		92.14	73.22	26.21	20.59		201.46	147.74	159.28	129.11		485.95	461.64	393.28	336,36	169.12	122.59	***************************************	532.72	437.57					
AR		=FIA+FIB	F1 U ppm	31.89	26.54	34.27	29.06			39,03	33.79	73.03	63.70	21.73	41,44	35.22		5.72	5.44	2.90	9.15	7.74	19.91	14.11	3.27	269.32	258.99	34.91	29.96	10.35	134.25	116.64	76.42		8.25	7.36	2.96	136.21	118.46					
AQ			=(((H1/1000)*50)/F1)	7.58	4.74	6.35	4.62			4.20	3.96	3.46	3,34		3,94	3.90		0.97	0.86		1.68	1.44	0.73	0.42		1.47	0.89	3.99	3,93		31.46	11.42			3.90	2.73		31.23	14,14					and the state of t
ΑP			Sample:	27-2-0	27-2-0	27-2-0b	27-2-0b			27-2-10	27-2-10	27-2-20	27-2-20		27-2-30	27-2-30		36-1-0	36-1-0		36-1-21	36-1-21	36-1-42	36-1-42		36-1-60	36-1-60	27 + C1	27 + CI		27 + D2	27 + D2			27 + G1	27 + G1		27 + D2b	27 + D2b				+	+
OV				FS	7	1	-			FS		-	FS			FS		FS	£		FS	FS	FS	33		FS	FS				F3	\forall		7	†	53	_		FS			1		T
AN	-	U from	MW digest	527.35						344.9		187.7			218.8			7			3,39					6.21			174.4		671.9				139.5			621.9						
AM	0	Joш	values	1125.30	99.086	1114.65	985.35	-		727.66	623.51	325.83	275.46		278.90	239.11		151.06	120.85		137.84	112.44	55.73	46.58		522.97	451.70	325.81	286.92		912.27	869.27			236.16	188.54		998.58	887.16					-
⊢ ∀			Sample: C:	27-2-0	27-2-0	27-2-0b	27-2-0b	27-2-0b	27-2-0b	27-2-10	27-2-10	27-2-20	61.20 27-2-20 27	27-2-20	27-2-30	27-2-30	27-2-30	36-1-0	36-1-0	36-1-0	36-1-21	36-1-21	36-1-42	36-1-42	36-1-42	36-1-60	36-1-60	27+C1	27+C1	27+C1	27+02	27+D2	27+D2	_		_	27+G1	27-D2b	27-D2b	27-D2b				+
ΑK	-	走	ndd D	170.26	168.90	102.54	102.18			92.03	92.49	59.74	61.20		82.58	83.22		32.09	27.48		15.98	13.69	90.7	5.96		24.81	21.32	95.46	93.64		159.92			-1	45.50				217.08					
₹	- 1	刮		1.2							9.02				0.63			1.69				0.62					1.56				0.7	0.63			0.74	1.02		1.68	1.29					
Į	THE PERSON NAMED AND POST OFFICE ADDRESS OF THE PERSON NAMED AND POST OF T	武	Total DF	5	50.7	S	50.7			5	50.7	5	50.7		\$	50.7		S	50.7		\$	50.7	5	50.7		\$	50.7	\$	50.7		2	50.7			5	50.7		2	50.7					
AH		Z	0 / 238	7117	7060	2496	5477			4436	4458	3178	3256		4129	4161		1643	1407		766.8	626.9	385.7	325.4		1206	1036	1771	4832		8092	8169			2275	2346		10370	10550					
AG		Z	Sample:	27-2-0	27-2-0	27-2-06	27-2-06			27-2-10	27-2-10	27-2-20	27-2-20		27-2-30	27-2-30		36-1-0	36-1-0		36-1-21	36-1-21	36-1-42	36-1-42		F4-36-1-60	F4-36-1-60	F4-27+C1	F4-27+C1		F4-27+D2	F4-27+D2			F4-27+G1	F4-27+G1		F4-27-D2b	F4-27-D2b					
AF		8	U ppm	12.67	10.92	8.46	7.26			14.81	13.06	8.53	7.34		9.56	8.11		7.11	6.14		69.9	5.69	2.55	2.60	_	5.52	4.70	11.58	9.97		32.59	28.91			3.92	3.70		35.41	31.36					T
AE		E	RSD (%)	0.5	1.74	2.35	1.88			1.01	1.8	1.78	2.44		1.22	1.45		0.87	1.68		1.69	2.01	98'0	1.47		1,4	0.49	1.16	2.25		8.0	2.1	***************************************		10.7	1.86		0.7	1.39		-	T		
P			ΞÌ	2	50.7	2	50.7			2	50.7	2	50.7		2	50.7		2	20.7		5	50.7	5	50.7		5	50.7	5	50.7		S	20.7			5	20.7		2	50.7					
AC		F3B		529.5	456.3	453.3	389.2			714	629.6	454	390.4		477.9	405.7		364.2	314.4		321	273.1	139	141.7		268.2	228.3	597.5	514.2		1649	1463			136.1	581		1721	1524					T
SE SE		F3B	Sample:	27-2-0	27-2-0	27-2-06	27-2-0b			27-2-10	27-2-10	27-2-20	27-2-20		27-2-30	27-2-30		36-1-0	36-1-0		12-1-98	36-1-21	36-1-42	36-1-42		36-1-60	36-1-60	27+CI	27+CI		27+D2	27+D2			27+G1	27+67		27-D2b	27-D2b				-	

[______]

| de Organic Residual | - | 0.55 | 0.04

 | 0.60 | 1.12 | 0
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 | 0 | = | 1.50
 | | | 0.67 | 1.23

 | 1.09 | 0.24
 | | | 1.28 | 2.31 | 0.01
 | C.I | | |

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 | | | | | | |
| 9 | F4 % | 12.91 | 4.49

 | 13.66 | 20.05 | 31.72
 | | | 21.84 | 11.73

 | 12.60 | 4.72
 | | | 30.12 | 20.02 | 3.37
 | 71.74 | | |

 |
 | | | | | |
 |

 | | | | | |
 | | | | | | |
| Oxide | F3 % | 3.38 | 0.59

 | 5.97 | 8.42 | 10.18
 | | | 21.04 | 15.19

 | 11.48 | 5.22
 | | | 11.82 | 13.16 | 1.69
 | 2.02 | | |

 |
 | | | | | |
 |

 | | | | | |
 | | | | | | |
| Carbonate | F2 % | 80.29 | 4.95

 | 74.41 | 47.90 | 42.03
 | | | 52.33 | 65.17

 | 45.11 | 35.53
 | | | 46.34 | 51.05 | 1.28
 | 17710 | | |

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 | | | | | | |
| xchangeable | F1 % | 2.88 | 0.17

 | 5.36 | 22,51 | 14.57
 | | | 4.12 | 89.9

 | 27.62 | 54.29
 | | | 10.44 | 13.46 | 0.39
 | +0.5 | | |

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| | | 27-2-0 |

 | 27-2-10 | 27-2-20 | 27-2-30
 | | | 36-1-0 | 36-1-21

 | 36-1-42 | 36-1-60
 | | 100 | Z/+CI | Z1 + DZ | 10,100
 | 101/7 | | |

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| | | 0.57 |

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 | 1 23 | 7 | 1.09 |

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 | 0.24 | | 1.28 | | 2.32 |
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 | | 1.53 | | | 2.30 |
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| | | 16.08 | -

 | 9.73 | |
 | | 13,66 | | 20.05

 | |
 | 31.72 | | | 48.12 |
 | 11.73 | | 12.60 |

 |
 | 4.72 | | 30.12 | | 17.64 |
 |

 | | 21.74 | | | 22.40 | |
 | | | | | | |
| | | 3.79 |

 | 2.96 | |
 | | 5.97 | | 8.42

 | |
 | 10.18 | | | 40.12 |
 | 15.10 | | 11.48 |

 |
 | 5.22 | | 11.82 | | 14.36 |
 |

 | | 5.82 | | | 11.97 | |
 | | | | | | |
| | | 76.79 |

 | 83.79 | |
 | | 74.41 | | 47.90

 | |
 | 42.03 | | 25.63 | 57.33 |
 | 65.17 | 14.00 | 45.11 |

 |
 | 35.53 | | 46.34 | | 51.96 |
 |

 | | 67.27 | | | 50.14 | |
 | | | | | | |
| | | 2.75 |

 | 3.00 | |
 | | 5.36 | | 22.51

 | |
 | 14.57 | | 5 | 4.12 |
 | 899 | | 29.72 |

 |
 | 54.29 | | 10.44 | | 13.73 |
 |

 | | 3.64 | | | 13.18 |
 | | | | | | |
| | | | 27-2-0

 | 27-2-00 | 27-2-0b | 27-2-0b
 | 27-2-0b | 27-2-10 | 27-2-10 | 27-2-20

 | 27-2-20 | 27-2-20
 | 27-2-30 | 27-2-30 | 26.4.0 | 20-1-00 | 36.1.0
 | 36-1-21 | 36-1-21 | 36-1-42 | 36-1-42

 | 36-1-42
 | 36-1-60 | 36-1-60 | 27+C1 | 27+C1 | 27+D2 | 27+D2
 | 27+D2

 | 27+D2 | 27+G1 | 27+G1 | 27+G1 | 27-D2b | 27-D2b
 | 27-D2b | | | | | |
| Residual | F5 % | 29'0 | 0.48

 | 0.57 | 0.47 |
 | | 0.57 | 0.63 | 1.05

 | 1.20 |
 | 1.39 | 8. | 130 | +0.0 | 0,70
 | 1 20 | 1.26 | 1.29 | 06.0

 |
 | 0.28 | 0.20 | 1.21 | 3 | 3.33 | 1.30
 |

 | | 1.62 | 1.43 | | 3.03 | 1.57
 | | | | | | 1 |
| Organic | F4 % | 15.03 | 17.14

 | 9.15 | 10.32 |
 | | 12.58 | 14.74 | 18.14

 | 21.95 |
 | 29.20 | 34.25 | :: | 11.12 | 85.22
 | 11.45 | 12.02 | 12.51 | 12.68

 |
 | 4.73 | 4.71 | 28.04 | 35.40 | 16.95 | 18.33
 |

 | | 18.95 | 24.53 | | 20.72 | 24.09
 | | | | | | |
| Oxide | F3 % | 3.79 | 3.80

 | 2.99 | 2.94 |
 | | 5.89 | 90'9 | 8.33

 | 8.51 |
 | 10.13 | 10.23 | 15.05 | 21.00 | 21.30
 | 14.75 | 15.63 | 10.35 | 12.61

 |
 | 5.22 | 5.23 | 11.87 | | 14.00 | 14.71
 |

 | | 5.53 | 6.10 | | 11.29 | 12.65
 | | | | | | |
| Carbonate | F2 % | 77.70 | 75.89

 | 84.24 | 83.34 |
 | | 75,63 | 73.19 | 50.30

 | 45,49 |
 | 44.63 | 39.43 | 6130 | 50.32 | 77.00
 | 66 04 | 64.30 | 46.43 | 43.80

 |
 | 38.41 | 32.64 | 48.30 | 75.71 | 51.49 | 52.42
 |

 | | 70.45 | 64.09 | | 51.73 | 48.55
 | | | | | | + |
| | F1% | 2.82 | 2.69

 | 3.06 | 2.94 |
 | | 5.33 | 5.39 | 22.18

 | 22.85 |
 | 14.65 | 14:49 | 3.16 | 2.00 | /+"+
 | 6.56 | 6.79 | 29.42 | 30.01

 |
 | 51.35 | 57.22 | 10.30 | OC. | 14.23 | 13.24
 |

 | | 3.44 | 3.85 | | 13.23 | 13.14
 | | | | | | 1 |
| Ex | | 7-2-0 | 7-2-0

 | -5-0b | -5-0p | -2-0b
 | 2.00 | -2-10 | -2-10 | -2-20

 | -5-20 | -2-20
 | -2-30 | 2.30 | 4.0 | 14.0 | 1.1.0
 | 1-21 | -1-21 | -1-42 | -1-42

 | -1-42
 | 1-60 | -1-90 | <u> </u> | 4 | +D2 | 7+D2
 | ,+D2

 | ,+D2 | +61 | 7+G1 | 7+G1 | -D2b | -D2b
 | -D2b | | | | | |
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| | Ufrom Exchangeable Carbonate Oxide Organic Residual | Exchangeable Carbonate Oxide Oxide Oxide Oxide Oxide Oxide Piss F1% F1% | Ufrom Exchangeable Carbonale Organic Organic Residual Residual Residual AMV digest % diff F1 % F2 % F3 % F4 % F5 % R5 % </td <td>U from Saching each field of Sach f</td> <td>U from Start Exchangeable Carbonared Start Oxide Organic Residual Residual</td> <td>U from Exchangeable Carbonache Oxide Oxide Organic Residual Residu</td> <td>Ufrom Exchangeable Carbonared Oxide Openie Residual Residual</td> <td>U from Sacial Submissible Carbonicable Carbonic</td> <td>U from Sacial Secretary U from Sacial Secretary D from Sacial Secretary D from Sacial Secretary D from Sacial Secretary D from Sacial Secretary Exchangeable Sacial Secretary</td> <td>MV digest % diff Exchangeable Carbonate Original Residant <th< td=""><td>We digest % diff Exchangeable Carbonare Oxide Organic Resident Resident</td></th<><td>U from NV digest % diff Exchangeable Carbonate Ca</td><td>U from NV digest % sidt Exchangeable Carbonate /td><td>U from MV digest S, diff Exchangeable Carbonate C</td><td>U from MV digest Schlammenble Carbonate Carbon</td><td>U from NV digest % diff Exchangeable Carbonate Ca</td><td>MV digest 5 differentiation Chickenine Oxide Organic Resident Resident Probability Resident Probability Resident Probability Probability Resident Probability Resident Probability Probability</td><td>MV digest % diff Exchangeable Garbonate /td><td>MV digest % diff Exchangeable Carbonate /td><td>U from National Montages /td><td>MV digest 5 differentiation Chickbanged Carbonate Original Resident Resident Profession Profession<td>WV digest % diff First Schangeable (Subbanishe (Subbanish</td><td>W. digest 5.6.din Conditionable (Dating Residual) Chapterable (Dating Residual) Conditional (Dating Residual) Chapterable (Dating Residual)</td><td>NW digest 5, 641 First Chinoscable Cycle Chinoscaple Cycle Chinos</td><td>NV Month of Table Seeding Seeding South of Table Seeding Seedin</td><td>VIV Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE CONTROL CONTROL CALIDROMINE CONTROL CALIDROMINE CONTROL CALIDROMINE CALIDROMINE<</td><td>NV Mignet S, 641 Configuration Cyclique Cyclique Residentification NV Mignet S, 641 E F18,56 F27,50 Cyclique Cyclique 277,20 2.75 7.679 3.79 16.06 0.77 272,40 2.78 277,26 2.66 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72<</td><td>NV Upons NV Upons</td><td>VI Time M. 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M. diget</td><td>NV Mignet No. 1</td><td> NW diget NY diget</td><td></td></td></td></td> | U from Saching each field of Sach f | U from Start Exchangeable Carbonared Start Oxide Organic Residual Residual | U from Exchangeable Carbonache Oxide Oxide Organic Residual Residu | Ufrom Exchangeable Carbonared Oxide Openie Residual Residual | U from Sacial Submissible Carbonicable Carbonic | U from Sacial Secretary U from Sacial Secretary D from Sacial Secretary D from Sacial Secretary D from Sacial Secretary D from Sacial Secretary Exchangeable Sacial Secretary | MV digest % diff Exchangeable Carbonate Original Residant Residant <th< td=""><td>We digest % diff Exchangeable Carbonare Oxide Organic Resident Resident</td></th<> <td>U from NV digest % diff Exchangeable Carbonate Ca</td> <td>U from NV digest % sidt Exchangeable Carbonate /td> <td>U from MV digest S, diff Exchangeable Carbonate C</td> <td>U from MV digest Schlammenble Carbonate Carbon</td> <td>U from NV digest % diff Exchangeable Carbonate Ca</td> <td>MV digest 5 differentiation Chickenine Oxide Organic Resident Resident Probability Resident Probability Resident Probability Probability Resident Probability Resident Probability Probability</td> <td>MV digest % diff Exchangeable Garbonate /td> <td>MV digest % diff Exchangeable Carbonate /td> <td>U from National Montages /td> <td>MV digest 5 differentiation Chickbanged Carbonate Original Resident Resident Profession Profession<td>WV digest % diff First Schangeable (Subbanishe (Subbanish</td><td>W. digest 5.6.din Conditionable (Dating Residual) Chapterable (Dating Residual) Conditional (Dating Residual) Chapterable (Dating Residual)</td><td>NW digest 5, 641 First Chinoscable Cycle Chinoscaple Cycle Chinos</td><td>NV Month of Table Seeding Seeding South of Table Seeding Seedin</td><td>VIV Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE CONTROL CONTROL CALIDROMINE CONTROL CALIDROMINE CONTROL CALIDROMINE CALIDROMINE<</td><td>NV Mignet S, 641 Configuration Cyclique Cyclique Residentification NV Mignet S, 641 E F18,56 F27,50 Cyclique Cyclique 277,20 2.75 7.679 3.79 16.06 0.77 272,40 2.78 277,26 2.66 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72<</td><td>NV Upons NV Upons</td><td>VI Time M. 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M. diget</td><td>NV Mignet No. 1</td><td> NW diget NY diget</td><td></td></td></td> | We digest % diff Exchangeable Carbonare Oxide Organic Resident Resident | U from NV digest % diff Exchangeable Carbonate Ca | U from NV digest % sidt Exchangeable Carbonate | U from MV digest S, diff Exchangeable Carbonate C | U from MV digest Schlammenble Carbonate Carbon | U from NV digest % diff Exchangeable Carbonate Ca | MV digest 5 differentiation Chickenine Oxide Organic Resident Resident Probability Resident Probability Resident Probability Probability Resident Probability Resident Probability Probability | MV digest % diff Exchangeable Garbonate | MV digest % diff Exchangeable Carbonate | U from National Montages | MV digest 5 differentiation Chickbanged Carbonate Original Resident Resident Profession Profession <td>WV digest % diff First Schangeable (Subbanishe (Subbanish</td> <td>W. digest 5.6.din Conditionable (Dating Residual) Chapterable (Dating Residual) Conditional (Dating Residual) Chapterable (Dating Residual)</td> <td>NW digest 5, 641 First Chinoscable Cycle Chinoscaple Cycle Chinos</td> <td>NV Month of Table Seeding Seeding South of Table Seeding Seedin</td> <td>VIV Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE CONTROL CONTROL CALIDROMINE CONTROL CALIDROMINE CONTROL CALIDROMINE CALIDROMINE<</td> <td>NV Mignet S, 641 Configuration Cyclique Cyclique Residentification NV Mignet S, 641 E F18,56 F27,50 Cyclique Cyclique 277,20 2.75 7.679 3.79 16.06 0.77 272,40 2.78 277,26 2.66 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72<</td> <td>NV Upons NV Upons</td> <td>VI Time M. 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M. diget</td><td>NV Mignet No. 1</td><td> NW diget NY diget</td><td></td></td> | WV digest % diff First Schangeable (Subbanishe (Subbanish | W. digest 5.6.din Conditionable (Dating Residual) Chapterable (Dating Residual) Conditional (Dating Residual) Chapterable (Dating Residual) | NW digest 5, 641 First Chinoscable Cycle Chinoscaple Cycle Chinos | NV Month of Table Seeding Seeding South of Table Seeding Seedin | VIV Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE Control CALIDROMINE CONTROL CONTROL CALIDROMINE CONTROL CALIDROMINE CONTROL CALIDROMINE CALIDROMINE< | NV Mignet S, 641 Configuration Cyclique Cyclique Residentification NV Mignet S, 641 E F18,56 F27,50 Cyclique Cyclique 277,20 2.75 7.679 3.79 16.06 0.77 272,40 2.78 277,26 2.66 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72 1.78 1.72 1.72< | NV Upons NV Upons | VI Time M. Schlinschlie Carbonicable Carbonicable <td>Uniformation of the part of the</td> <td>Uniformation between the control of the con</td> <td>NV Mellon Septemblish Coloration Original State Forticol Annual Library Coloration Coloration Annual Library Coloration Annual Library Coloration Annual Library Coloration Annual Library Annual Librar</td> <td>NVM dipers Septemble Properties (Particular) Companie (Partic</td> <td>U from No. 1 Septembroad of the control o</td> <td>VICTORY ACT Figure 1 Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control<</td> <td>University Act and series Findal messale Colored problems of the pro</td> <td>Virtual part of the /td> <td> N. 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M. diget</td> <td>NV Mignet No. 1</td> <td> NW diget NY diget</td> <td></td> | Uniformation of the part of the | Uniformation between the control of the con | NV Mellon Septemblish Coloration Original State Forticol Annual Library Coloration Coloration Annual Library Coloration Annual Library Coloration Annual Library Coloration Annual Library Annual Librar | NVM dipers Septemble Properties (Particular) Companie (Partic | U from No. 1 Septembroad of the control o | VICTORY ACT Figure 1 Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control Control< | University Act and series Findal messale Colored problems of the pro | Virtual part of the | N. M. diget M. M. diget | NV Mignet No. 1 | NW diget NY diget | |

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APPENDIX E

Vegetation Transect Data

			T				1							
ch size													A STATE OF THE PROPERTY OF THE	
e grass pat	13													
rass speci	3													
# herb specie	4				13.984									
total	101.5			% of total	0.340	90.920	0.280	0.760	0.440	0.480	0.200	6.460	0.120	100.000
pnshes	ı			std dev	ı	139.86	2.83	2.52	3.02	3.94	0.71	14.76	1.732051	
grasses	6.94			avg size	17	98.83	7	12.67	3.14	4	1.25	17.94	2	
herbs	1.66			sum length	17	4546	14	38	22	24	10	323	9	2000
litter	0.48		2 Sec 27	# patches	1	47	2	3	7	9	8	18	n	
bare ground	92.42		y Statistics for F1-F		artemesia	bare ground	Blue Grama grass	Snakeweed	Kochia weed	Soil litter	Lope?	Indian Rice Grass	Tumbleweed	
Locn	F1-F2		Summar										And in contract the first of the contract of t	
Land type	Disturbed Plain											ENTERTHEN THE CANADA CONTRACTOR STATES OF THE CANADA CONTRACTOR STATES OF THE CANADA CONTRACTOR CON		-
	27													
81	82	83	84	85	98	87	88	68	06	91	92	93	94	95
	Land type Locn bare ground litter herbs grasses bushes	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 # patches sum length avg size std dev % of total	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 *** *** *** *** *** ** *** *** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** **	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 mark mark std dev % of total mark mark mark mark 17 17 0.340 mark mark mark mark 47 4546 98.83 139.86 90.920	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 A patches sm length avg size std dev % of total artemesia 1 17 17 0.340 bare ground 47 4546 98.83 139.86 90.920 Blue Grama grass 2 14 7 2.83 0.280	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 sm length avg size std dev % of total # partenesia 1 17 0.340 bare ground 47 4546 98.83 139.86 90.920 Blue Grama grass 2 14 7 2.83 0.280 Snakeweed 3 38 12.67 2.52 0.760	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec. 27 m + + + 101.5 m artemesia 1 17 0.340 m bare ground 47 4546 98.83 139.86 90.920 m Blue Grama grass 2 14 7 2.83 0.760 m Kochia weed 3 38 12.67 2.52 0.760 m Kochia weed 7 2 3.14 3.02 0.440	Land type Loen bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 m 101.5 101.5 artemesia # patches sum length avg size std dev % of total bare ground 47 4546 98.83 139.86 90.920 Blue Grama grass 2 14 7 2.83 0.280 Snakeweed 3 38 12.67 2.52 0.760 Kochia weed 7 22 3.14 3.02 0.440 Soil litter 6 24 4 3.94 0.480	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 m m # patches sum length avg size std dev % of total artemesia 1 17 17 0.340 bare ground 47 4546 98.83 139.86 90.920 Blue Grama grass 2 14 7 2.83 0.280 Snakeweed 3 38 12.67 2.52 0.760 Kochia weed 7 22 3.14 3.02 0.440 Soil litter 6 24 4 3.94 0.480 Lope? 8 10 1.25 0.71 0.200	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 m 101.5 101.5 artemesia # patches sum length avg size std dev % of total bare ground 47 4546 98.83 139.86 90.920 Blue Grama grass 2 14 7 2.83 0.280 Snakeweed 3 38 12.67 2.52 0.760 Kochia weed 7 22 3.14 3.02 0.440 Complex 8 10 1.25 0.71 0.200 And the complex of the complex	Land type Locn bare ground litter herbs grasses bushes total 27 Disturbed Plain F1-F2 92.42 0.48 1.66 6.94 101.5 Summary Statistics for F1-F2 Sec 27 m 10.1.5 101.5 artenesia # patches sm length avg size std dev % of total bare ground 47 4546 98.83 139.86 90.920 Blue Grama grass 2 14 7 2.83 0.280 Snakeweed 3 38 12.67 2.52 0.760 Kochia weed 7 22 3.14 3.04 0.480 Lope? 8 10 1.25 0.71 0.200 Lope? 8 10 12.5 0.71 0.200 Tumbleweed 3 6 2 17.32051 0.120

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Summary Section 27 transects

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z	ch size															Annual control of the						
M	e grass pat	12.58																				
Г	rass specie	8																				
Я	# herb speciegrass specife grass patch size	3																				
ſ	total	89.86			% of total	4.34	65.96	0.56	99.0	0.02	0.32	1.32	4.98	0.02	0.22	10.20	1.00	0.04	5.46	0.16	4.74	100.000
Į	bushes	4.74			std dev	4.06	29.76	3.21	21.92		6.67	6.87	12.6			14.42			13.11			
Н	grasses	21.62			avg size	3.62	24.25	9.33	16.5	1	5.33	9	8.89	1	11	17	50	2	13.65	8	237	
Ð	herbs	1.38			# patches sum length	217	3298	28	33	-	16	99	249	1		510	20	2	273	8	237	2000
Ł	litter	4.98		Section 27	# patches	09	136	ж	2	-	3	=	28			30	1	1	20		1	
Ξ	bare ground	65.96		Summary Statistics for G1-F1 Section 27	Name	ag sp	bare ground	Blue grama grass	galleta	grass	Snakeweed	Kochia weed	ground litter	losc	muhly	Indian Rice grass	rock	Tumbleweed	Sand dropseed grass	stco	tamarisk	
Q	Locn	G1-F1		Summary																		
С	Land type	Former Pond																				
В		27																				
	55	99	57	58	59	09	19	62	63	64	65	99	29	89	69	70	71	72	73	74	75	9/

Page 1

Summary Section 27 transects

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Z							TOTAL STATE OF THE				And the second s				AND THE PARTY OF T			AND											
M	h size																												
Γ	grass pate	7.8	9.13																										
К	rass species	2	_																										
J	therb specie#grass speciere grass patch size	3	4				9.13														7.87837838								
I	total	97.52	100.86			% of total	3.84	43.2	12.6	0.56	9.0	0.82	0.02	38.02	0.34	100				% of total	0.04	46.02	10.46	0.28	1.2	41.4	0.12	0.48	100
Н	bushes	0	5.04			std dev	20.32	25.86	60.6	5.86	14.14	2.87		16.62	1					std dev	1	42.27	7.49	0.52	4.63	18.03	2.83	2.83	
IJ	grasses	11.66	12.6			avg size	27.43	23.74	9.13	5.60	15.00	10.25	1.00	17.93	17.00					avg size	2.00	36.52	9.02	1.40	3.75	22.75	3.00	12.00	
Щ	herbs	0.44	2			sum length	192	2160	630	28	30	41	_	1901	17	2000				sum length	2	2301	523	14	09	2070	9	24	2000
Ε	litter	41.4	38.02		c 27 01	# patches	7	91	69	5	2	4		106				AND THE RESEARCH WAS AND THE PROPERTY OF THE P	Sec 27 01	# patches	_	63	58	10	16	91	2	2	
D	bare ground	44.02	43.2		Summary statistics A3-A4 Sec		Fourwing saltbush	bare ground	Blue Grama grass	Depi	Gasp	Snakeweed	Herb	ground litter	dood				Summary Statistics for A2-A3 Sec 27 01	Name	atrb	bare ground	Blue grama grass	depi	eltr	ground litter	mustard	dood	
၁	Locn	A2-A3	A3-A4		Summar							ETRANSA PARA TRANSPORTE EN ESTE ANAMANANA ANAMANANA ANAMANA PROPRIATA DE CONTRA PARA DE CONTRA P	AND THE THE PARTY AND THE PART	skelin spieka dyk kiej sigele dekiele gelinek deligity dekiele keles pieka da					Summary										
9	Land type	Undisturbed												ing kada indemokratelar kerkelar indemokratelar independent depekter indemokrate endemokratelar indemokratelar															
	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	20	51	52

Page 1

	А	В	C	D	E	Ľ	Ð	H	I	ſ	X	Г	M	z
$\overline{-1}$		Land type	Locn	bare ground	litter	herbs	grasses	pushes	total	# herb specie#grass speciege grass patch size	grass species	e grass patel	h size	
7	27	Waste Piles		95.3	0.48	0.02	3.98	0	99.78	_	_	24.86		
3	27		C4-D4	98.88	0.25	0.81	80.0	0	100.02	3	_	n/a		
4	36				WORLD FOR BETWEEN THE WORLD THE COLUMN TO THE COLUMN TH									
5					A female or									
9		Sum	Summary for H2-G2 Sec 27 01	7 01	Additional company of the company of									Andreas Commission of the Comm
7			Name	# patches	sum length	avg size	std dev	% of total						
∞			bare ground	17	4765	317.67		95.300	24.86					Avidable de la company de la c
6			scrap iron	ı	2	2	1	0.040						
10			ground litter	4	24	9	5.83	0.480					The state of the s	
11			Loasaceae	ı	10	10	ŀ	0.200						
12			Indian Rice grass	8	199	24.86	25.72	3.980						A THE RESIDENCE AND A STREET AND A STREET AS A STREET
13					2000			100.000						
14														
15		Summa	Summary Statistics C4-D4 Sec 27 01	ec 27 01										
16			name	# patches	sum length	avg size	std dev	% of total						
17			bare ground	15	3955	263.67	230.82	98.875	3					
18			buckwheat	1	3	3		0.075						
19			mustard	1	2	2		0.050						
20			ground litter	3	10	3.33	4.04	0.250						
21			aster	П	3	3		0.075						
22			Tumbleweed	8	27	3.38	1.41	0.675						
23					4000			100.000						

Summary Section 27 transects

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APPENDIX F

Soil ICP-MS Uranium Data

						1								
Σ	u/ rsd	7.9	4.4	4.2	9.6	9.9		5.9	6.5			4.9	13.0	6.7
_	U / 238	7.1	923.1	961.4	33.6	4.7		86.1	104.4			2.0	0.0	2.5
¥	Ca / 44	0.0	13252.3	14227.7	0.0	10937.2		9051.6	10784.4			33459.4	57.1	286.3
ſ	Ca / 43	0.0	12645.6	13640.4	0.0	10253.8		9458.6	11040.4			32018.0	56.4	265.9
_	K / 39	0.0	2961.0	3069.2	0.0	9.0099		2527.8	3633.2			20052.0	14.3	278.4
I	Mg / 24	0.0	2099.2	2174.2	0.0	5420.7						14477.8	4.4	275.4
9	Na / 23	0.0	1376.7	1639.8	0.0	1408.5		854.4				2289.0	255.5	274.8
T	vol (ml)	20	20	20	20	20		20	20			20	20	50
Е	mass (g)	0.222	0.2489	0.2486	0.1950	0.2246		0.2789	0.2129			0.2116	1.0000	_
O	Date/Time:	10/1/2002 0:00	10/2/2002 0:18	10/1/2002 23:30	10/1/2002 0:00	10/1/2002 23:49		10/2/2002 0:04	10/2/2002 0:14			10/2/2002 0:28	10/2/2002 0:38	10/1/2002 23:11
ပ	sample point	දුද	12	12	4	-g-		h2	h4			brs sed	blank	
В	Sample:	866	875	867	868	869		873	874			876	877	CCV 50/5000/0.5
А	Total DF	91.11	5	5	91.11	2		91.11	91.11			ည	5	
	18	19	20	21	22	23	24	25	26	27	28	29	30	31

	Total DF Mass (Mass (g) Vol. (ml)	nl) Na / 23	Mg / 24	K/ 39	Ca / 43	Ca / 44	U / 238
0.1902	2	-	0.00	0.00	00.00	0.00	0.00	5.93
0.2709	Q	51.5		6965.52	11	9041.49	9452.12	5.01
0.2017	_	50	1472.73	6484.88	11056.02	7178.98	7578.09	4.94
0.26	,,	50						6.01
0.1736	اي	20			-			3.77
0.2037	<u> </u>	51	1546.02	6569.66	-+	10134.90	10643.15	2.70
0.2285	2	20	1557.11	7120.35		7505.47	7862.14	2.91
0.2046	ဖြ		1478.01	7035.68	11436.95	8558.16	8944.28	2.46
0.2319	တ	20						2.07
	Ì			THE RESERVE OF A PERSON AND PROPERTY AND PRO				
0.203	က	20		-				540.15
0.2248	∞	20	1267.35	1	(r)	14830.96	13959.07	410.81
0.194	4	_	0.00	\dashv	-	0.00	0.00	1467.27
0.2403	ဗျ	20	1419.48	1529.55	2630.05	16017.48	15201.83	869.95
0.186	ဖ	50						344.89
0.1986	യ്	50						211.73
0.24		20						284.79
0.2316	ဖ	50						187.72
0.2363	ಬ	50						270.21
0.2263	ಬ	20						218.80
0.2608	8	20						81.98
0.2504	4		540.14	748.20	1464.46	8274.76	7653.75	32.31
0.2451	Σ	20						50.86
0.2724	4		567.36	1748.53	2597.28	16360.13	15455.21	28.76
0.2522	7,4	50						65.66
0.2425	7,1	20						61.90
0.2405	~							59.81
0.2119	-							49.48
0.2313	က္							0.61
0.2471	7	20						0.73
0.2293	೮	50	1592.02	10632.36	3 14478.85	22001.74	22655.91	1.56
0.2195	35	20	1664.01	10867.88		22464.69	23257.40	1.85
0.2195	र्फ	20	1468.11	10223.23	3 14086.56	22291.57	21118.45	2.39
-		50	150.60	3.34	7.22	81.95	76.85	0.02
-		50						5.13
-		20	101.70	710.50	-	706.00	730.00	0.08
-		50	87.95	638.00	337.15	694.50	643.50	0.08
		50			-			
-		20	322.85	+-	-	330.70	347.50	2.37
_		50	320.45	-	341.70	329.80	350.30	2.40
-			Man and a second					

ppms36elemts	
Soil Surface Sample 36	

		(- Autobio				[1	
Total DF	Sample	Comple noint	Date/Time:	(v) 336m	la, low	Na / 22	Ma / 24	C: / 30	7 3d	C3 / 43	C3 / 44	11 / 228	N II	
105.9	1054	A1	9/6/2002	0.2448	55.25	861.93	4662.85		5005.90	8012.15	7456.94	16.50	3 24	o street
105.9	1064	A1 Dup	9/6/2002	0.1519	50	1026.66	4558.92	THE RESERVE THE PROPERTY OF TH	5069.12	6339.70	5816.33	19.44	8.56	2.08
5	1055	A2	9/6/2002	0.2571	20	1081.29	9105.41		5830.42	20458.97	20847.92	2.16	5.81	AND DESCRIPTION OF THE PERSON
5	1056	A3	9/6/2002	0.2291	20	1158.66	11082.50		5401.57	15128.76	15403.75	1.46	6.32	
2	1057	B1	9/6/2002	0.2495	54.5	1017.26	3152.04		3045.01	6963.77	7284.87	1.23	6.51	***************************************
105.9	1058	B2	9/6/2002	0.2171	52.75	1198.11	6249.33		5498.54	13298.05	12542.40	5.54	5.85	
2	1081	B2 dup	10/2/2002 3:13	0.0665	50	3297.74	7699.25	0.00	7235.34	15593.98	17180.45	3.83	4.5	1.21
2	1062	B3	9/6/2002	0.2157	20	942.05	7044.51		4601.30	11761.71	12167.36	3.15	7.49	***************************************
ı,	1050	2	0/06/3/0	0.0343	2	032.00	11320 40		1711 01	26569 50	27220 05	243	7 43	THE RESERVE AND ADDRESS OF THE PERSONS ASSESSED.
105.9	1060	5 8	9/6/2002	0.2343	28	1169 90	10133.06		7053.28	20818 51	19575.65	5.57	3.72	
91.11	1082	C2 dup	10/2/2002 3:28	0.0215	515	11526.42	9962.26	000	12506.12	24169.07	24720.00	5.89	5.34	0 23
105.9	1061	3	9/6/2002	0 2351	50	747 98	3145 47		4134 41	2235 22	2070 61	8.55	6.26	
2	1063		9/6/2002	0.212	20	911.32	14941.04		5719.34	27122.64	27783.02	1.95	6.56	
91.11	1067	D2	10/2/2002 0:57	0.2614	54.5	1269.51	8560,71	00'0	7449.45	17709.37	17250.69	11.56	9.22	
5	1068	D3	10/2/2002 1:11	0.2591	50	1396.37	4258.97	0.00	4376.69	25935.93	27016.60	1.45	3.65	
91.11	1066		10/2/2002 0:48	0.2283	20	1353.26	9691.20	00.00	5989.93	-	16579.06	5.56	8.36	
5	1069	E2	10/2/2002 1:21	0.2117	20	1659.90	12132.74	00.00	13167.22	-	12881.44	11.45	5.25	
91.11	1070	E3	10/2/2002 1:36	0.1765	20	1266.86	6838.53	0.00	9535.41	8671.39	8220.96	11.75	7.26	
2	1071	Σ	10/2/2002 1:41	0.2343	50	1415.49	8408.02	00:00	9974.39	7458.39	7859.58	5.41	9.1	
5	1076	F1 dup	10/2/2002 2:30	0.2033	20	1274.23	7385.64	0.00	8470.24	3735.86	4082.64	5.07	4.42	0.24
91.11	1072	F2	10/2/2002 1:56	0.2182	52.1	1012.63	10286.29	00.00	6377.59	17544.95	16799.98	2.71	90.9	
5	1073	F3	10/2/2002 2:00	0.2037	50	1286.70	4374.08	0.00	5638.19	4788.91	5225.82	6.07	3.77	
												WHICH THE PROPERTY OF THE PROP	THE RESIDENCE AND THE PARTY OF	
2	1074	55	10/2/2002 2:10	0.2073	20	1396.29	13663.77	0.00	7952.24	45224.31	46767.97	3.49	4.39	
91.11	1075	G2	10/2/2002 2:25	0.2134	54.1	1263.77	6705.46	0.00	6396.17	4276.79	4213.41	17.84	7.57	
ۍ ا	1083	63	10/2/2002 3:33	0.2409	09	1129.31	/015.36	0.00	8096.72	10695.31	11436.28	2.23	4.6	
50.7	1093	1	2/3/03 8:57 PM	0.2599	50.00	1405.35	7651.02	919.78	8003.08	4399.77	2745.29	17.31	2.25	
2.0	1094	71 9	Z/3/03 8:41 PM	0.2292	20.50	1505.75	13938.18	5440 74	7010.25	40300 00	77.53.77	3.07	3.44	
20.7	1095	H3.	Z/3/03 8:37 PM	0.2309	20.00	1526.81	9230.66	5149.54	/318.6/	10309.38	9284.98	10.72	3.78	
50.7	1006	_	2/3/03 10·32 DM	0 1700	50.00	1700 59	8305 88	7061 78	7847 06	5591 18	1914 41	15.64	3 10	
50.7	1097		2/3/03 10:32 I M	0.11.00	50.00	1240.23	11325 32	4153 32	9692 98	8747 14	6305 88	4.23	4.03	
50.7	1098	2 8	2/3/03 10:02 PM	0.1866	50.00	1837.08	11122.72	5988.75	13140.41	14957.13	11446.95	17.19	3.43	
5.0	1099		2/3/03 9:47 PM	0.1608	50.00	1935.32	16620.02	6741.29	9123.13	24365.67	24070.27	4.58	1.88	
5.0	1102	32	2/3/03 11:27 PM	0.1848	57.00	1825.67	11106.98	6579.06	10055.19		11116.23	3.96	2.25	
5.0	1103	J3	2/3/03 11:17 PM	0.1426	55.00	2259.78	9923.91	8732.12	10174.61	8573.98	8454.42	7.03	1.45	
50.7	1104	조	2/3/03 11:12 PM	0.1658	54.00	1790.99	15353.20	8308.44	12884.44		70512.67	18.57	1.43	
50.7	1105	K2	2/3/03 11:02 PM	0.1518	50.00	1655.14	9868.25	8122.53	9575.10		4291.83	7.57	1.46	PORTER PROPERTY AND ADDRESS OF THE PERSON NAMED IN COLUMN NAME
50.7	1106	\$	2/3/03 10:52 PM	0.2109	50.00	1401.61	11017.07	1581.32	10149.36		13259.84	5.91	3.86	
50.7	1107	ב	2/3/03 10:42 PM	0.3154	55.00	1134.18	7697.21	3201.65	6373.65	15012.52	13920.89	6.95	2.92	
50.7	1108	L2	2/4/03 12:43 AM	0.2286	52.00	1206.28	6885.56	5163.60	6719.51	6594.40	3748.73	9.98	2.34	
5.0	1109	F3	2/4/03 12:28 AM	0.3070	56.00	1074.76	5184.10	4064.10	5353.75		3921.82	2.62	1.61	
5.0	1113	T3 dnb	2/3/03 11:37 PM	0.3063	20.00	477.96	5169.77	4513.55	5527.26	3586.35	3576.56	2.38	0.0	0.17
	According to the second					1, 10,	0000		00.000	0000	1 00,0		ı	
50.7	1110	M1	2/4/03 12:23 AM	0.2724	58.00	1167.45	7203.16	2081.10	6724.08	5108.00	2499.71	4.28	3.65	
5.0	1111	M2	2/4/03 12:07 AM	0.2393	20.00	814.67	4059.76	6318.43	4987.46	2927.29	2887.59	2.07	1.75	
50.7	1112	M3	2/3/03 11:53 PM	0.2802	22.00	1106.67	7818.17	5132.94	7221.45	3694.15	1353.02	5.54	2.51	
u	4077	72014	40/0/0000 0:30	-	60	402.05	2 05	00	14.22	50.45	08 08	300	CV V	The state of the s
0 4	10//	Dialik	10/2/2002 2:39	-	200	192.03	30.00	00.00	17 14	59.13	64.70	0.03	24.46	
٠.	1089	biank	10/2/2002 3:53	-	20	167.40	3.00	0.00	17.14	02.20	04.10	0.01	3.01	



0													0.03				90.0		0.00	
z	10.42	3.13	6.11		34.55	11.11	18.06	33.63	31.65	39.01	38.74	5.07	6.83	0.85	2.04	0.97	0.73	2.8	0.41	0.19
Σ	0.01	1.83	1.36		0.00	0.00	0.00	90.0	0.01	0.01	0.01	2.5135	2.468	13.28	13.36	13.23	13.34	1.03	1.03	13.25
٦	17.62	25779.48	23127.84		433.10	0.00	0.00					290.9	292.5	1237.00	1222.50	1260.75	1290.75	72.05		1263.75
×	68.80	25629.69	22326.60 23127.84		1044.00			1.77	1.25	1.01	1.36	266.1	271.05	1196.25	1240.25	1261.75	1286.75	128.48	103.48	1246.25
7	7.51	18104.00	13725.12			0.77				0.90	1.14	282.75	289.65	1284.00	1352.00	1400.50	1449.00	156.08	136.18	1440.75
_		6735.41				0.00						0	0	279.50	205.23	226.35	259.00			255.75
I	3.36	12677.97	10364.22		0.02	0.14		1.76	1.43	1.22	1.26	277.6	272.75	1249.50	1327.25	1386.25	1456.00	152.15	133.08	1388.75
9	234.20	2134.52	1396.77		7.28	0.15		55.58	8.32	1.36	1.40	273.65	271.35	1303.00	1346.25	1398.25	1460.50	150.60	141.65	1375.00
ட	50.00	55.50	53.9		50.00	50	20	50.00	50.00	50.00	50.00	50	20	50.00	50.00	50.00	50.00	50.00	50.00	50.00
Е	1.0000	0.2149	0.2489		1.00	_	-	0.20	0.20	0.20	0.20	-	-	0.20	0.20	0.20	0.20	0.20	0.20	0.20
D	2/3/03 9:42 PM	2/3/03 9:32 PM	9/6/2002		2/3/03 8:27 PM	10/2/02 1:07 AM	10/2/02 2:58 AM	2/3/03 8:22 PM	2/3/03 10:12 PM	2/4/03 12:02 AM	2/4/03 1:03 AM	10/2/02 1:02 AM	10/2/02 2:54 AM	2/3/03 8:17 PM	2/3/03 10:07 PM	2/3/03 11:58 PM	2/4/03 12:58 AM	2/4/03 12:48 AM	2/4/03 12:53 AM	2/4/03 1:07 AM
C	blank	BRS std	Buf Riv Sed		BLANK	Blank Rinse	CCV 50/5000/0.5	CCV 50/5000/0.5	CCV 50/5000/5	CCV 50/5000/5	CCV 50/5000/5	CCV 50/5000/5	ECS 5 ppb	ECS 5 ppb	ICV 50/5000/5					
В	1100	1101	1065		ICP internal check															
∢	5.0	5.0	5		1.00	τ-	-	1.00	1.00	1.00	1.00	τ-	-	1.00	1.00	1.00	1.00	1.00	10.14	1.00
	22	26	22	28	29	9	61	62	63	64	92	99	29	89	69	20	71	72	73	74

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Soil Surface Samples (27 s27smetals_ppm

2	stdev	The state of the s									0.49						23.74							86.35				11.73		1.49							30.51		32.40		
ø	u/rsd												7.88											4.35		4.19		9.55		6.61							5.9		6.48		
۵.	U / 238	163.9	7.3		50.7	11.2	4.6	174.4	13.8	113.1	113.8	10.7	7.1		621.9	96.2	62.6	8.1	71.6	26.3	6.6		963.0	923.1	1117.9	961.4	50.2	33.6	6.8	4.7	139.5	58.9	56.5	63.5		129.2	86.1	150.2	104.4		
0	Th / 232	7.1	11.3		8.2	13.9	8.1	6.4	14.8	4.2	4.2	12.9	9.6		6.8	5.2	16.3	8.7	3.9	3.0	10.9		5.7	3.5	5.9	3.3	8.6	5.7	10.1	6.9	5.0	4.9	4.6	7.4		5.1	2.5	6.4	3.1		
z	Pb / 208	12.8	17.1		14.0	20.0	10.3	8.9	20.0	7.3	7.3	234.5	186.3		23.0	7.7	6.1	61.2	10.9	11.5	19.5		51.7	45.9	60.3	48.1	39.4	29.5	51.5	41.4	17.0	19.0	19.2	29.9		16.3	11.8	21.0	15.8		
Σ	Se / 82	27.0	2.9		6.1	3.2	1.3	5.9	2.7	6.5	6.5	3.4	10.5		6.8	3.9	3.1	2.0	2.5	3.1	1.2		27.9	63.7	18.8	40.4	6.0	13.1	1.8	2.2	6.3	9.8	9.0	7.3		16.7	36.6	6.6	22.4		
	As / 75	10.8	3.9		3.8	4.1	2.2	4.0	3.8	3.9	4.1	4.8	10.1		2.3	4.1	3.0	3.8	4.7	4.0	4.4		7.8	15.0	7.4	13.5	4.8	8.7	3.4	6.3	4.1	7.0	7.7	4.6		4.7	8.2	5.5	10.3		_
¥	2n / 66	28.2	28.8		20.5	36.1	16.9	8.7	38.8	181.4	198.5	63.4	165.2		22.9	10.2	8.5	33.0	16.3	14.8	34.5		24.0	52.2	23.5	48.5	35.4	70.3	33.4	69.2	12.2	15.8	16.7	22.6		17.9	35.0	24.4	46.7		
٦	Cu / 63	13.9	11.0		7.4	12.8	5.4	3.8	14.2	6.1	6.9	13.5	23.1		29.3	3.6	3.5	9.6	2.1	4.0	10.3		5.1	7.9	5.4	8.3	9.3	11.7	7.8	11.8	2.8	4.0	4.9	6.2		3.6	5.9	4.8	6.4		-
_	Fe / 56	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	28536.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	9674.6	0.0	9288.0	0.0	18559.0	0.0	17003.6	0.0	0.0	0.0	0.0		0.0	8277.2	0.0	9375.3		
I	Mn / 55	282.3	148.2		121.8	151.4	114.5	120.0	139.5	155.1	178.0	172.4	247.3		205.5	162.1	194.3	187.5	115.6	126.5	170.3		149.0	239.5	162.2	249.4	193.6	206.7	164.1	246.2	273.6	210.0	169.8	164.4		153.8	163.1	164.1	177.1		
၅	V / 51	124.4	52.8		70.5	7.77	27.9	71.1	81.4	86.0	97.9	62.7	82.4		59.9	48.2	37.7	53.5	50.5	56.4	56.6		158.2	241.5	201.0	288.2	79.9	77.5	39.4	57.9	103.3	80.1	62.3	124.5		144.5	140.4	111.3	110.9		
ш	(ml) lov	20	20	-	20	20	20	20	20	20	20	20	20		20	20	50	20	20	20	20		20	20	20	20	20	20	20	50	20	20	20	20		20	20	20	20		
ш	mass (g)	#######################################	0.1952		0.2113	0.1784	0.2605	0.3202	0.1640	0.2014	0.2014	0.2220	0.222		0.1883	0.2385	0.2288	0.1889	0.2326	0.2055	0.2263		0.2489	0.2489	0.2486	0.2486	0.1950	0.1950	0.2240	0.2246	0.2460	0.2133	0.2133	0.2474		0.2789	0.2789	0.2129	0.2129		
0	Date/Time:	6/6/2002 21:12			6/7/2002 13:05	6/7/2002 13:11	6/7/2002 13:16	6/7/2002 13:22	6/7/2002 13:28	6/7/2002 13:33	6/7/2002 14:42	7/23/2002 15:43	10/1/2002 0:00		6/7/2002 13:39	6/7/2002 13:45	6/7/2002 13:51	7/17/2002 18:03	7/17/2002 18:09	7/17/2002 18:15	7/17/2002 18:33		7/23/2002 16:29	10/2/2002 0:18	7/23/2002 15:48	10/1/2002 23:30	7/23/2002 15:54	10/1/2002 0:00	7/23/2002 16:11	10/1/2002 23:49	6/7/2002 13:56	6/7/2002 14:14	6/10/2002 12:26	6/7/2002 14:19		7/23/2002 16:17	10/2/2002 0:04	7/23/2002 16:23	10/2/2002 0:14		
၁	sample point	a1	a3		b2	P 4	င္	દ	ន	2	Z	පි	55		d2	4 5	d4	-e1	e1	63	e5		12	12	12	12	f4	4	-01	-g.1	g1	93	8	g2		h2	h2	44	h4		
В	Sample:	829	830	Transactive management and a second s	831	832	833	834	835	836	836	866	998		837	838	839	896	897	868	899	grighe i Aint bh'impleisinn magannin an gan an a	875	875	298	867	868	868	869	698	870	871	871	872	manufactions and becaming them as a second s	873	873	874	874		
Α	Total DF								THE PERSON NAMED IN COLUMN 2 I				91.11											5		5		91.11		5							91.11		91.11		
_	-	2	က	4	2	ဖ	7	∞	6	9	=	12	13	14	15	19	12	8	19	8	21	22	23	24	52	56	27	82	53	င္က	31	32	33	34	35	36	37	88	ဓ္ဌ	40	7

			L		ļ	L		1	1	<u> </u>		<u></u>	_	<u></u>					<u>_</u>		<u> </u>	-									<u> </u>	 		
Ø					4.92		12.96		THE REAL PROPERTY AND ADDRESS OF THE PERSON NAMED IN COLUMN 1																	6.68								
۵	0.1	2.5	2.6	2.5	2.0	1.0	0.0	0.7	2.9	2.8	6.5	6.5	4.2	4.2	0.4	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	2.5	0.0	0.0	0.0	0.0	0.0			
0	0.2	10.3	10.4	10.3	8.3	0.5		6.7	13.0	12.6	14.6	14.6	12.1	12.1	2.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0			
z	0.2	166.1	172.7	166.1	173.0	0.1	0.1	159.6	15.7	15.7	15.6	15.2	14.9	14.7	1.5	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	2.2	0.0	0.0	0.0	0.0	0.0			
Σ	0.4	1.3	1.4	1.3	1.5	0.2	0.0	0.3	5.7	6.5	5.4	5.3	4.9	4.9	0.4	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	2.6	0.0	0.0	0.0	0.0	0.0			
_	0.2	6.3	9.9	6,3	17.1	0.0		6.1	16.3	18.5	14.1	12.7	13.4	13.4	1.6	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	2.5	0.1	0.0	0.1	0.1	0.1			
х	1.9	127.6	125.3	127.6	390.1	2.2	3.0	131.5	94.0	122.2	93.9	87.1	75.5	74.2	9.5	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0		2.6	0.1	0.1	0.1	0.1	0.1			
7	1.1	43.6	45.1	43.6	94.7	0.4	0.4	41.8	45.8	62.6	44.1	43.2	50.0	49.6	9.9		0.0	0.1	0.1	0.1	0.0	0.0		0.0		2.4	0.0	0.0	0.0	0.0	0.0			
_	0.0	0.0	0.0	0.0	49456.5	0.0	15.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	271.4	0.0	0.0	0.0	0.0	0.0			
ı	0.3	313.1	334.6	313.1	669.7	0.1	0.1	289.4	413.1	573.5	410.0	462.8	342.4	343.1	49.4	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	2.7	0.0	0.0	0.0	0.0	0.0			
ဖ	0.7	51.4	62.5	51.4	115.8	0,4		44.7	84.7	115.5	83.5	6.86	75.4	74.7	10.7	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	2.7	0.0	0.0	0.0	0.0	0.0			
ц.	50	22	20	S S	22	20	20	20	200	200	200	200	200	200	22	-		-	-	-	-		-	-	-	22	-		-	-	-			
ш	1.0000	0.2116	0.2116	0.2116	0.2116	1.0000	1.0000	0.2471	0.5003	0.5003	0.5003	0.5003	0.5006	0.5006	0.5006	-	1	-		-	Ψ-	-	-	-	1	-	1	-	-	1	-			
O	6/6/2002 21:06	7/23/2002 16:34	7/23/2002 21:36	7/23/2002 16:34	10/2/2002 0:28	7/23/2002 16:40	10/2/2002 0:38	7/17/2002 18:46	6/6/2002 17:02	6/6/2002 21:23	6/7/2002 12:19	6/7/2002 14:31	6/10/2002 12:21	6/10/2002 14:59	7/23/2002 17:09	6/7/2002 12:08	6/10/2002 12:09	7/23/2002 17:15	7/17/2002 17:38	7/23/2002 16:00	6/7/2002 14:02	6/10/2002 14:06	6/7/2002 14:08	6/10/2002 14:12	7/23/2002 16:05	10/1/2002 23:11	6/7/2002 12:14	6/7/2002 14:25	6/10/2002 12:15	6/10/2002 14:53	7/23/2002 17:03			
ט	blank				prs sed		blank	prs sed																										
n	827	876	876	876	876	877	877	901	2709	2709	2709	2709	2709	2709	2709	100 ppb	100 ppb	100 ppb check	100 ppb QC	100 ppb QC	20 ppb QC	20 ppb QC	Blank Rinse	Blank Rinse	Blank Rinse	CCV 50/5000/0.5	mojo 1/10	mojo 1/10	mojo 1/10	mojo 1/10	mojo 1/10			

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>	stdev	0.65				0.14				91.46	422.36		51.66	***************************************									1.47																					-
_	U / 238	5.47	4.94	6.01	3.77	2.80	2.46	2.07		475.48	1168.61	344.89	248.26	187.72	270.21	218.80		81.98	32.31	50.86	28.76	65.66	60.85	49.48		0.61	0.73	1.56	1.85	2.39	0.02	5.13	0.08	0.08		2.37	2.40	0.26						
_	depth	0	5	10	15	20	25	30		0	5	9	15	20	25	30		0	5	10	15	20	25	30																				
S	S27 point	9	1-5	1-10	1-15	1-20	1-25	1-30		2-0	2-5	2-10	2-15	2-20	2-25	2-30		3-0	3-5	3-10	3-15	3-20	3-25	3-30		std	std	std	std	std	blank	100 ppb	std	std	std	std	std	std						
×																																	-											
3	U / rsd		1.44	6.93			7	6.3	6.12				5.23		2.93									5.66		8.23								7.23	5.37	10.64	3.8		7.36	4.81		8.22	5.89	
7	U / 238	5.93	5.01	4.94	6.01	3.77	2.70	2.91	2.46	2.07		540.15	410.81	1467.27	869.95	344.89	211.73	284.79	187.72	270.21	218.80		81.98	32.31	50.86	28.76	99:59	61.90	59.81	49.48		0.61	0.73	1.56	1.85	2.39	0.02	5.13	0.08	0.08		2.37	2.40	
	Th / 232	12.48	11.51	11.11	12.60	11.54	11.09	11.54	11.95	12.37		2.56	4.07	3.43	3.37	2.90	4.04	3.97	5.05	3.40	2.98		4.17	2.33	2.27	3.77	3.94	3.21	22.04	2.65		6.46	69.9	6.44	6.38	6.29		5.41	0.43	0.42	0.33	2.33	2.30	
Z	Pb / 208	23.41	18.99	15.97	23.19	20.64	15.61	16.02	17.04	24.58		10.50	7.53	22.25	8.84	8.30	10.05	11.85	12.38	15.52	10.45		5.93	2.34	5.60	3.92	8.67	6.37	6.43	7.09		146.37	159.55	120.02	119.52	107.38	0.05	5.21	0.56	0.48	0.53	2.10	2.10	
Σ	Se / 82	0.85		2.81	0.68	0.54	1.37	1.38	1.32	0.59		110.96	83.81	33.40	145.59	19.73	8.33	8.23	5.28	28.29	40.50		15.98	15.74	38.31	8.39	7.09	9.16	7.13	6.14		0.47	0.33	1.13			0.01	5.01	0.05			2.44	2.30	
7	As / 75	3.54	8.44	7.67	3.63	4.36	7.92	8.11	7.98	4.15		11.65	9.97	7.81	15.87	7.66	6.01	7.12	4.96	10.85	6.50		5.55	0.43	5.97	9.60	7.45	4.54	4.19	6.80		99.9	60.9	13.09	13.32	13.29		5.45	0.68		69.0	2.37	2.28	
۷	2u / ee	39.14	82.64	74.91	34.65	38.77	78.72	96.77	79.30	34.58		11.84	19.46	15.93	23.35	16.68	20.40	15.90	14.69	12.48	14.80		8.49	18.60	7.54	17.21	15.85	51.34	11.82	9.08		144.73	131.49	302.22	317.08	362.64	0.52	4.36	3.97	4.11	4.80	2.37	2.34	
,	Cn / 63	12.05	19.56	17.65	11.14	12.16	18.14	17.64	18.39	10.88		4.60	4.11	2.73	4.07	3.96	3.65	3.21	4.04	4.37	2.73		3.44	4.47	1.94	3.80	2.08	2.70	2.19	3.95		44.12	41.78	67.51	72.35	73.62	0.33	4.98	1.35	1.25	2.40	2.15	2.16	
+	Fe / 56	0.00	31348.65	29647.99	00.00	0.00	31120.77	31247.26	31573.80	0.00		0.00	8138.35	0.00	8707.87	0.00	0.00	0.00	00.00	0.00	00.00		00.00	6070.29	0.00	8616.01	0.00	0.00	0.00	0.00		0.00	00.0	34387.27	35148.06	37175.40	13.84	0.00	1507.00	1575.00	0.00	336.40	340.95	
Е.	Mn / 55	177.97	318.05	222.86	146.06	198.04	304.20	239.39	229.96	140.15		229.41	262.68	262.11	283.60	159.62	200.63	164.71	231.00	136.99	156.19		207.82	144.33	150.49	266.52	238.30	172.23	142.62	199.46		303.07	289.36	471.65	485.88	453.99	0.05	5.36	20.07		25.48	2.52	2.55	
פ	V / 51	71.56	102.68	95.79	90'59	68.15	95.99	97.99	99,63	64.25		240.49	226.87	246.08	248.65	168.63	121.35	141.75	119.17	175.33	138.58		59.74	40.36	83.52	46.77	261.70	58.58	78.73	42.54		44.96	44.68	79.76	80.91	63.10		5.35	4.96	4.10	4.98	2.45	2.48	
L	Vol. (ml)	20	51.5	22	20	င္သ	51	20	20	20		20	20	20	20	22	20	20	20	S	90		90	20	20	20	20	20	20	20		20	50	20	50	20	90	20	90	20	20	20	9	
u	Mass (g)	0.1902	0.2709	0.2017	0.26	0.1736	0.2037	0.2285	0.2046	0.2319		0.203	0.2248	0.194	0.2403	0.186	0.1986	0.24	0.2316	0.2363	0.2263		0.2608	0.2504	0.2451	0.2724	0.2522	0.2425	0.2405	0.2119	-	0.2313	0.2471	0.2293	0.2195	0.2195	-	-	-	-	-	-	1	
	Total DF		5	5			2	5	5				105.9		105.9									105.9		105.9								S	2	105.9	2		-	21.18		-	-	
ر	sample point	1-0	1-0 dup	1-5	1-10	1-15	1-20	1-20 dup	1-25	1-30		2-0	2-0 dup	2-5	2-5 dup	2-10	2-15	2-15 dup	2-20	2-25	2-30		3-0	3-5	3-10	3-15	3-20	3-25	3-25 dup	3-30		std	std	std	std	std	blank	100 ppp	std	std	std	std	std	Andrews of the Assessment of the Party of th
1	Date/Time:	7/17/02 4:01 PM	9/6/02 4:54 PM	9/6/02 5:03 PM	7/17/02 4:07 PM	7/17/02 4:13 PM	9/6/02 5:13 PM	9/6/02 6:20 PM	9/6/02 5:22 PM	7/17/02 4:19 PM		7/17/02 4:25 PM	9/6/02 6:06 PM	7/17/02 4:31 PM	9/6/02 6:16 PM	7/17/02 4:37 PM	7/17/02 4:44 PM	7/17/02 5:02 PM	7/17/02 4:50 PM	7/17/02 4:56 PM	7/17/02 5:14 PM		7/17/02 5:20 PM	9/6/02 5:46 PM	7/17/02 5:26 PM	9/6/02 5:56 PM	7/17/02 5:32 PM	7/17/02 5:51 PM	7/17/02 6:40 PM	7/17/02 5:57 PM		7/17/02 5:08 PM	7/17/02 6:46 PM	9/6/02 6:30 PM	9/6/02 6:40 PM	9/6/02 6:45 PM	9/6/02 6:49 PM	7/17/02 5:38 PM	9/6/02 7:04 PM	9/6/02 7:09 PM	7/17/02 6:21 PM	9/6/02 5:32 PM	9/6/02 7:13 PM	CANADA MANAGEMENT AND
	Sample:			947	-		948	-	_			_	952		_	884		888			890		-		892		893		_	895			901				2967	100 ppb QC	2709	-		CV 50/5000/C	CV 50/5000/c	
	Ŧ	2	ო	4	2	9	7	8	6	9	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	58	30	ઝ	32	33	34	32	36	37	38 10	33	9		42 CV	43 CV	



œ	U stdev		2.08				,	1.2.1					0.23									0.24											Andreadan and the state of the												0.17				***************************************
ø	%ps. ∩	3.24	8.56	5.81	6.32	6.51	5.85	4,5	7.49	1	1.43	3.72	5.34	6.26	6.56	9.22	3.00	8.36	5 25	7.26	9.1	4.42	90.9	3.77		4.39	7.57	4.6	2.25	3.44	3.18	0, 0	3.19	4.03	3.43	2.00	1.45		1.43	1.46	3.86	2.92	2.34	1.61	6.0	10.0	3.65	1.75	2.51
۵	U / 238	16.50	19.44	2.16	1.46	1.23	5.54	3,83	3.15	97.0	2.13	5.57	5.89	8.55	1.95	11.56	1.40	5.56	11.45	11.75	5.41	5.07	2.71	6.07		3.49	17.84	2.23	17.31	3.07	16.72	, ,	15.64	4.23	17.19	00.4 AQ	7.03		18.57	7.57	5.91	6.95	9.98	2.62	2.38	00,	4.28	2.07	5.54
0	Th / 232	3.97	3.95	5.48	5,93	2.64	4.32	4.12	4.93		5.05	6.35		3.92	90.9	5.54	3.14	631	861	5.81	7.04	6.34		4.05		79.7	5.49	5.04	6.37	7.41	5.65	1	5.94	7.45	8.22	4. c	6.55		6.83	7.11	7.37	5.10	4.46	3.86	3.93	7.	4.71	4.22	6.71
z	Pb / 208	8.87	2.68	7.38	9.11	4.46	5.88	/0./	7.40	1	4.34	8.28	12.46	5.60	8.71	16.22	15.0	10.49	15.77	12.73	13.04	11.88	9.78	7.68		11.64	12.15	7.34	15.30	15.06	11.48	00 17	15.69	13.89	16.44	14 14	13.02		17.27	14.04	10.82	9.85	8.24	7.53	7.52	0	9.86	7.23	11.32
Σ	Se / 82	19.45	15.02	0.78	09.0	1.55	1.11		2.14	20	L9:0	2.04		7.38	0.52	6.90		1 39	2 63	4 39	1.26		1.64	1.51		3.24	4.94	1.22	2.31	1.31	4.78	1	5.57	1.84	5.19	4.13	2.29		3.25	1.74	2.05	4.19	1.23	0.82	0.81		1.86	0.85	1.40
1	As / 75	5.85	7.86	3.44	3.32	2.01	5.24	20.0	4.91	200	3.05	2.55		4.69	4.15	4.41	7.50	4.52	5 82	4.61	5 09		6,26	2.81		8.64	4.84	3.85	5.39	76.7	4.77	.,	5.15	8.51	7.22	20.0	609		9.17	12.16	7.47	5.03	4.39	4.13	4.42		4.38	4.14	7.20
¥	Zu / 66	18.71	20.51	33.99	33.48	17.88	21.53	03.00	31.34	70.70	31.84	33.95	207.60	29.09	33.40	45.51	74.01	36.88	57.63	53.40	44 64	38.96	35.17	29.28		40.30	46.82	37.19	56.02	59.07	58.54	e e	78.76	65.56	86.25	20.00	58.59		102.59	51.25	47.23	46.63	39.44	46.39	44.91	0000	39.88	28.58	43.10
٦	Cu / 63	7.00	7.32	6.13	22.98	5.16	8.09	17.09	7.05	3	b.04	5.59	32.03	6.33	0.9	10.65	0.33	898	13.84	13.48	11 49	10.00	8.64	8.67		12.01	10.57	7.85	11.23	9.91	15.11	1	15.27	12.78	15.82	11 87	12.86		24.24	11.24	8.97	8.30	7.62	69'9	5.62		7.54	5.82	8.67
_	Fe / 56	10693.40	10780.12	12024.50	13077.26	7097.01	12328.58	120/0.09	11961.06	4440400	11124.63	16032.08	17833.37	11144.19	13674.53	15132.40	10082.98	13771 35	24492 24	16951 84	19545 45	17533 20	12936.65	12042.22		19290.88	15271.72	13731.84	15565.60	16544.70	12194.91	10000	15867.65	18525.93	22534.83	18380 20	16523.14		19600.24	19855.07	17828.35	13464.01	12183.38	9844.69	9784.52		12140.82	10068.95	15602.96
I	Mn / 55	156.11	148.19	144.85	170.23	101.97	155.29	134.00	152.97	70707	137.26	156.96	152.99	126.69	133.28	128.95	186.80	155.32	273.64	212.24	308.37	257.26	148.71	204.76		173.37	217.72	205.50	262.02	194.00	234.96		269.74	246.57	534.57	221.02	222.14		337.09	295.16	219.35	295.23	215.12	136.22	135.18		192.29	167.26	198.05
9	V / 51	227.05	217.38	27.15	25.10	16.85	94.57	107.33	103.59	17.00	22.75	40.28	64.96	310.29	22.88	33.21	75.37		80 AB	38 13	25.44	32.64	29.85	24.45		35.79	37.11	26.88	34.82	35.16	28.89		38.09	38.31	48.26	45.52	36.61		60.25	39.62	35.23	29.68	26.09	24.46	19.75		25.27	22.46	30.15
L.	vol (ml)	55.25	20	20	29	54.5	52.75	200	22	S	2	28	51.5	20	22	54.5	2	50	20	3 6	20	50	52.1	50		22	54.1	50	50.00	50.50	50.00		50.00	50.00	50.00	20.00	55.00		54.00	50.00	50.00	55.00	52.00	56.00	50.00		58.00	50.00	55.00
ш	mass (g)	0.2448	0.1519	0.2571	0.2291	0.2495	0.2171	0.0000	0.2157	0,00	0.2343	0.2226	0.0215	0.2351	0.212	0.2614	U.Z591	0.2283	0.2447	0.4117	0 2343	0 2033	0.2182	0.2037		0.2073	0.2134	0.2409	0.2599	0.2292	0.2909	1	0.1700	0.2622	0.1866	0.1008	0.1040		0.1658	0.1518	0.2109	0.3154	0.2286	0.3070	0.3063		0.2724	0.2393	0.2802
D	Date/Time:	9/6/2002	3/6/2002	9/6/2002	9/6/2002	3/6/2002	9/6/2002	10/2/2002 3:13	9/6/2002	000000	3/6/2002	9/6/2002	10/2/2002 3:28	9/6/2002	9/6/2002	10/2/2002 0:5/	10/2/2002 1:11	10/2/2002 0:48	10/2/2002 1:21	10/2/2002 1.21	10/2/2002 1:41	10/2/2002 2:30	10/2/2002 1.56	10/2/2002 2:00		10/2/2002 2:10	10/2/2002 2:25	10/2/2002 3:33	2/3/03 8:57 PM	2/3/03 8:41 PM	2/3/03 8:37 PM		2/3/03 10:32 PM	2/3/03 10:22 PM	2/3/03 10:02 PM	2/3/U3 9:47 PM	2/3/03 11:2/ FIM		2/3/03 11:12 PM	2/3/03 11:02 PM	2/3/03 10:52 PM	2/3/03 10:42 PM	2/4/03 12:43 AM	2/4/03 12:28 AM	2/3/03 11:37 PM		2/4/03 12:23 AM	2/4/03 12:07 AM	2/3/03 11:53 PM
C	sample point	A1	A1 Dup	A2	A3	B4	B2	dno zg	B3	7	5	22	C2 dup	ឌ	50	70.5	3	1	123	7 6	1	F1 din	F2	F3		61	62	83	H	H2	H3		=	12	<u>e</u>	5 5	20 (5)	The same of the sa	Σ	2	చ	7	77	L3	T3 qnb		Ä.	M2	M3
8	Sample:	1054	1064	1055	1056	1057	1058	1001	1062	4000	601	1060	1082	1061	1063	106/	1008	1066	1060	1070	1071	1076	1072	1073		1074	1075	1083	1093	1094	1095	A STATE OF THE PERSON NAMED IN COLUMN NAMED IN	1096	1097	1098	1088	1103		1104	1105	1106	1107	1108	1109	1113		1110	1111	1112
A	Total DF	105.9	105.9	5	2	2	105.9	c	2	ı	c	105.9	91.11	105.9	2	91.11	n	91 11	u	91 11		2 10	91.11	2	-	S	91.11	2	50.7	5.0	50.7		50.7	50.7	50.7	0.0	0, 0,	2	50.7	50.7	50.7	50.7	50.7	5.0	5.0		50.7	5.0	50.7
		4	က	4	2	و	4	0	ი ;	2;	4	4	_	_	4	_	- e	_	╀	_	+	33	1	Ļ	26	27		58	30	31	32	က္က	34	32	38	<u>ئ</u> و	ရှင်	9	14	42	43	44	45	46	47	48	49	20	51

Soil Surface Samples S 36 ppms36smetal

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Ö	4.42	3.01	10.42	3.13	6.11		34.55	11.11	18.06	33.63	31.65	39.01	38.74	5.07	6.83	0.85	2.04	0.97	0.73	2.8	0.41	0.19
Ь	0.05	0.01	0.01	1.83	1.36		0.00	00.00	00.0	90.0	0.01	0.01	0.01	2.5135	2.468	13.28	13.36	13.23	13.34	1.03	1.03	13.25
0		0.01		6.45	6.05		0.00	0.00		0.02	0.01	0.01	0.01	2.019	1.919	13.26	13.42	13.25	13.33	0.84	0.83	13.01
z	0.05	0.04	0.09	210.74	119.88		0.00	0.00		0.02	0.02	0.01	0.01	2.1675	2.0775	11.43	11.26	10.90	10.91	1.07	1.03	10.83
Σ				2.00	1.18	-				-0.05	0.02	0.04	0.02	0	2.5585	13.77	12.61	12.38	12.55	1.20	1.23	12.57
Γ				16.93	13.68					0.02	0.04	0.05	0.04	0	2.502	12.90	12.28	12.16	12.37	1.19	1.48	12.43
Y	69.0	2.76	4.64	436.98	316.60		-0.03	0.00	0.00	90.0	0.05	0.05	90.0	0	2.522	12.48	12.51	12.41	12.61	1.15	0.07	12.44
7	0.72	0.49	0.62	80.14	82.27		0.05	0.00	0.00	0.32	60'0	0.03	0.02	0	2.36	10.72	10.41	10.36	10.48	1.14	96.0	10.41
1	16.92	12.48		37447.65	34865.01		-0.67	90'0	0.21	-1.81	-2.73	-2.08	-1.55	0	271	8.59	9.31	10.14	10.46	117.73	96.68	10.56
н	0.10	90.0	0.44	546.74	477.93		90.0	2.75		0.40	0.28	0.28	0.29	0	2.7435	12.64	12.74	12.98	13.30	1.47	3.89	12.74
G	0.23		6.94	87.55	78.61		6.27			0.15	0.11	0.13	0.14	2.738	2.745	11.98	12.06	12.52	12.87	0.95	1.50	12.92
L.	20	20	50.00	55.50	53.9		50.00	50	50	50.00	50.00	50.00	50.00	50	90	50.00	50.00	50.00	50.00	50.00	50.00	50.00
ш	1	,- -	1.0000	0.2149	0.2489		1.00	-	-	0.20	0.20	0.20	0.20	1	Ţ	0.20	0.20	0.20	0.20	0.20	0.20	0.20
D	10/2/2002 2:39	10/2/2002 3:53	2/3/03 9:42 PM	2/3/03 9:32 PM	9/6/2002		2/3/03 8:27 PM	10/2/02 1:07 AM	10/2/02 2:58 AM	2/3/03 8:22 PM	2/3/03 10:12 PM	2/4/03 12:02 AM	2/4/03 1:03 AM	10/2/02 1:02 AM	10/2/02 2:54 AM	2/3/03 8:17 PM	2/3/03 10:07 PM	2/3/03 11:58 PM	2/4/03 12:58 AM	2/4/03 12:48 AM	2/4/03 12:53 AM	2/4/03 1:07 AM
C	blank	blank	blank	BRS std	Buf Riv Sed		BLANK	Blank Rinse	Blank Rinse	CCV 50/5000/0.5	CCV 50/5000/0.5	CCV 50/5000/5	CCV 50/5000/5	CCV 50/5000/5	CCV 50/5000/5	ECS 5 ppb	ECS 5 ppb	ICV 50/5000/5				
В	1077	1089	1100	1101	1065		ICP internal check	ICP internal check	ICP internal check	ICP internal check	ICP internal check	ICP internal check	ICP internal check	ICP internal check	ICP internal check	ICP internal check	ICP internal check					
4	2	5	5.0	5.0	5		1.00		-	1.00	1.00	1.00	1.00	1	-	1.00	1.00	1.00	1.00	1.00	10.14	1.00
	23	24	22	26	57	28	29	9	61	62	63	64	92	99	67	89	69	70	71	72	73	74

ø	U stdev						0.84											90.0					0.97										
۵	Ursd %	5.76	3.6	6.32	3.77	7.09	8.37	5.79	5.1		5.37	6.1	7.39	6.67	4.89	4.6	4.09	92'9		6.98	3.63	8.65	8.23	5.75	9.49	4.33	5.71		8.14	8.02			
0	U / 238	48.60	71.86	49.07	20.57	19.07	20.26	248.55	9.88		2.08	0.53	0.53	0.48	0.47	0.50	0.56	0.64		15.88	13.52	9.02	10.40	8.89	9.30	5.20	4.01		0.05	1.36			
z	T.	3.08	4.12	3.30	3.53	3.20	2.74	5.54	5.91		4.05	3.88	3.75	3.25	2.94	3.01	3.80	4.12		6.61	9.60	7.90	8.65	10.02	12.76	12.07	9.24		90.0	6.12			
M	Pb	4.69	6.58	8.52	9.61	3.13	6.17	5.09	5.65		6.03	5.33	9.94	4.35	4.24	3.96	5.72	5.05		9.27	10.90	10.24	11.41	11.28	17.41	12.11	10.56		0.31	124.81			
٦	Se / 82	17.00	21.00	45.41	41.80	5.66	7.08	1.31												5.02		0.80	0.73		1.47	0.68	0.88		0.00	1.02			
Х	As / 75	17.00	21.70	21.27	24.60	16.39	15.94	3.70	4.50		2.75	3.09	4.48	2.57	2.45	2.37	2.75	2.70		4.04	5.32	4.68	3.95	5.43	7.45	5.77	5.17		0.03	12.86			
ſ	Zu / 66	14.04	13.34	24.81	11.84	19.35	22.09	20.00	20.31		24.69	24.28	22.22	24.62	18.83	17.42	22.99	32.07		41.11	58.23	42.59	42.30	60.19	53.67	56.33	55.39		12.23	313.67			
-	Cn / 63	0.85	0.53	1.76	0.82	4.13	5.15	3.78	6.25		90'9	5.08	5.47	4.39	4.60	4.41	6.59	5.37		13.20	7.78	5.43	8.64	7.84	5.51	7.96	13.18		2.13	68.70			
I	Mn / 55	82.13	96.47	40.86	39.95	36.00	20.13	296.71	126.09		156.59	132.06	142.64	111.64	102.43	97.94	117.46	119.77		462.82	358.05	244.89	238.35	331.65	248.30	312.71	254.94		0.65	456.13			
9	V / 51	427.25	528.65	1146.98	662.24	88.85	68.25	23.92	23.39		20.89	22.15	20.99	18.18	15.51	17.75	18.64	18.83		31.28	38.39	29.12	29.85	36.54	31.03	35.28	35.79		0:30	74.58			
F	vol (ml)	50	50	20	20	55	20	50	50		20	50	50	50	53	20	55.5	51.75		50	20	50	20	61.5	58	56.5	50		50	50.1			
Е	mass (g)	0.178	0.1885	0.2463	0.2259	0.1878	0.1486	0.2066	0.2409		0.2199	0.2628	0.2444	0.2122	0.2155	0.2231	0.237	0.2522		0.1412	0.2515	0.2105	0.1277	0.2496	0.2462	0.2338	0.2228		-	0.23			
D	Date/Time	9/6/2002	9/6/2002	9/6/2002	9/6/2002	10/2/2002 2:44	10/2/2002	9/6/2002	9/6/2002		9/6/2002	9/6/2002	9/6/2002	9/6/2002	9/6/2002	9/6/2002	9/6/2002	9/6/2002		9/6/2002	9/6/2002	9/6/2002	10/2/2002 3:03	9/6/2002	9/6/2002	9/6/2002	9/6/2002		9/6/2002	9/6/2002			
၁	sample point	1-0	1-7	1-21	1-35	1-49	1-49	1-60	1-70		2-0	2-10	2-20	2-30	2-40	2-50	2-60	2-60		3-10	3-20	3-30	3-30	3-40	3-50	3-60	3-70		Blank	std BRS 8704			
В	Sample	1030	1031	1032	1033	1078	1087	1035	1036		1037	1038	1039	1040	1042	1043	1044	1052		1045	1046	1047	1080	1048	1049	1050	1051		1053	1041			
A	Total DF	105.9	105.9	105.9	105.9	91.11	91.11	105.9	105.9		5	5	5	5	5	5	5	5		105.9	105.9	105.9	91.11	105.9	5	105.9	105.9		2	5			
	-	2	က	4	2	ၑ	7	8	6	10	11	12	13	14	15	16	17	9	19	20	21	22	23	24	25	56	27	28	58	30	3	32	33

APPENDIX G

Vegetation ICP-MS Uranium Data

	+	ر		E	ഥ	Ŋ	H	ı	ſ	K	Γ	Σ	z	0
Location	san	leaves/stems	mass (g)	vol (mi)	U / 238	U / 238	pt avg	pt stdev			Soil U	CR		
JR S27	-	-	0.2989	20	1.906	0.32	0.32	0.00			156.2			
JR S27	-A1-3	1	0.2636	20	1.717	0.33								
1000		•	.,000											
JK 527	1	leaves	0.3945	20	68.82	8.72	5.81	4.12			1			
JR S27	A1-3	stem	0.3783	20	21.88	2.89								
JR S27	-E1-2	stem	0.3951	20	0.5576	0.07	0.10	0.17			6 1			
JR S27		leaves	0.3949	50	2.415	0.31	210	1.0			0.1			
														-
JR S27	B4-3	stem	0.3973	50	0.9304	0.12	0.17	0.08			11.2			
JR S27	B4-3	leaves	0.3867	50	1.765	0.23								
JR S27	-CI-3	ī	0.3852	50	0.2189	0.03	0.07	0.04			4.6			
JR S27	-CI-3	leaves	0.3852	50	0.8135	0.11								
JR S27	-C1-3	stem	0.3788	50	0.6489	0.09								
								pt avg	pt stdev					
JR S27	CI-1	T	0.5003	50	151.5	15.14	1.78	1.21	0.17		174.4			NAME OF THE OWNER O
JR S27	CI-1	•	0.3986	50	3.462	0.43								
JR S27	C1-1	•	0.3979	50	3.493	0.44								
JR S27	C1-1	·	0.3957	50	3.655	0.46								
JR S27	C1-1	ŧ	0.398	50	5.457	0.69								***************************************
JR S27	C1-1		0.3999	50	5.179	0.65								
JR S27	C1-1	•	0.3973	50	5.254	99.0								
JR S27	CI-1	1	0.393	50	6.139	0.78								
JR S27			0.3962	50	5.915	0.75								
JR S27	CI-1	1	0.3977	50	8.907	1.12								
JR S27	CI-1	1	0.3982	50	5.983	0.75								
JR S27	C1-1	ı	0.3966	50	6.577	0.83								
JR S27		•	0.3998	50	3.187	0.40								
JR S27	C1-1	leaves	0.3948	50	8.336	1.06	1.11							
JR S27		leaves	0.3888	50	8.37	1.08								
JR S27		leaves	0.3952	50	10.15	1.28		1.09						
JR S27	CI-1	leaves	0.3899	50	8.131	1.04								
JR S27	CI-1	stem	0.3821	50	2.986	0.39	0.38							
JR S27	C1-1	stem	0.3821	50	2.82	0.37			Location	sample pt	pt avg	Soil U	S	pt stdev
JR S27	C1-1	stem	0.397	50	3.479	0.44			JR S27	Ş	0.07	4.6	1.59	0.04
JR S27	C1-1	stem	0.391	50	3.308	0.42			JR S27	B4	0.17	11.2	1.54	0.08
JR S27	C1-1	stem	0.3944	50	2.285	0.29			JR S27	-E1	0.19	8.1	2.32	0.17
JR S27	C1-3	leaves	0.3925	50	15.15	1.93	1.93	1.33	JR S27	-A1	0.32	156.2	0.21	000
JR S27	C1-3	stem	0.3970	50	5.68	0.72	0.72		JR S27	[]	1.09	174.4	0.63	0.17
						stem	0.38		JR S27	CI	1.33	174.4	0.76	
						leaves	1.11		JR S27	AI	5.81	;		4.12
-		THE RESIDENCE OF THE PROPERTY				plant	3.00							
-				-					-					

E F G H I J	vol (ml) U / 238 U (ppm) avg	50 11.51	0.4 50 5.494 0.70	50 5.853	
D E	plt/ sht mas		bogr 0.		
၁		A5-3	A5-3	A5-3	
В	Location	JR S27	JR S27	JR S27	
A	Sample:	232	233	233	L

Γ	ms			
F	leaves/stems	stem	leaves	
-	sample poin	D4-3	D4-3	
H	U (ppm)	7.62	10.23	
Ð	U/ 238	58.51	80.69	
ഥ	vol (ml)	50	50	
Э	mass (g)	0.3841	0.3945	
D	leaves/stems	stem	leaves	**************************************
င	sample point	D4-3	D4-3	
В	Location	JR S27	JR S27	
Ą	Sample:	279	280	

	Z	Soil U	6.8	63.5	139.5				
1 1	M	avg Plant U	0.35	2.16	2.52				
ſ	7		-G1-1	1		XG1-1			
1 1	4	Location	JR S27		Company and a succession				
-	2		0.35		2.16	2.52			1.16
H_I	I			0.43				The state of the s	1 68
H	1	U / 238	1.576	1.197	4.165	8.695	30.77		
٢		vol (ml)	50	90	50	50	50		
THE CHAPTER SERVICE	1	mass (g)	0.2966	0.1392	9960.0	0.3846	0.3928		
п	7	leaves/stem	stem	stem	stem	stem	seed		
٦		plt/ sht	deop	deop	qeop	deop	deop		
	2	sample poin	-G1-1	-G1-1	G5-3	XG1-1	XG1-1		
l H		Location	JR S27						
A		Sample:	180	181	189	309	310	L	
┢	Ţ		7	n	4	5	9	7	∞

	100		0.47	1 1	0.94	3.729 0.47 0.71 6.843 0.94 0.71 23.89 3.00 19.54 247 1.89
		1		I	1 1	
Ŧ,	ı		I			1 1
U / 238 3.729 6.843	3.729	6 843	2	23.89		19.54
		\vdash	0	7.3.	19	
50 50 50 50	50 50 50	50	50		50	60
mass (g) 0,3929	0.3929	-	0.3645	0.3957	0.3957	17000
eaves/stems	11000000	leaves	stem	stem	stem	leavee
	pit/ sht	erlo	erlo	erlo	erlo	erlo
	sample poin	C5-1	C5-1	E5-1	E5-1	E5-1
	Location	JR S27	JR S27	JR S27	JR S27	JR S27
A	Sample:	799		295	295	296
7	7	7	т	4	5	9

0	avg Plant U	5.26	0.86	0.95	0.48	777	25.10	030	0.89	4.6																			
Ь		G5-2	A3-1	A3-2	A5-2	D4-1	D4-2	F1.2	E5-3	F4-3																			
0																													
z																													
Σ					leaves	leaves	stem		stem	leaves		leaves	stem		stem	leaves				stem	leaves		stem	leaves		leaves		7.824281	
T		G5-2	G5-2		A3-1	A3-1	A3-1		A3-2	A3-2		A5-2	A5-2		D4-1	D4-1		D4-2		E1-2	E1-2		E5-3	E5-3		F4-3		6.13	CO CO
4		5.26				98.0				0.95		0.48			7.77			25.10			9.30			68.0		4.6			
	U / 238	6.07	4.45		1.04	69.0	69.0		1.41	0.48		0.29	99'0		5.53	10.01		25.10			13.53		0.75	1.02		4.60			
-	(mdd) n	6.07	4.45		1.04	69.0	69.0		1.41	0.48		0.29	99.0		5.53	10.01		25.10		90'9	13.53		0.75	1.02		4.60			Ī
u u	0/ 238	48.34	34.76		8.108	5.418	5.385		9.964	3.809		2.316	5.203		44.02	78.62		197.5		33.66	104.5		5.899	7.576		36.3			İ
	vol (mi)	20	20		20	20	50		20	50		20	50		20	50		50		20	50		50	20		50			
1	mass (g)	0.3985	0.3905		0.3908	0.3908	0.3888		0.3530	0.3966		0.3991	0.3918		0.3979	0.3926		0.3934		0.3323	0.3861		0.3935	0.3707		0.3946			
Towns from	leaves/stem				leaves	leaves	stem		stem	leaves		leaves	stem		stem	leaves				stem	leaves		stem	leaves		leaves			
alt obt	più sut	gusa	gusa		gusa	gusa	gusa		gusa	gusa		gusa	gusa		gusa	gusa		gusa		gusa	gusa		gusa			gusa			
nion olumb	sample poin	2-65	G5-2		A3-1	A3-1	A3-1		A3-2	A3-2		A5-2	A5-2		<u>4</u>	D4-1		D4-2		E1-2	E1-2		E5-3	E5-3		F4-3			
7		JR 52/	JR S27		JR S27	JR S27	JR S27		JR S27	JR S27		JR S27	JR S27		JR S27	JR S27		JR S27		JR S27	JR S27		JR S27	JR S27		JR S27			
Commis.	Sampine.	213	214		220	220	221		222	223		230	253		ı	277		278		301	289		298	299		308			
-	1	1	-	4	~	٥	7	00	6	9	=1	7	13	4	्य	16	17	18	19	2	21	22	23	24	25	26	27	28	-

-	-	_	-						_			-	-,							-,
c	Soil 11	156 20	11.20	11 20	63.50	73.30	50.70	06.00	50.80	50.80						e/u	377			
а	ave plant []	0.79	0.05	0.66	465	0.85	3.44	0.72	5.46	2.40						84 47				
0	sample point		R4-1	B4-2	G5-1	A3-3	R2-2	E5-2	F4-1	F4-2						A1-2				
z																				
Z																				
H	Soil U	156.2		n/a		11.2	11.2		63.5		73.3			50.7	6.6	50.8	50.8			
×	avg plant U	0.29		84.47 n		0.95	99.0		4.65		0.85			3.44	0.72	5.46	2.40			
~	sample poin avg plant U	-A1-2	-A1-2	A1-2	A1-2	B4-1	B4-2	B4-2	G5-1	G5-1	A3-3	A3-3	A3-3	B2-2	E5-2	F4-1	F4-2			
,	U (ppm) s		0.31	63.16	105.79	0.95	0.59	0.73	4.10	5.20	0.79	0.95	0.81	3.44	0.72	5.46	2.40		12.23	29.30659
Н	U / 238	1.959	1.918	502	833.6	7.376	4.602	5.755	32.2	40.04	6.182	7.562	6.314	26.27	5.737	42.39	18.93		plant avg	plant stdev
G	vol (ml)	50	50	50	50	50	50	50	50	20	20	20	50	20	50	20	50		a	ď
F.	mass (g)	0.3612	0.3103	0.3974	0.3940	0.3864	0.3924	0.3927	0.3935	0.387	0.3926	0.3963	0.3913	0.3823	0.3967	0.3882	0.3946			
Ε	leaves/stems	•	ı	ī	1		r		,	1	t	1	,	1	1	ı	1			
Ω	plt/sht	hija	hija	hija	hija	hija	hija	hija	himu											
ပ	sample point	-A1-2	-A1-2	A1-2	A1-2	B4-1	B4-2	B4-2	G5-1	G5-1	A3-3	A3-3	A3-3	B2-2	E5-2	F4-1	F4-2			
8	Location	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27			
A	Sample:	207	208	216	217	240	241	254	168	169	224	225	226	236	297	305	306			
7	-	7	33	4	5	9	7	8	6	2	Ξ	12	13	14	15	16	17	18	19	20

-	V	B	0		Ε	H	g	Н	I	l l	K	Т	M	Z
-1	Sample:	Location	sample poin	plt/ sht	leaves/stem	mass (g)	vol (ml)	U/ 238	U / 238			sample poin Plant U		Soil U
7	205	JR S27	-A1-1	kosc		0.2137	50	1.926	0.45			-A1-1	0.65	156.2
3	206	JR S27	-A1-1	kosc		0.1629	50	2.094	0.64	0.65		B2-1	3.00	507
4	206	JR S27	-A1-1	kosc		0.1629	50	2.831	0.87			C1-2	28.80	1744
5	234	JR S27	B2-1	kosc		0.1491	50	8.951	3.00	3.00		3-1	1 22	13.8
9	250	JR S27	C1-2	kosc		0.3975	50	229.7	28.89	28.89		D2-2	27.43	6179
7	257	JR S27	C3-1	kosc		0.3922	50	9.559	1.22	1.22		-E1-1	0.44	8
∞	273	JR S27	D2-2	kosc	•	0.3958	50	223.1	28.20	27.425		E3-1	16.42	26.3
6	273	JR S27	D2-2	kosc		0.3958	50	211	26.65			E3-2	6.38	26.3
10	281	JR S27	-E1-1	kosc	stem	0.2805	50	2.635	0.47	0.44		E3-3	5.87	26.3
=	282	JR S27	-E1-1	kosc	leaves	0.3725	50	2.998	0.40			F2-1	347.67	1040.45
12	292	JR S27	E3-1	kosc	-	0.2423	50	79.56	16.42	16.42		F2-2	323.55	1040.45
13	293	JR S27	E3-2	kosc		0.2819	50	35.96	6.38	6.38		F2-3	343.60	1040.45
4	294	JR S27	E3-3	kosc		0.1539	50	18.07	5.87	5.87		H4-1	5.44	150.2
15	302	JR S27	F2-1	kosc		0.3417	50	2376	347.67	347.67				
16	303	JR S27	F2-2	kosc	,	0.3100	50	2006	323.55	323.55				
17	304	JR S27	F2-3	kosc		0.0953	50	624.9	343.60	343.60	12.91413		5.94822	
18	741	JR S27	H4-1	kosc		0.2453	50	26.68	5.44	5.44				
19														
20									92.09	92.09 144.5457				

I														
	A	В	၁	Ω	田	IT.	Ð	H	Н	ſ	노	T	Σ	z
-	322	Location												
7] 2 6 0	JR S27	C4-1	memn	stem	0.3909	50	101.1	12.93	27.70	11.31		27.70	11.31
3		JR S27	C4-1	memn	leaves	0.3899	50	331.1	42.46			AND DESCRIPTION OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF	26.76	11.31
4		JR S27	C4-2	memn	stem	0.3868	50	207	26.76	26.76	11.31		29.58	11.31
5		JR S27	C4-3	memn	leaves	0.3999	50	363.6	45.46	29.58	11.31		The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa	
9	326	JR S27	C4-3	memn	stem	0.3976	50	108.9	13.69	***************************************		THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF THE PARTY NAMED AND ADDRESS OF		
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=	Sample:	Location	sample poin	plt/sht	eaves/stem	mass (g)	vol (ml)	U / 238	(mdd) n	U / 238	sample point	Avg Plant U	Soil U		Avg Plant U	Soil U
7	136 136	JR S27	H2-1	orhy	ı	0.3978	50	35.69	4.50	4.5	H2-1	5.52	129.2	H2-1	5.52	129.20
6	137	JR S27	H2-1	orhy	,	0.3985	50	34.82	4.40	4.4	H2-1			G3-1	9.35	58.90
4	138	JR S27	H2-1	orhy	•	0.3998	50	54.97	6.90	6.9	H2-1			H2-2	25.98	129.20
5	139	JR S27	H2-1	orhy	•	0.3974	50	43.44	5.50	5.5	H2-1			G1-1	13.63	139.50
9	140	JR S27	H2-1	orhy		0.3999	50	37.24	4.70	4.7	H2-1			H2-2	12.62	129.20
7	141	JR S27	H2-1	orhy	1	0.3979	50	38.32	4.80	4.8	H2-1			H2-3	65.90	129.20
8	150	JR S27	H2-1	orhy	•	0.3959	50	40.39	5.10	5.1	H2-1					
6	151	JR S27	H2-1	orhy		0.3968	50	38.25	4.80	4.8	H2-1					
10	152	JR S27	H2-1	orhy		0.3948	50	50.89	6.40	6.4	H2-1			Page 1		
11	153	JR S27	H2-1	orhy	•	0.398	50	54.72	06:9	6.9	H2-1					
12	154	JR S27	H2-1	orhy		0.3928	50	35.35	4.50	4.5	H2-1					
13	156	JR S27	H2-1	orhy		0.397	50	43.18	5.40	5.4	H2-1					
14	158	JR S27	H2-1	orhy	,	0.3866	50	51.14	6.61	6.614071	H2-1				THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUMN TO THE PE	
15	158	JR S27	H2-1	orhy		0.3866	50	52.58	08.9	6.8	H2-1					
16	170	JR S27	G3-1	orhy		0.3895	50	79.43	10.20	10.2	G3-1	9.35	58.9			
17	171	JR S27	G3-1	orhy		0.393	50	66.72	8.50	8.5	G3-1		-			
18	178	JR S27	H2-2	orhy	•	0.3970	50	211.9	26.69	26.68766	H2-2	25.98	129.2			
19	178	JR S27	H2-2	orhy	•	0.3970	50	200.7	25.28	25.27708	H2-2					
20	182	JR S27	G1-1	orhy	•	0.3950	50	102.5	12.97	12.97468	GI-1	13.63	139.5			
21	183	JR S27.	G1-1	orhy	,	0.3886	50	111	14.28	14.28204	GI-1					The second
22	188	JR S27	H2-2	orhy		0.3942	20	99.48	12.62	12.61796	H2-2	12.62	129.2			
23	190	JR S27	H2-3	orhy	·	0.3947	50	459.4	58.20	58.1961	H2-3	65.90	129.2			
24	204	JR S27	H2-3	orhy		0.3989	50	587.2	73.60	73.60241	H2-3					

c_map_by_species_S27

В	В		D		E	щ	G	H		J	K	Γ	M	Ŋ	0
sample poin plt/ sht leaves/stems	Location sample poin plt/sht leaves/stems	plt/ sht leaves/stems	leaves/stems	S	ma	mass (g)	vol (ml)	U / 238	586	Avg plant U	sample point		sample point	Avg plant U	
JR S27 G3-3 spcr -	G3-3 sper -	G3-3 sper -	•	.0	0	3668	50	85.07	1000	11.34	G3-3		G3-3	11.34	l
G3-3 sper -	G3-3 sper -	G3-3 sper -	*		0	3991	50	96.13	0.441		G3-3		G1-2	41.09	
JR S27 G1-2 spor -	G1-2 spcr -	G1-2 spcr -			$^{\circ}$.2669	50	274.2	51.37	41.09	G1-2		B2-3	B2-3 2.49	50.7
JR S27 G1-2 spor -	G1-2 spcr -	G1-2 spcr -	3	1		0.1511	50	93.11	30.81		G1-2				1
JR S27 A5-1 spcr -	A5-1 spcr -	A5-1 spcr -		•	.	0.3754	50	8.151	1.09	1.09	A5-1				
237 JR S27 B2-3 spcr -	B2-3		spcr -	•	-	0.3910	50	15.1	1.93	2.49	B2-3		A5-1	1.09	
ı	B2-3		sper -	1		0.3896	50	23.81	3.06		B2-3				
									15.85						
									18.61865						

_	T	6	3	19	19	16	16	-	Т	T	T	Ţ	Т	T
ď	Soil U	58.9	139.5	4.6	4.6	621.9	621.9	8.		and the second				
0		12.70	40.42	0.07	0.085	21.54	33.49	0.53						
z	sample poin avg plant U	G3-2	G1-3	-C1-1	-C1-2	D2-1	D2-3	-E1-3						***************************************
Z										-	-			
7														
×	sample point	G3-2	G3-2	G1-3	G1-3	-CI-1	-C1-2	-C1-2	D2-1	D2-1	D2-3	-E1-3	-E1-3	15.55 16.77596
<u> </u>	SS	12.70		40.42		0.07	0.085		21.54		33.49	0.53		15.55
	U (ppm)	13.20	12.20	29.88	50.95	0.07	20.0	0.10	11.95	31.14	33.49	69.0	0.37	
Н	U / 238	85.76	26.42	192.8	331.2	0.5395	0.5423	0.8258	49.18	247.4	255.3	5.49	2.913	
G	vol (ml)	50	50	50	50	50	50	50	20	50	50	50	50	
F	mass (g)	0.3244	0.108	0.3226	0.3250	0.3615	0.3890	0.3957	0.2058	0.3973	0.3812	0.3963	0.3903	
E	leaves/stem	1	•		•	stem	stem	leaves	stem	leaves		leaves	stem	
Ω	pit/sht	saka	saka	saka	saka	satr	satr	satr	satr	satr	satr	satr	satr	
၁	sample poin	G3-2	G3-2	G1-3	G1-3	-C1-1	-C1-2	-C1-2	D2-1	D2-1	D2-3	-E1-3	-E1-3	
В	Location	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	JR S27	
Ą	Sample:	172	173	186	187			247	271	272	274	285	286	
	\exists	7	n	4	S	9	7	∞	6	10	11	12	13	14

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Д	Soil U	71.6	58.9	8.09	13.8	8.09	79.4	8.09	6.6	na
ပ	avg plant U	5.78	2.92	1.54	4.24	0.78	8.93	0.71	1.89	17.9
В			2	3	4	5	9	7	7	grsq
A	plant	asbr	asta	paob	scbr	sihy	chna	erlo	erlo	
	9	7	8	6	10	11	12	13	14	15